

**FORMULAS
IN GEARING**

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FORMULAS

IN

GEARING.

FIFTH EDITION.

Charles E. Stealy

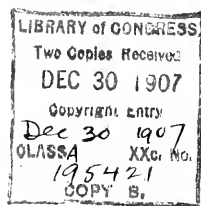
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Preface.

This book deals with the subject of Gearing essentially from the draughtsman's standpoint.

Its aim is to condense as much as possible the solution of all problems in gearing which in the ordinary practice may be met with, to the exclusion of problems dealing with transmission of power and strength of gearing.

The simplest and briefest being the symbolical expression, it has, whenever available, been resorted to. The mathematics employed are of a simple kind, and will present no difficulty to any one familiar with ordinary Algebra and the elements of Trigonometry.

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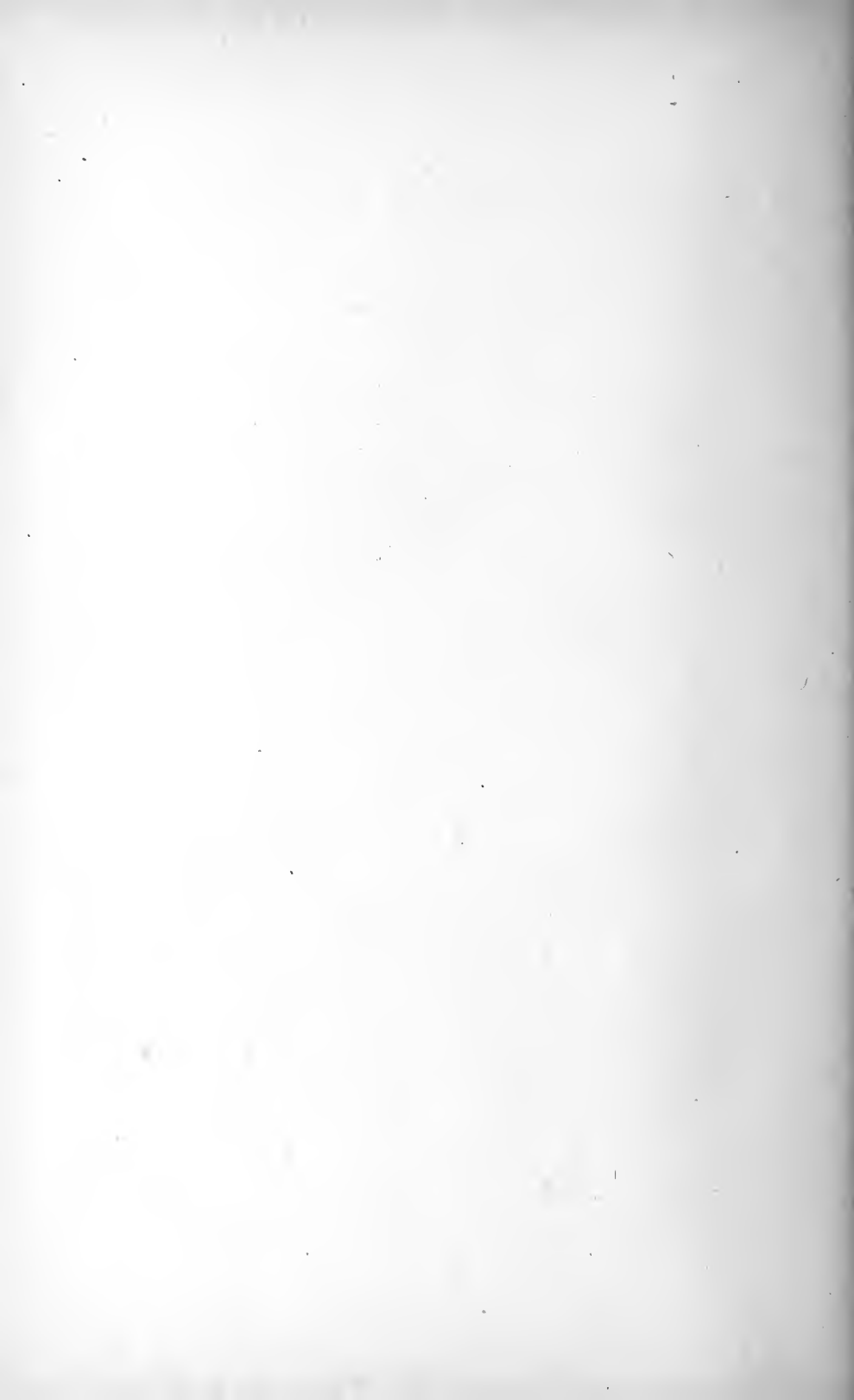
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FORMULAS IN GEARING.

CHAPTER I.

SYSTEMS OF GEARING.

There are in common use two systems of gearing, viz.: the involute and the epicycloidal.

In the involute system the outlines of the working parts of a tooth are single curves, which may be traced by a point in a flexible, inextensible cord being unwound from a circular disk the circumference of which is called the *base circle*, the disk being concentric with the pitch circle of the gear.

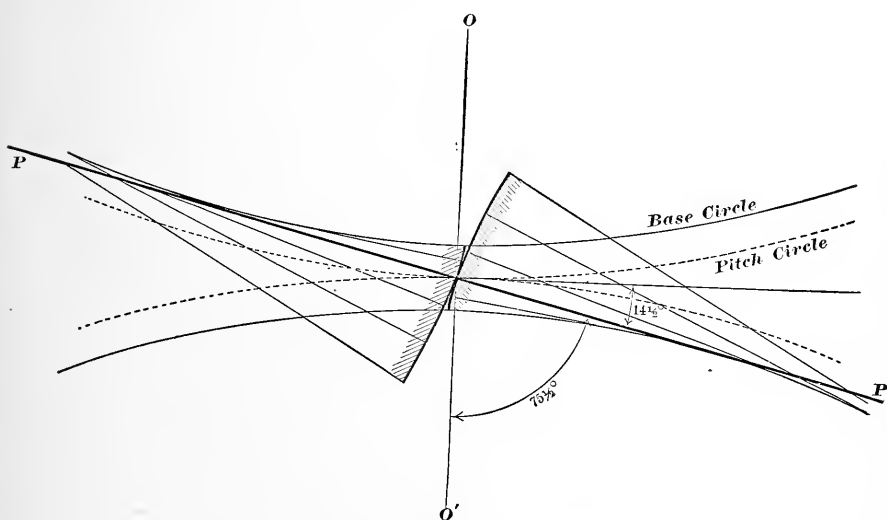


Fig. 1.

In *Fig. 1* the two base circles are represented as tangent to the line P P. This line (P P) is variously called "the line of pressure," "the line of contact," or "the line of action."

In our practice this is drawn so as to make with a normal to the centre line ($O O'$) $14\frac{1}{2}^\circ$, or with the centre line $75\frac{1}{2}^\circ$.

The rack of this system has teeth with straight sides, the two sides of a tooth making, together, an angle of 29° (twice $14\frac{1}{2}^\circ$).

This applies to gears having 30 teeth or more. For gears having less than 30 teeth special rules are followed, which are explained in our "Practical Treatise on Gearing."

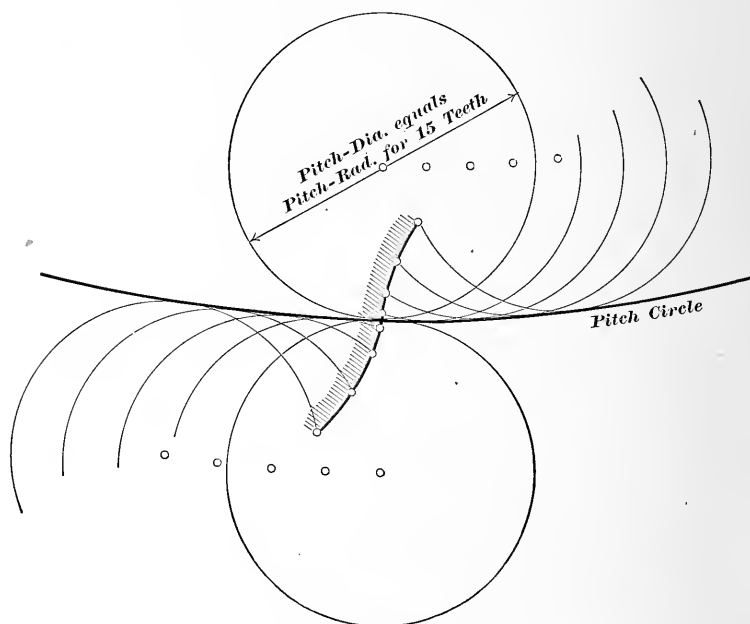


Fig. 2.

In *epicycloidal*, or double-curve teeth, the formation of the curve changes at the pitch circle. The outline of the faces of epicycloidal teeth may be traced by a point in a circle rolling on the *outside* of pitch circle of a gear, and the flanks by a point in a circle rolling on the *inside* of the pitch circle. The faces of one gear must be traced by the same circle that traces the flanks of the engaging gear.

In our practice the diameter of the rolling or describing circle is equal to the radius of a 15-tooth gear of the pitch required; this is the base of the system. The same describing circle being used for all gears of the same pitch.

The teeth of the rack of this system have double curves, which may be traced by the base circle rolling alternately on each side of the pitch line.

An advantage of the involute over the epicycloidal tooth is, that in action gears having involute teeth may be separated a little from their normal positions without interfering with the angular velocity, which is not possible in any other kind of tooth.

The obliquity of action is sometimes urged as an objection to involute teeth, but a full consideration of the subject will show that the importance of this has been greatly over-estimated.

The tooth dimensions for both the involute and epicycloidal gears may be calculated from the formulas in Chapter II.

CHAPTER II.

SPUR GEARING.

Two spur gears in action are comparable to two corresponding plain rollers whose surfaces are in contact, these surfaces representing the pitch circles of the gears.

PITCH OF GEARS.

For convenience of expression the pitch of gears may be stated as follows:

Circular pitch is the distance from the centre of one tooth to the centre of the next tooth, measured on the pitch line.

Diametral pitch is the number of teeth in a gear per inch of pitch diameter. That is, a gear that has, say, six teeth for each inch in pitch diameter is six diametral pitch, or, as the expression is universally abbreviated, it is "six pitch." This is by far the most convenient way of expressing the relation of diameter to number of teeth.

Module is the pitch diameter of a gear divided by the number of teeth.

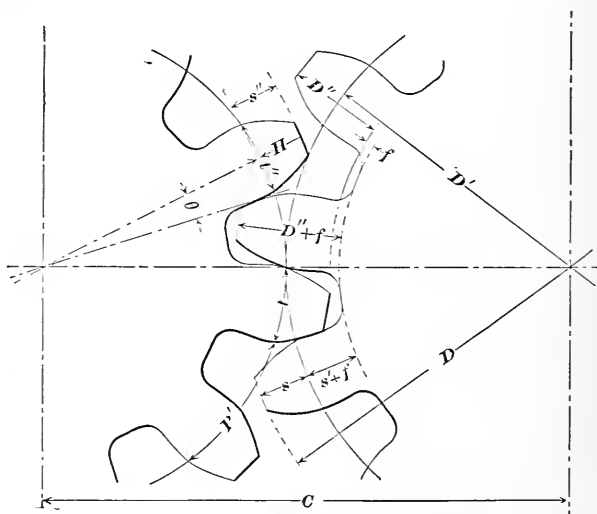


Fig. 3.

FORMULAS.

N = number of teeth.

s = addendum and module.

t = thickness of tooth on pitch line.

t'' = chordal thickness of tooth.

f = clearance at bottom of tooth.

D'' = working depth of tooth.

$D'' + f$ = whole depth of tooth.

D' = pitch diameter.

D = outside diameter.

P' = circular pitch.

P = diametral pitch.

H = height of arc.

s'' = distance from chord to top of tooth.

c = centre distance.

θ = $\frac{1}{4}$ the angle subtended by circular pitch.

$$P = \frac{N + 2}{D} = \frac{\pi}{P'}$$

$$P' = \frac{\pi}{P} = d \pi \frac{\theta}{90^\circ} = \frac{D' \pi}{N}$$

$$s = \frac{1}{P} = \frac{P'}{\pi} = .3183 P' = \frac{D'}{N} = \frac{D}{N + 2}$$

$$t = \frac{P'}{2} = \frac{\pi}{2P}$$

$$f = \frac{t}{10}$$

$$s + f = \frac{1}{P} \left(1 + \frac{\pi}{20} \right) = .3683 P'$$

$$D'' = 2 s = \frac{2}{P}$$

$$D'' + f = \frac{2.157}{P} = .6866 P'$$

$$D' = \frac{N}{P} = \frac{N P'}{\pi}$$

$$D = D' + 2 s = \frac{N + 2}{P}$$

$$\theta = \frac{90^\circ}{N}$$

$$t'' = D' \sin \theta$$

$$H = \frac{D'(1 - \cos \theta)}{2}$$

$$s'' = s + H$$

CHAPTER III.

BEVEL GEARS—AXES AT RIGHT ANGLES.

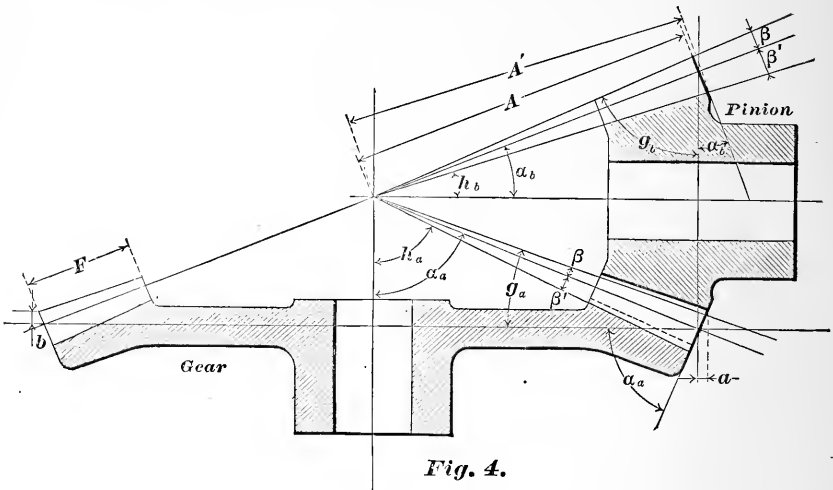


Fig. 4.

FORMULAS.

$N_a =$ } Number of teeth { gear.
 $N_b =$ } pinion.

$P =$ diametral pitch. $P' =$ circular pitch.

$\alpha_a =$ } centre angle = angle of edge { gear.
 $\alpha_b =$ } or pitch angle. { pinion.

$\beta =$ angle of top. $\beta' =$ angle of bottom.

$g_a =$ } angle of face { gear.
 $g_b =$ } pinion.

$h_a =$ } cutting angle { gear.
 $h_b =$ } pinion.

$A =$ apex distance from pitch circle.

$A' =$ apex distance from large bottom of tooth.

$D' =$ pitch diameter. $D =$ outside diameter.

$s =$ addendum and module.

$t =$ thickness of tooth at pitch line.

$f =$ clearance at bottom of tooth.

$D'' =$ working depth of tooth.

$D'' + f =$ whole depth of tooth. $2a =$ diameter increment.

$b =$ distance from top of tooth to plane of pitch circle.

$F =$ width of face.

$$\tan \alpha_a = \frac{N_a}{N_b}; \quad \tan \alpha_b = \frac{N_b}{N_a};$$

$$\tan \beta = \frac{2 \sin \alpha}{N}; \text{ or } \tan \beta = \frac{s}{A}.$$

$$\tan \beta' = \frac{\sin \alpha \left(2 + \frac{\pi}{10}\right)}{N} = \frac{2.314 \sin \alpha}{N}; \quad \tan \beta' = \frac{s + f}{A};$$

$$g_a = 90^\circ - (\alpha_a + \beta); \quad g_b = 90^\circ - (\alpha_b + \beta)$$

$$h = \alpha - \beta' \quad (\text{See page 41.})$$

$$A = \sqrt{\left(\frac{N_a}{2P}\right)^2 + \left(\frac{N_b}{2P}\right)^2}$$

$$A = \frac{N}{2 P \sin \alpha}$$

$$A' = \frac{A}{\cos \beta'} \quad A' = \frac{N}{2 P \sin \alpha \cos \beta'}$$

$$A = \frac{\frac{1}{2} D}{\sin (\alpha + \beta)} \cos \beta$$

$$P = \frac{N}{2 A \sin \alpha}$$

$$D' = \frac{N}{P} \text{ or } = \frac{N P'}{\pi} \quad D = D' + 2 a$$

$$2 a = 2 s \cos \alpha \quad (\text{For tables see pages 70 to 73.})$$

$$b = a \tan \alpha \begin{cases} a \text{ for gear} = b \text{ for pinion} \\ a \text{ for pinion} = b \text{ for gear} \end{cases}$$

$$P = \frac{\pi}{P'} \quad P' = \frac{\pi}{P}$$

$$s = \frac{1}{P} = \frac{P'}{\pi} = .3183 \quad P' = A \tan \beta$$

$$s + f = .3685 \quad P' = A \tan \beta' = \frac{1}{P} \left(1 + \frac{\pi}{20}\right)$$

$$D'' = 2 s$$

$$t = \frac{P'}{2} = \frac{\pi}{2 P} \quad f = \frac{t}{10}$$

$$*F = \frac{A}{3} \text{ or } *F = \frac{5 P'}{2}$$

NOTE.—Formulas containing notations without the designating letters a and b apply equally to either gear or pinion. If wanted for one or the other, the respective letters are simply attached.

*The formula giving the lesser value of F should always be used.

BEVEL GEARS WITH AXES AT ANY ANGLE.

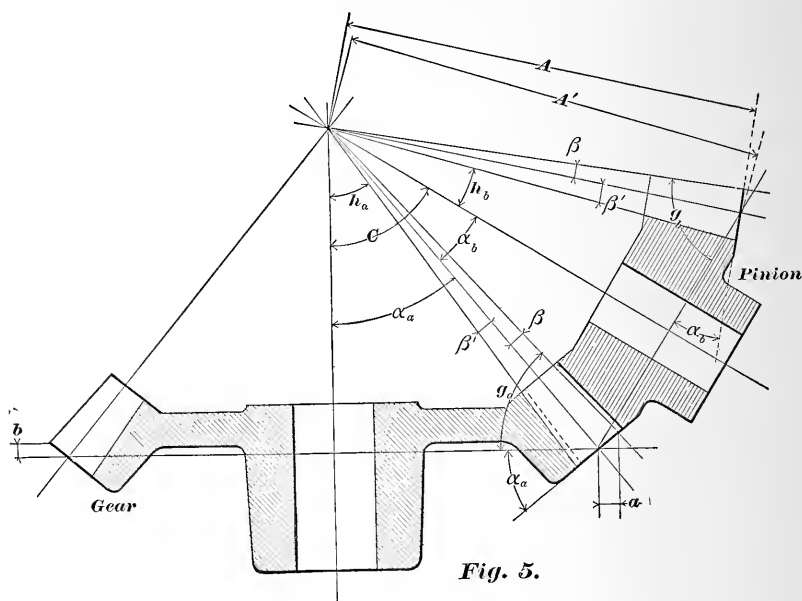


Fig. 5.

FORMULAS.

C = angle formed by axes of gears.

N_a = } number of teeth { gear.
 N_b = } number of teeth { pinion.

P = diametral pitch. P' = circular pitch.

α_a = } angle of edge = pitch angle { gear.
 α_b = } angle of edge = pitch angle { pinion.

β = angle of top. β' = angle of bottom.

g_a = } angle of face { gear.
 g_b = } angle of face { pinion.

h_a = } cutting angle { gear.
 h_b = } cutting angle { pinion.

A = apex distance from pitch circle.

A' = apex distance from large bottom of tooth.

D' = pitch diameter. D = outside diameter.

$2a$ = diameter increment.

b = distance from top of tooth to plane of pitch circle.

NOTE.—The formulas for tooth parts as given on page 13 apply equally to these cases.

$$\tan \alpha_a = \frac{\sin C}{\frac{N_b}{N_a} + \cos C}; \text{ or } \cot \alpha_a = \frac{N_b}{N_a \sin C} + \cot C$$

$$\tan \alpha_b = \frac{\sin C}{\frac{N_a}{N_b} + \cos C}; \text{ or } \cot \alpha_b = \frac{N_a}{N_b \sin C} + \cot C$$

NOTE.—The above formulas are correct only for values of C less than 90° . If C is greater than 90° , consult page 19.

$$\tan \beta = \frac{2 \sin \alpha}{N}; \text{ or } \tan \beta = \frac{s}{A};$$

$$\tan \beta' = \frac{\sin \alpha \left(2 + \frac{\pi}{10}\right)}{N} = \frac{2.314 \sin \alpha}{N}; \tan \beta' = \frac{s+f}{A};$$

$$g_a = 90^\circ - (\alpha_a + \beta) \text{ for Cases I and II.}$$

$$g_a = \beta, \text{ for Case III.}$$

$$g_a = 90^\circ - (\alpha_a - \beta) \text{ for Case IV.}$$

$$g_b = 90^\circ - (\alpha_b + \beta)$$

$$h = \alpha - \beta' \quad (\text{See page 41.})$$

$$A = \frac{N}{2 P \sin \alpha}$$

$$A' = \frac{A}{\cos \beta'}$$

$$D' = \frac{N}{P} \text{ or } \frac{N P'}{\pi}$$

$$D = D' + 2 a \left\{ \begin{array}{l} \text{for Cases I and II,} \\ \text{and pinions in Cases III and IV.} \end{array} \right.$$

$$D = D', \text{ for gear in Case III.}$$

$$D = D' - 2 a, \text{ for gear in Case IV.}$$

$$2 a = 2 s \cos \alpha$$

$$b = s \sin \alpha$$

NOTE.—Formulas containing notations without the designating letters a and b apply equally to either gear or pinion. If wanted for one or the other, the respective letters are simply attached.

The formulas given for α_a and α_b (when C , N_a and N_b are known) undergo some modifications for values of C greater than 90° .

For bevel gears at any angle but 90° we may distinguish four cases; C , N_a , N_b being given.

I. Case. See pages 16 and 17.

II. Case. C is greater than 90° .

$$\tan \alpha_a = \frac{\sin (180 - C)}{\frac{N_b}{N_a} - \cos (180 - C)}; \quad \tan \alpha_b = \frac{\sin (180 - C)}{\frac{N_a}{N_b} - \cos (180 - C)}$$

III. Case. $\alpha_a = 90^\circ$; $\alpha_b = C - 90^\circ$

IV. Case.

$$\tan \alpha_a = \frac{\sin E}{\cos E - \frac{N_b}{N_a}}; \quad \tan \alpha_b = \frac{\sin E}{\frac{N_a}{N_b} - \cos E}$$

For an example to apply to Case III., the following condition must be fulfilled:

$$N_a \sin (C - 90^\circ) = N_b$$

To distinguish whether a given example belongs to Case II. or Case IV., we are guided by the following condition:

Is: $N_a \sin (C - 90^\circ)$ $\begin{cases} \text{smaller than } N_b, \text{ we have Case II.} \\ \text{larger than } N_b, \text{ we have Case IV.} \end{cases}$

UNDERCUT IN BEVEL GEARS.

By undercut in gears is understood a special formation of the tooth, which may be explained by saying that the elements of the tooth below the pitch line are nearer the centre line of the tooth than those on the pitch line. Such a tooth outline is to be found only in gears with few teeth. In a pair of bevel gears where the pinion is low-numbered and the ratio high, we are apt to have undercut. For a pair of running gears this condition presents no objection. Should, however, these gears be intended as patterns to cast from, they would be found useless, from the fact that they would not draw out of the sand. We have stated on page 10 (see Fig. 1) that the base of our involute system is the $14\frac{1}{2}^\circ$ pressure angle.

If a pair of bevel gears with teeth constructed on this basis have undercut, we can nearly eliminate the undercut—and for the practical working this is quite sufficient—by taking as a basis for the construction of the tooth outline a pressure angle of 20° .

The question now is: When do we and when do we not have undercut? Let there be:

N = number of teeth in gear.

n = number of teeth in pinion.

$$\frac{n\sqrt{N^2 + n^2}}{N} = \phi$$

where we have undercut for ϕ less than 30 .

This formula is strictly correct for epicycloidal gears only. It is, however, used as a safe and efficient approximation for the involute system.

WORM AND WORM WHEEL.



FORMULAS.

L = lead of worm.

N = number of teeth in gear.

m = turns per inch of worm.

d = diameter of worm.

d' = pitch diameter of worm.

d'' = diameter of hob.

D = throat diameter.

D' = pitch diameter of worm wheel.

B = blank diameter (to sharp corners).

C = distance between centres.

P = diametral pitch.

P' = circular pitch for worm wheels or axial pitch for worms.

$\left. \begin{matrix} r' \\ r'' \end{matrix} \right\}$ See figure 7.

s = addendum and module.

t = thickness of tooth at pitch line.

t^n = normal thickness of tooth.

f = clearance at bottom of tooth.

D'' = working depth of tooth.

$D'' + f$ = whole depth of tooth.

b = pitch circumference of worm.

v = width of worm thread tool at end.

w = width of worm thread at top and width of hob tool at end.

δ = angle of tooth of worm wheel with its axis, or the angle of thread of worm with a line at right angles to its axis.

If the lead is for single, double, triple, etc., thread, then

$$L = P', 2 P', 3 P', \text{ etc.}$$

In multiple threaded worms and their mating wheels, if the angle δ is more than 15° the tooth parts should be figured on the normal as for spiral gears. In using the formulas for spiral gears, it should be borne in mind that while P' is the axial pitch for worms it is the circular pitch for spiral gears.

$$\alpha = 60^\circ \text{ to } 90^\circ$$

$$L = \frac{1}{m}$$

$$P' = \frac{\pi T}{N + 2}$$

$$D' = \frac{N P'}{\pi} = \frac{N}{P}$$

$$D = \frac{N}{P} + 2s$$

$$b = \pi (d - 2s) = \pi d'$$

$$\tan \delta = \frac{L}{b} \quad \left\{ \begin{array}{l} \text{Practical only when width of wheel on wheel pitch} \\ \text{circle is not more than } \frac{2}{3} \text{ pitch diameter of worm.} \end{array} \right.$$

$$t^n = t \cos \delta$$

$$r' = \frac{d}{2} - 2s$$

$$r'' = r' + D'' + f$$

$$C = \frac{D' + d}{2} - s = \frac{D' + d''}{2}$$

$$B = D + 2 \left(r' - r' \cos \frac{\alpha}{2} \right) \quad \begin{array}{l} \text{A measurement of sketch is} \\ \text{generally sufficient.} \end{array}$$

$$d'' = d + 2f$$

$$v = .31 P'$$

$$w = .335 P'$$

NOTE.—The notations and formulas referring to tooth parts, given on page 13, for spur gears, apply to worm wheels and are here used.

NOTE.—Hob and worm should be marked, as per example :

4 turns per 1" single .25 P' ; .25 L.

2 turns per 1" double .25 P' ; .50 L.

UNDERCUT IN WORM WHEELS.

In worm wheels of less than 30 teeth the thread of the worm (when 29°) interferes with the flank of the gear tooth. Such a wheel finished with a hob will have its teeth undercut. To avoid this interference two methods may be employed.

First Method.—Make throat diameter of wheel

$$D = \cos^2 14\frac{1}{2}^\circ \frac{N}{P} + 4s = \frac{.937 N}{P} + 4s$$

This formula increases the throat diameter, and consequently the centre distance. The amount of the increase can be found by comparing this value of D with the one as obtained by formula on page 23. To keep the original centre distance, the outside diameter of the worm must be reduced by the same amount the throat diameter is increased.

Second Method.—Without changing any of the dimensions we found by the formulas given on page 23, we can avoid the interference to be found in worm wheels of less than 30 teeth by simply increasing the angle of worm thread. We find the value of this angle by the following formula:

Let there be

2γ = angle of worm thread.

N = number of teeth in worm wheel.

$$\cos \gamma = \sqrt{1 - \frac{2}{N}}$$

From this formula we obtain the following values:

N	29	28	27	26	25	24	23	22	21	20
2γ	$30\frac{1}{4}$	31	$31\frac{1}{2}$	$32\frac{1}{4}$	$32\frac{3}{4}$	$33\frac{1}{2}$	$34\frac{1}{4}$	35	36	37

N	19	18	17	16	15	14	13	12
2γ	38	39	40	$41\frac{1}{2}$	$42\frac{3}{4}$	$44\frac{1}{2}$	$46\frac{1}{4}$	48

As this latter formula involves the making of new hobs in many cases, on account of change of angle, we prefer to reduce the diameter of worm as indicated by first method, if the distance of centres must be absolute.

CHAPTER V.

SPIRAL OR SCREW GEARING.

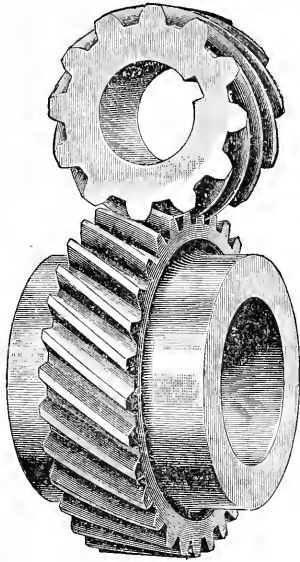


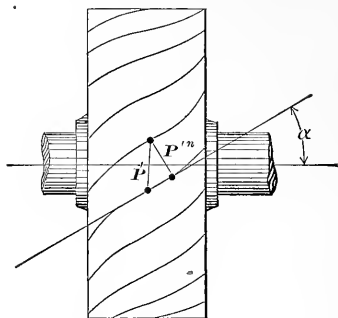
Fig. 8.

RIGHT HAND SPIRAL GEARS.

In spiral gearing the wheels have cylindrical pitch surfaces, but the teeth are not parallel to the axis. The line in which the pitch surface intersects the face of a tooth is part of a screw line, or helix, drawn at the pitch surface. A screw wheel may have one or any number of teeth. A one-toothed wheel corresponds to a one-threaded screw, a many-toothed wheel to a many-threaded screw. The axes may be placed at any angle.

Consider spiral gears with :

- I. Axes parallel.
- II. Axes at right angles.
- III. Axes any angle.

**Fig. 9.**

LEFT HAND SPIRAL GEAR.

Let there be :

$$\left. \begin{array}{l} N_a = \\ N_b = \end{array} \right\} \text{ number of teeth in gears } \left\{ \begin{array}{l} a \\ b \end{array} \right.$$
 C = centre distance. P' = circular pitch (circumferential not axial). P^n = normal diametral pitch. P'^n = normal circular pitch. γ = angle of axes. L_1 = exact lead of spiral on pitch surface. L_2 = approximate lead of spiral on pitch surface. T = number of teeth marked on cutter to be used when teeth are to be cut on milling machine. D' = pitch diameter. D = outside diameter.
$$\left. \begin{array}{l} \alpha_a = \\ \alpha_b = \end{array} \right\} \text{ angle of teeth with axis}$$
 t = thickness of tooth. s = addendum and module. $D'' + f$ = whole depth of tooth.NOTE.—Letters a and b occurring at bottom of notations refer to gears a and b .

I.—AXES PARALLEL.

Gears of this class are called twisted gears. The angle of teeth with axes in both gears must be equal and the spirals run in opposite directions. The angles are generally chosen small (seldom over 20°) to avoid excessive end thrust. End thrust may, however, be entirely avoided by combining two pairs of wheels with right and left-hand obliquity. Gears of this class are known as Herringbone gears. They are comparatively noiseless running at high speed.

II.—AXES AT RIGHT ANGLES.

Here we must always have:

1. The teeth of same hand spiral;
2. The normal pitches equal in both gears; and
3. The sum of the angles of teeth with axes = 90° .

CHOOSING ANGLE OF TEETH WITH AXES.

1. If in a pair of gears the ratio of the number of teeth is equal to the direct ratio of the diameters, *i. e.*, if the number of teeth in the two gears are to each other as their pitch diameters, then the angles of the spirals will be 45° and 45° ; for, this condition being fulfilled, the circular pitches of the two gears must be alike, which is only possible with angles of 45° . In such a combination either gear may be the driver.

2. If the ratio of the diameters determined upon is larger or smaller than the ratio of the number of teeth, then the angles are:

$$\tan \alpha_a = \frac{D'_a N_b}{D'_b N_a} \quad \tan \alpha_b = \frac{D'_b N_a}{D'_a N_b}$$

In such gears the velocity ratio is measured by the number of teeth, and not by the diameters.

3. Given N_a , N_b and C :

If P_a' is made = P_b' , then we have case "1" and

$$P' = \frac{\pi C}{\frac{1}{2}(N_a + N_b)}$$

But if P_a' is assumed, then:

$$P_b' = \frac{C \pi - \frac{1}{2} N_a P_a'}{\frac{1}{2} N_b}$$

and

$$\tan \alpha_a = \frac{P_a'}{P_b'} \quad \tan \alpha_b = \frac{P_b'}{P_a'}$$

The gear whose P' or α is larger will ordinarily be the driver, on account of the greater obliquity of the teeth.

4. Given N_a , N_b and C or D' .

See case "7" under III., considering $\gamma = 90^\circ$.

III.—AXIS AT ANY ANGLE (γ).

5. Given case "1," under II., then angles of spirals = $\frac{1}{2} \gamma$, for the same reason.

6. Analogous cases to "2" and "3," under II., may be worked out, when angles of axes = γ , but they have been

omitted, partly because the formulas are too cumbersome, and partly because they are to some extent covered by cases "5" and "7."

7. Given N_a , N_b and C , or one of the pitch diameters. We find the angles by a graphic method, which for all practical purposes is accurate enough; ro and vo are the axes of gears forming angle γ (see diagram, Fig. 10.) On these axes we lay off lines or and ov representing the ratio of the number of teeth (velocity ratio), so that $N_a:N_b::rs:sv$, and

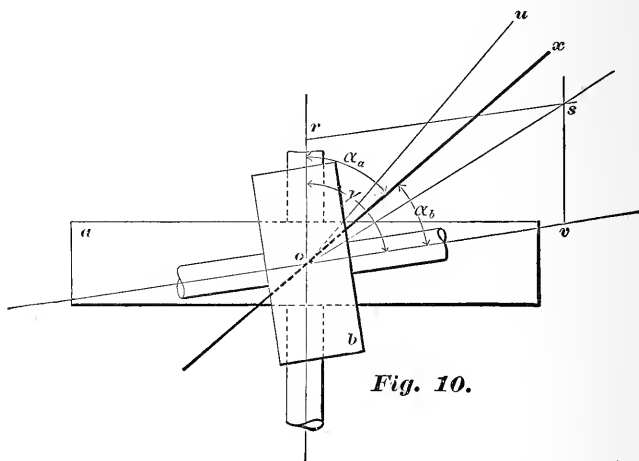


Fig. 10.

construct parallelogram $orsv$. Then, according to McCord,* the angles formed by the tangent so in the pitch contact o with the axes of the gears insures *the least amount of sliding*. In bisecting angle γ by tangent uo and using angles produced in this manner we *equally distribute the end thrust* on both shafts. Both methods have their advantages; to profit by both we select angles α_a and α_b , produced by tangent os , bisecting angle uos .

Thus we have when angles are found and C given,

$$P'^n = \frac{2 C \pi \cos \alpha_a \cos \alpha_b}{N_a \cos \alpha_b + N_b \cos \alpha_a}$$

and when D'_a given

$$P'^n = \frac{D'_a \pi \cos \alpha_a}{N_a} \quad \text{and}$$

$$D'_b = \frac{P'^n N_b}{\pi \cos \alpha_b}$$

*McCord, Kinematics, page 278.

GENERAL FORMULAS.

$$\gamma = \alpha_a + \alpha_b$$

$$P_a'^n = P_b'^n$$

$$D' = \frac{P' N}{\pi} \text{ or } = \frac{P'^n N}{\pi \cos \alpha}$$

$$D = D' + 2 s \text{ or } = D' + \frac{2}{P^n}$$

$$P' = \frac{D' \pi}{N} \text{ or } = \frac{P'^n}{\cos \alpha}$$

$$P'^n = P' \cos \alpha$$

$$P^n = \frac{\pi}{P'^n} \text{ (Pitch of cutter.)}$$

$$s = \frac{P'^n}{\pi} \text{ or } = \frac{1}{P^n}$$

$$t = \frac{P'^n}{2}$$

$$D'' + f = 2 s + \frac{t}{10}$$

$$T = \frac{N}{\cos^3 \alpha} \text{ (See Note 1.)}$$

$$L_1 = \frac{N P'}{\tan \alpha} \text{ or } \frac{N \pi}{P \tan \alpha} \text{ or for cases where axes are at right angles } \begin{cases} L_{1a} = N_a P'_b \\ L_{1b} = N_b P'_a \end{cases}$$

$$L_2 = \frac{10 W G_2}{S G_1} \text{ (See Note 2 and examples.)}$$

$$\begin{pmatrix} \cos 45^\circ = .70711 \\ \cos^3 45^\circ = .3535 \\ \tan 45^\circ = 1.000 \end{pmatrix}$$

NOTE 1.—Cutters of regular involute system.

Use No. 1 cutter for T from 135 up.	No. 5 cutter for T from 21 to 25
" 2 " " " 55 to 134	" 6 " " " 17 to 20
" 3 " " " 35 to 54	" 7 " " " 14 to 16
" 4 " " " 26 to 34	" 8 " " " 12 to 13

NOTE 2.—Gears used on spiral head of milling machines made by Brown & Sharpe Mfg. Co.

W =	number of teeth in	gear on	worm.
G ₁ =	"	1st	stud.
G ₂ =	"	2d	stud.
S =	"	"	screw.

Should a spiral head of different construction be used, the formula might not apply.

The following data are usually required in cutting spiral gears in a Universal Milling Machine, and it will be found convenient to arrange them in tabular form as follows :

	GEAR.	PINION.
No. of Teeth - - - - -		
Pitch Diameter - - - - -		
Outside Diameter - - - - -		
Circular Pitch - - - - -		
Angle of Teeth with Axis - - - - -		
Normal Circular Pitch - - - - -		
Pitch of Cutter - - - - -		
Addendum s - - - - -		
Thickness of Tooth t - - - - -		
Whole Depth $D'' + f$ - - - - -		
No. of Cutter - - - - -		
Exact Lead of Spiral - - - - -		
Approximate Lead of Spiral - - - - -		
Gears on Milling Machine to Cut Spiral		
Gear on Worm - - - - -		
1st Gear on Stud - - - - -		
2nd Gear on Stud - - - - -		
Gear on Screw - - - - -		

If the exact lead L_1 can be obtained by the gears at hand, L_1 will equal L_2 and we shall have from the formula

$$L_2 = \frac{10 W G_2}{S G_1}$$

$$\frac{L_1}{10} = \frac{W G_2}{S G_1} \quad (\text{for B. \& S. Milling Machine.})$$

Example I.

Required the gears for cutting a spiral of $2\frac{1}{2}''$ lead.

$\frac{2\frac{1}{2}}{10} = \frac{1}{4}$ factoring, in the most simple way, we have

$$\frac{1}{4} = \frac{1 \times 1}{2 \times 2} = \frac{1 \times 28}{56 \times 2} = \frac{32 \times 28}{56 \times 64} = \frac{W G_2}{S G_1}$$

Thus the gearing will be 32 T. on worm, 64 T. 1st. on stud, 28 T. 2nd on stud, and 56 T. on screw.

Trying these gears on the Milling Machine we find that they cannot be used, and as we have no other regular gears in the ratio of 2 to 1 that can be used we must try, by factoring, to get such ratios for the two pairs of gears as to be able to use the gears at hand, bearing in mind that the combined ratio must be $\frac{1}{4}$.

$$\frac{1}{4} = \frac{18}{72} = \frac{3 \times 6}{9 \times 8} = \frac{24 \times 6}{9 \times 64} = \frac{24 \times 48}{72 \times 64}$$

These gears are at hand and the combination can be used on the machine, giving the exact lead of $2\frac{1}{2}''$.

Example II.

Required the gears for cutting a spiral of 8.639" lead.

$8.639 = 8\frac{639}{1000}$; reducing, by continued fractions, to a smaller fraction of approximately the same value, as described on pages 50 and 51

$$\begin{array}{r}
 639 \overline{) 1000} \text{ (1} \\
 \underline{639} \\
 361 \overline{) 639} \text{ (1} \\
 \underline{361} \\
 278 \overline{) 361} \text{ (1} \\
 \underline{278} \\
 83 \overline{) 278} \text{ (3} \\
 \underline{249} \\
 29 \overline{) 83} \text{ (2} \\
 \underline{58} \\
 25 \overline{) 29} \text{ (1} \\
 \underline{25} \\
 4 \overline{) 25} \text{ (6} \\
 \underline{24} \\
 1 \overline{) 4} \text{ (4} \\
 \underline{4}
 \end{array}$$

$$\frac{1}{1} \quad \frac{1}{2} \quad \frac{1}{3} \quad \frac{3}{11} \quad \frac{2}{25} \quad \frac{1}{36} \quad \frac{6}{241} \quad \frac{4}{1000}$$

Selecting $\frac{16}{25}$ as an approximation near enough for our purpose, and in fact as near as we are likely to find gears for, we have for our lead $8\frac{16}{25}$. Applying the formula as in Example I.

$$\frac{8\frac{16}{25}}{10} = \frac{W G_2}{S G_1}$$

$$\frac{8\frac{16}{25}}{10} = \frac{216}{250} = \frac{108}{125} \text{ factoring we have}$$

$$\frac{9 \times 12}{25 \times 5} = \frac{9 \times 48}{100 \times 5} = \frac{72 \times 48}{100 \times 40} \text{ the gears required,}$$

these being regular gears furnished with the Milling Machine.

Proof:

$$\begin{aligned} \frac{72 \times 48 \times 10}{100 \times 40} &= 8.640 = L_2 \\ &\quad 8.639 = L_1 \\ &\quad .001'' \text{ error in lead.} \end{aligned}$$

In shops where much work is done in milling spirals it is desirable to have a full set of gears for the milling machine, from the smallest to the largest numbers of teeth that can be used. This makes it possible, in most cases, to get closer approximations than could be otherwise obtained, and often saves a great deal of figuring.

When the use of continued fractions does not bring a close enough approximation, one method to secure a closer result is to add to or subtract from the numerator and denominator of the fraction to be reduced, any numbers nearly in proportion to the given fraction, seeing that the numbers added or subtracted are such as to make the fraction reducible to lower terms. By a little ingenuity and patience extremely close approximations can generally be reached in this way.

Take, as an illustration, the fraction in Example II.

$$\frac{8\frac{639}{1000}}{10} = \frac{8639}{10000}$$

Adding 9 to the numerator and 10 to the denominator, these

being in about the same ratio to each other as the numerator and denominator of the fraction, we have

$$\frac{8639+9}{10000+10} = \frac{8648}{10010} = \frac{4324}{5005} = \frac{47 \times 92}{55 \times 91}$$

All of the gears in this case are special.

Applying the same proof as in Example II. we find that this train of gears will give a lead of 8.6393+, making an error of .0003" in the lead.

No doubt a much closer approximation even than this could be obtained by further trial.

Another method is to multiply both terms of the fraction by some number which will make one term of the fraction easily reducible, and adding one to or subtracting it from the other term to make it possible to reduce that also.

There is an element of uncertainty in both these methods, as we never feel sure that we have obtained the best combination; practical work, however, rarely requires accuracy beyond a point that can readily be reached.

The tables of prime numbers and factors, pages 116 to 149, will be found convenient in reducing and factoring fractions. These tables are condensed as much as possible and give all numbers from 1 to 10,200.

The table of leads, pages 154 to 171, gives all leads obtainable with the regular gears furnished with the Universal Milling Machines made by Brown & Sharpe Mfg. Co.

CHAPTER VI.

INTERNAL GEARING.

PART A.—INTERNAL SPUR GEARING.

A little consideration will show that a tooth of an internal or annular gear is the same as the space of a spur—external gear.

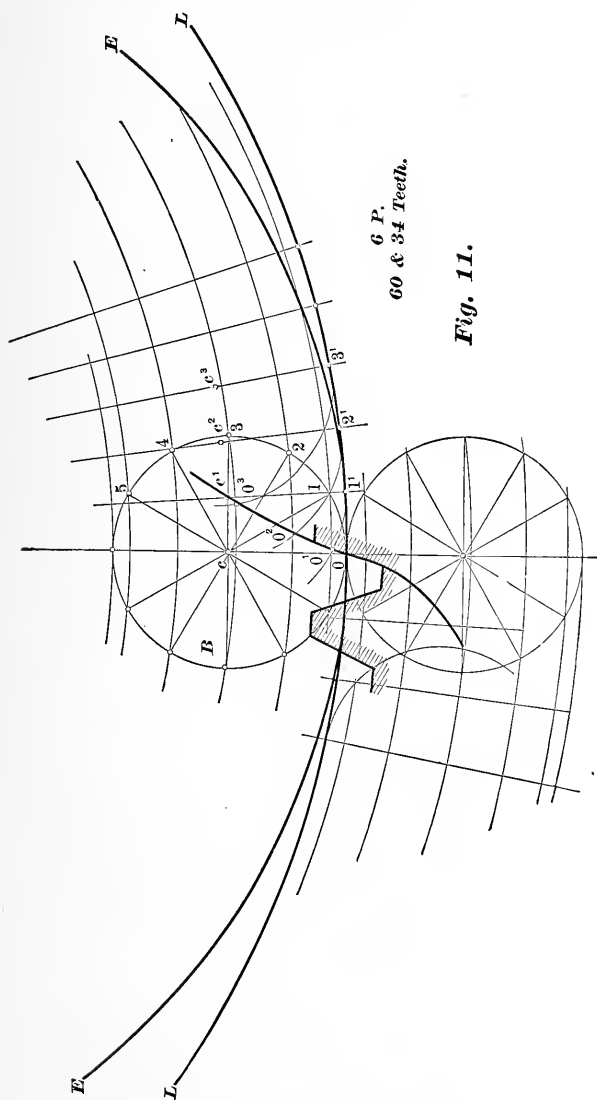
The epicycloidal form of tooth is preferable for internal gears, as there is less difficulty in overcoming the interferences. The involute form of tooth can be used by changing the pressure angle beyond the limit of interference. Special constructions are required when the difference between the number of teeth in gear and pinion is small.

In using the system of epicycloidal form of tooth in which the gear of 15 teeth has radial flanks, this difference must be at least 15 teeth, if the teeth have both faces and flanks. Gears fulfilling this condition present no difficulties. Their pitch diameters are found as in regular spur gears, and the inside diameter is equal to the pitch diameter, less twice the addendum.

If, however, this difference is less than 15, say 6, or 2, or 1, then we may construct the tooth outline (based on the epicycloidal system) in two different ways.

First Method.—To explain this method better, let us suppose the case as in Fig. 11, in which the difference between gear and pinion is more than 15 teeth. Here the point o of the describing circle B (the diameter of which in the best practice of the present day is equal to the pitch radius of a 15 tooth gear, of the same pitch as the gears in question) generates the cycloid o, o^1, o^2, o^3 , etc., when rolling on pitch circle LL of gear, forming the face of tooth; and when rolling on the outside of LL the flank of the tooth. In like manner is the face and flank of the pinion tooth produced by B rolling outside and inside of EE (pitch circle of pinion). A little study

of Fig. 11 (in which the face and flank of a gear tooth are produced) will show the describing circle B divided into 12



equal parts and circles laid through these points (1, 2, 3, etc.), concentric with L L. We now lay off on L L the distances 0-1, 1-2, 2-3, etc., of the circumference of B, and obtain points

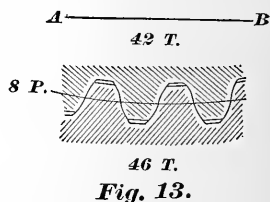
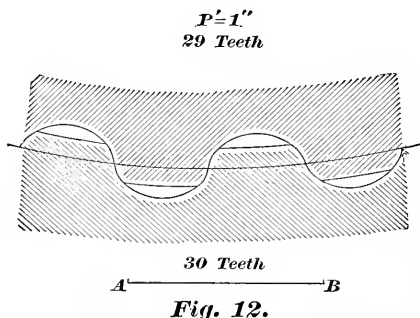
$1^1, 2^1, 3^1$, etc. [Ordinarily it is sufficient to use the chord.] It will now readily be seen that B in rolling on L L will successively come in contact with $1^1, 2^1, 3^1$, etc., c meanwhile moving to c^1, c^2, c^3 , etc. (points on radii through $1^1, 2^1, 3^1$, etc.), and the generating point o advancing to o^1, o^2, o^3 , etc., being the intersections of B with c^1, c^2, c^3 , etc., as centres and the circles laid through 1, 2, 3, etc. Points o, o^1, o^2, o^3 , etc., connected with a curve give the face of the tooth; in like manner the flank is obtained.

In this manner the form of tooth is obtained, when the difference of teeth in gear and pinion is less than 15, with the exception that the diameter of describing circle B

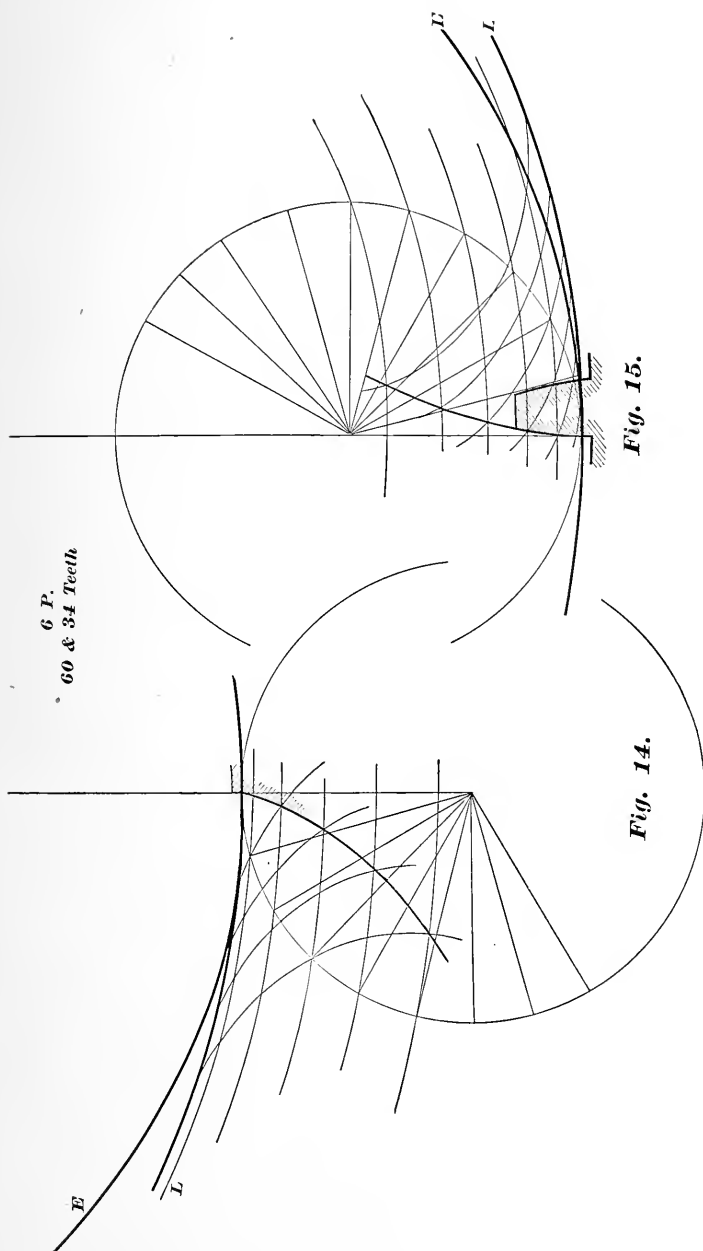
$$= \frac{1}{2} \left(\frac{Na - Nb}{P} \right)$$

where P = diametral pitch, Na and Nb number of teeth in gears.

The distances of the tooth above and below the pitch line as well as the thickness t are determined as in regular spur gears by the pitch, except when the difference in gear and pinion is very small, where we obtain a short tooth, as in Figs. 12 and 13. In such a case the height of tooth is arbitrary and only conditioned by the curve. In internal gears it is best to allow more clearance at bottom of tooth than in ordinary spur gears.



In a construction of this kind it is suggested to draw the tooth outline many times full size and reduce by photography. An equally multiplied line A B will help in reducing.



Second Method.—The difference between gear and pinion being very small, it is sometimes desirable to obtain a smooth action by avoiding what is termed the “friction of approaching action.”* This is done, the *pinion driving*, by giving gear only flanks, Fig. 14, and the *gear driving*, by giving gear only faces, Fig. 15. In both these cases we have but one describing circle, whose diameter is equal to the difference of the two pitch diameters. The construction of the curve is precisely the same as described under A. The describing circle has been divided into 24 parts simply for the sake of greater accuracy.

PART B.—INTERNAL BEVEL GEARS.

The pitch surfaces of bevel gears are cones whose apexes are at a common point, rolling upon each other. The tooth forms for any given pair of bevel gears are the same as for a pair of spur gears (of same pitch) whose pitch radii are equal to the respective apex distances of the normal cones (*i. e.*, cones whose elements are perpendicular upon the elements of the bevel gear pitch cones). (Compare Fig. 17, page 40.)

The same is true of internal bevel gears, with the modification that here one of the pitch cones rolls inside of the other. The spur gears to whose tooth forms the forms of the bevel gear teeth correspond, resolve themselves into internal spur gears (Fig. 16). The problem is now to be solved as indicated in the first part of this chapter.

* McCord, Kinematics, pages 107, 108.

8 P.
Gear 40 Teeth
Pinion 20 Teeth

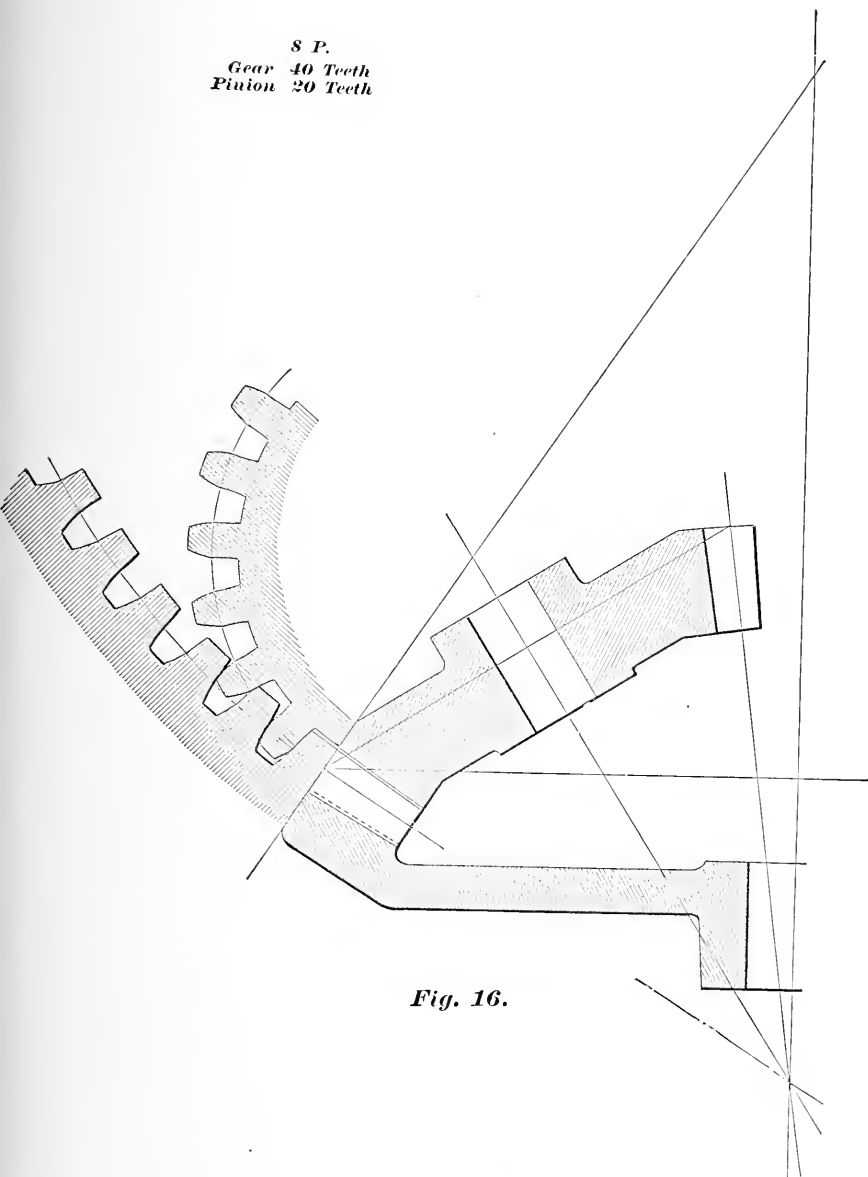
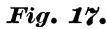


Fig. 16.

DIMENSIONS AND FORM FOR BEVEL GEAR CUTTERS.



In bevel gearing the curve is also dependent on the number of teeth in the mating gear; therefore gears with the same

number of teeth cannot always be cut with the same number of cutter. Thus, a 19 tooth pinion would be cut with a No. 4 cutter if it were to run with a 20 tooth gear, and with a No. 6 cutter if it were to run with a 50 tooth gear.

In order to find the curve to be used for gear and pinion, find the back cone radius, $a b$, for the gear and $b c$ for the pinion, and multiplying each by twice the diametral pitch, we obtain a number equivalent to the number of teeth for which cutters of proper curves may be selected.

For table, see Note 1, page 29.

The number of teeth for which the cutter should be selected can also be found by the following formulas:

N_a = number of teeth in gear.

N_b = number of teeth in pinion.

T_a = number of teeth to select cutter for gear.

T_b = number of teeth to select cutter for pinion.

α = centre angle of gear.

$$T_a = \frac{N_a}{N_b} \sqrt{N_a^2 - N_b^2}$$

$$T_b = \frac{N_b}{N_a} \sqrt{N_a^2 - N_b^2}$$

The above formulas apply only when axes of gears are at right angles. For axes at any angle the following formula can be used:

$$T = \frac{N}{\cos \alpha}$$

The tables, pages 86 and 87, are convenient for selecting cutters for bevel gears. They apply only when the axes are at right angles.

It is the practice to make bevel gear cutters .005" thinner than the space at the small end of the tooth. Theoretically the cutting angle (h) is equal to the pitch angle less the angle of bottom (or $h = a - B'$). Practically, however, better results are obtained by making $h = a - B$ (substituting angle of top for angle of bottom), and in calculating the depth at small end, to add the full clearance (f) to the obtained working depth, giving an equal amount of clearance at the large and small ends. This is done to obtain a tooth thinner at the top and more

curved. As the small end of the tooth determines the thickness of cutter, we shall have to find the tooth part values at the small end. These are obtained by multiplying the tooth part values at the large end by the constant,

$$1 - \frac{2 PF \sin \alpha}{N} \quad \text{where}$$

P = diametral pitch.

F = length of face of tooth measured on pitch line.

N = number of teeth in gear.

α = angle of edge or centre angle of gear.

EXAMPLE. Given gears 17 and 27 teeth, 12 pitch, $\frac{3}{8}$ " face.
Required tooth parts at small end of tooth.

$\alpha = 32^\circ 12'$ (obtained from table, page 78).

$\sin 32^\circ 12' = .53288$

$$1 - \frac{24 \times .375 \times .53288}{17} = .718 \text{ constant.}$$

$t = .1309$

$t' = .1309 \times .718 = .0940$

$s = .0833$

$s' = .0833 \times .718 = .0598$

$f = .0131$

$f = .0131$

$s + f = .0964$

$s' + f = .0598 + .0131 = .0729$

$D'' + f = .1798$

$D''' + f = .0729 + .0598 = .1327$

If in gears of more than 30 teeth the faces are proportionately long, we select a cutter whose curve corresponds to the midway section of the tooth. The curve of the cutter is found by the method explained in the first part of this chapter.

CHAPTER VIII.

THE INDEXING OF ANY WHOLE OR FRACTIONAL NUMBER—DIFFERENTIAL INDEXING.

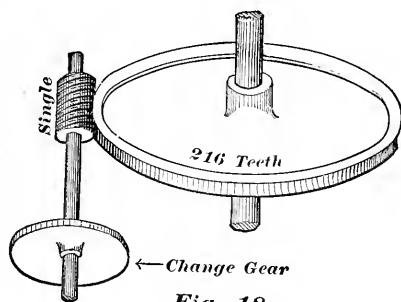


Fig. 18.

In indexing on a machine the question simply is : How many divisions of the machine index have to be advanced to advance a unit division of the number required. To which is the

$$\text{answer} = \frac{\text{divisions of machine index}}{\text{number to be indexed}}$$

Suppose the number of divisions in index wheel of machine to be 216.

EXAMPLE I.—Index 72.

Answer : $\frac{216}{72} = 3$ (3 turns of worm).

EXAMPLE II.—Index 123.

$$\frac{216}{123} = 1 + \frac{93}{123}$$

If now we should put on worm shaft a change gear having 123 teeth, give the worm shaft, Fig. 18, one turn, and in addition thereto advance 93 teeth of the change gear (to give the fractional turn), we would have indexed correctly one unit of the given number, and so solved the problem. Should we not have change gear 123 we may try those on hand. The question then is: How many teeth (χ) of the gear on hand (for instance 82) must we advance to obtain a result equal to the one when advancing 93 teeth of the 123 tooth gear? We have:

$$\frac{93}{123} = \frac{\chi}{82} \text{ where } \chi = 62$$

EXAMPLE III.—Index 365, change gear 147.

$$\frac{216}{365} = \frac{\chi}{147} \text{ where } \chi = 87 - \frac{3}{365}$$

Here 147 is the change gear on hand. In indexing for a unit of 365 we advance 87 teeth of our 147 tooth gear. It is evident that in so doing we advance too fast and will have indexed three teeth of our change gear too many when the circle is completed. To avoid having this error show in its total amount between the last and the first division, we can distribute the error by dropping one tooth at a time at three even intervals.

EXAMPLE IV.—Index 190.

$$\frac{216}{190} = 1 + \frac{26}{190} \quad \text{Change gear on hand 88 T}$$

$$\frac{26}{190} = \frac{\chi}{88} \text{ where } \chi = 12 + \frac{8}{190}$$

To distribute the error in this case we advance one additional tooth at a time of the change gear at eight even intervals.

EXAMPLE V.—Index 117.3913.

$$\frac{216}{117.3913} = 1 + \frac{986087}{1173913}$$

This example is in nowise different from the preceding ones, except that the fraction is expressed in large numbers. This fraction we can reduce to lower approximate values, which for practical purposes are accurate enough. This is done by the method of continued fractions. [For an explana-

tion of this method we refer to our "Practical Treatise on Gearing."]

$$\begin{array}{r}
 \frac{986087}{1173913} \\
 986087) 1173913 (1 \\
 \underline{986087} \\
 187826) 986087 (5 \\
 \underline{939130} \\
 46957) 187826 (3 \\
 \underline{140871} \\
 46955) 46957 (1 \\
 \underline{46955} \\
 2) 46955 (23477 \\
 \underline{46954} \\
 1) 2 (2 \\
 \underline{2} \\
 0
 \end{array}$$

$$\begin{array}{r}
 \frac{986087}{1173913} = \frac{1}{1 + \frac{1}{5 + \frac{1}{3 + \frac{1}{1 + \frac{1}{23477 + \frac{1}{2}}}}}}
 \end{array}$$

1	5	$c = 3$	1	23477	2
$a = 1$	$b = 5$	$d = 16$	$\frac{21}{25}$	493033	$\frac{986087}{1173913}$
$a^1 = 1$	$b^1 = 6$	$d^1 = 19$	$\frac{21}{25}$	586944	$\frac{986087}{1173913}$

NOTE.—Find the first two fractions by reduction $\frac{1}{1} = \frac{1}{1}$ and $\frac{1}{1 + \frac{1}{5}} = \frac{5}{6}$; the

others are then found by the rule $\begin{cases} b c + a = d \\ b^1 c + a^1 = d^1 \end{cases}$

The fraction $\frac{21}{25}$ is a good approximation; putting therefore a change gear of 25 teeth on worm shaft, we advance (beside the one full turn) 21 teeth to index our unit.

Of course, in using any but the correct fraction we have an error every time we index a division; so that when indexed around the whole circle, we have multiplied this error by the number of divisions.

In the present example this error is evidently equal to the difference between the correct and the approximate fraction used. Reducing both common fractions to decimal fractions we have:

$$\begin{array}{r}
 \frac{986087}{1173913} = .84000006 \\
 \frac{21}{25} = .84000000 \\
 \frac{.84000000}{.00000006} = \text{error in each division.}
 \end{array}$$

$.00000006 \times 117.3913 = .00000704348$ total error in complete circle. This error is expressed in parts of a unit division. (To find this error expressed in inches, multiply it by the distance between two divisions, measured on the circle.) In this case the approximate fraction being smaller than the correct one, in indexing the whole circle we fall short $.00000704348$ of a division.

EXAMPLE VI.—Index 15.708

$$\frac{216}{15.708} = 13 + \frac{11796}{15708}$$

$$\frac{11796}{15708} = \frac{983}{1309}$$

$$\begin{array}{r} 983 \overline{) 1309} (1 \\ \underline{983} \\ 326 \\ 983 \overline{) 326} (3 \\ \underline{978} \\ 5 \\ 326 \overline{) 5} (65 \\ \underline{30} \\ 26 \\ 25 \\ \underline{1} 5 (5 \\ \underline{5} \\ 0 \end{array}$$

$$\frac{983}{1309} = \frac{1}{1 + \frac{1}{3 + \frac{1}{65 + \frac{1}{5}}}}$$

$$\begin{array}{r} 1 \quad 3 \quad 65 \quad 5 \\ \hline 1 \quad 3 \quad 196 \quad 983 \\ \hline 1 \quad 4 \quad 261 \quad 1309 \end{array}$$

In using the approximation $\frac{1}{\frac{1}{2} + \frac{1}{8}}$ the error for each division (found as above) will be $.000002927$, for the whole circle $.0000460$. In this case, the approximation being larger than the correct fraction, we overreach the circle by the error.

DIFFERENTIAL INDEXING.

In differential indexing the spindle or driven shaft and the index plate are connected by a train of gearing which causes the plate to turn either in the same or opposite direction to that in which the crank is turned. The total movement of the crank at every indexing is, therefore, equal to its movement relative to the plate, *plus* the movement of the plate, when the plate revolves in the same direction as the crank, or *minus* the movement of the plate, when the plate revolves in the opposite direction to the crank.

N = number of divisions required.

H = number of holes in index plate.

nz = number of holes taken at each indexing.

V = ratio of gearing between index crank and spindle.

x = ratio of the train of gearing between the spindle and the index plate.

S = gear on spindle. } Drivers.
 G_1 = 1st gear on stud. }
 G_2 = 2d gear on stud. } Driven.
 W = gear on worm. }

$$x = \frac{HV - Nz}{H} \text{ if } HV \text{ is greater than } Nz.$$

$$x = \frac{Nz - HV}{H} \text{ if } HV \text{ is less than } Nz.$$

$$x = \frac{S}{W} \text{ (For simple gearing).}$$

$$x = \frac{S G_1}{G_2 W} \text{ (For compound gearing).}$$

As applied to the spiral head of a Milling Machine made by Brown & Sharpe Mfg. Co., V is equal to 40 and the index plates furnished have the following numbers of holes:—15, 16, 17, 18, 19, 20, 21, 23, 27, 29, 31, 33, 37, 39, 41, 43, 47, 49.

The gears furnished have the following numbers of teeth:—24 (2), 28, 32, 40, 44, 48, 56, 64, 72, 86, 100. These index plates and gears provide for the indexing of all divisions up to 382.

In selecting the index circle to be used, it is best to select one with a number having factors that are contained in the change gears on hand, for if H contains a factor not found in the gears, x cannot usually be obtained, unless the factor is cancelled by the difference between HV and Nz , or unless N contains the factor.

Multiplying the numbers of holes in the plates by 40 gives all the values of HV that can be obtained with the regular index plates. Following is a table of these products, which will be found convenient to use, especially when many combinations are to be obtained.

15 × 40	600	21 × 40	840	37 × 40	1480
16 × 40	640	23 × 40	920	39 × 40	1560
17 × 40	680	27 × 40	1080	41 × 40	1640
18 × 40	720	29 × 40	1160	43 × 40	1720
19 × 40	760	31 × 40	1240	47 × 40	1880
20 × 40	800	33 × 40	1320	49 × 40	1960

When HV is greater than Nz and gearing is simple, use 1 idler.

When HV is greater than Nz and gearing is compound, use no idlers.

When HV is less than Nz and gearing is simple, use 2 idlers.

When HV is less than Nz and gearing is compound, use 1 idler.

Select " n " so that the ratio of gearing will not exceed 6 : 1 on account of the excessive stress upon the gears.

EXAMPLE 1.

$N = 59$. Required H , n and x .

Assume $H = 33$ $n = 22$

$$\text{Then } x = \frac{(33 \times 40) - (59 \times 22)}{33} = \frac{22}{33} = \frac{2}{3}$$

We now select gears giving this ratio, as 32 and 48, the 32 being the gear on spindle and the 48 the gear on worm. HV is greater than Nz and the gearing is simple, requiring one idler.

EXAMPLE 2.

$N = 319$. Required H , n and x .

Assume $H = 29$ $n = 4$

$$\text{Then } x = \frac{(319 \times 4) - (29 \times 40)}{29} = \frac{116}{29} = \frac{4}{1}$$

When the ratio is not obtainable with simple gearing, try compound gearing. $\frac{4}{1}$ can be expressed as follows: $\frac{3 \times 4}{1 \times 3}$ or $\frac{72 \times 64}{24 \times 48}$, for which there are available gears.

HV is less than Nn and the gearing is compound, requiring one idler.

SPACING FOR QUARTER DEGREES.

EXAMPLE 3.

Required H , n and x for spacing $\frac{1}{4}$ degree or 1440 divisions.

Assume $H = 33$ $n = 1$

$$\text{Then } \frac{(1440 \times 1) - (33 \times 40)}{33} = \frac{120}{33} \text{ or } \frac{64 \times 100}{40 \times 44}$$

One idler is required.

ALIKANT OR FRACTIONAL SPACING.

EXAMPLE 4.

Required: A Vernier to read to $\frac{1}{12}$ degree or 5 minutes, the scale being divided to degrees.

Each Vernier space can equal $11\frac{1}{12}$ degree.

$\frac{11}{12} \times \frac{1}{360} = \frac{11}{4320}$ or $\frac{4320}{11}$ spaces in whole circle = $392\frac{8}{11}$ spaces.

Assume $H = 18$ $n = 2$.

$$\text{Then } \frac{(392\frac{8}{11} \times 2) - (18 \times 40)}{18} = \frac{720\frac{1}{11}}{18} =$$

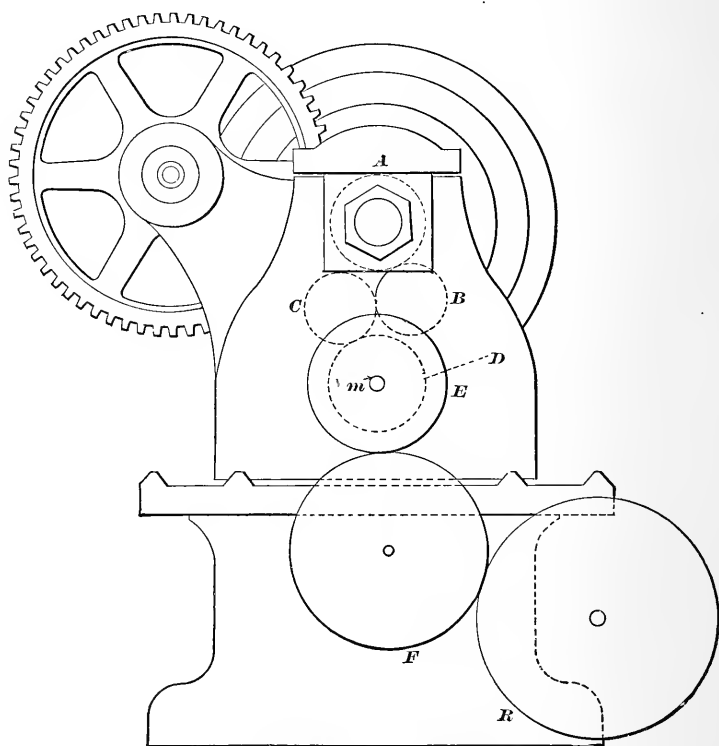
$$\frac{720}{11} \times \frac{1}{18} = \frac{40}{11} = \frac{64 \times 100}{40 \times 44}$$

One idler is required.

CHAPTER IX.

THE GEARING OF LATHES FOR SCREW CUTTING.

The problem of cutting a screw on a lathe resolves itself into connecting the lathe spindle with the lead screw by a train of gears in such a manner that the carriage (which is actuated by

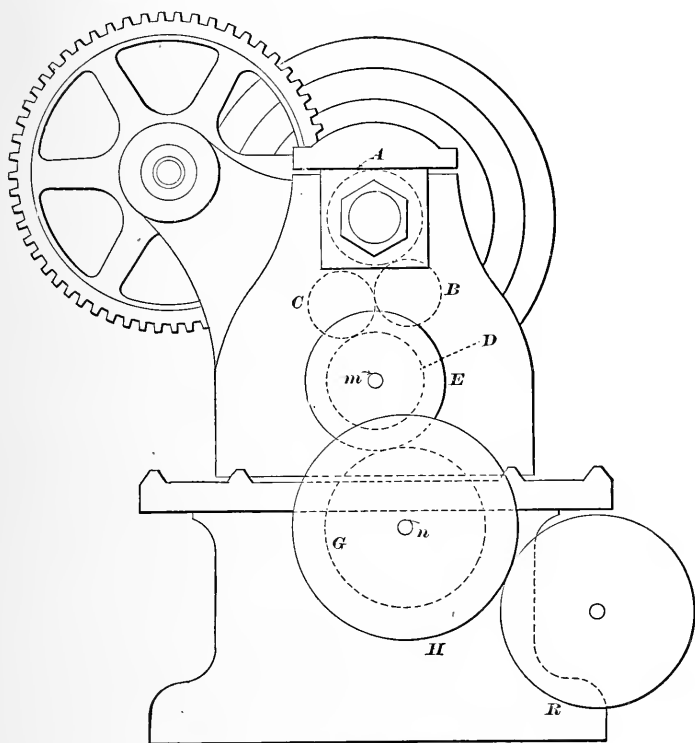


Simple Gearing.

Fig. 19.

the lead screw) advances just one inch, or some definite distance, while the lathe spindle makes a number of revolutions equal to the number of turns per inch or the definite distance to be cut.

The lead screw has, with the exception of a very few cases, always a single thread, and to advance the carriage one inch it therefore makes a number of revolutions equal to its number



Compound Gearing.

Fig. 20.

of threads per inch. Should the lead screw have double thread, it will, to accomplish the same result, make a number of revolutions equal to half its number of threads per inch. It follows that we must know in the first place the number of turns per inch of lead screw.

It ought to be clearly understood that one or more intermediate gears, which simply transmit the motion received from one gear to another, in no wise alter the ultimate ratio of a train of gearing. An even number of intermediate gears simply change the direction of rotation, an odd number do not alter it.

The gearing of a lathe to solve a problem in screw cutting can be accomplished by

A. Simple gearing.

B. Compound gearing.

Referring to the diagrams, Figs. 19 and 20, we have in Fig. 19 a case of simple, and in Fig. 20 a case of compound gearing.

In simple gearing the motion from gear E is transmitted either directly to gear R on lead screw or through the intermediate F. In compound gearing the motion of E is transmitted through two gears (G and H) keyed together, revolving on the same stud *n*, by which we can change the velocity ratio of the motion while transmitting it from E to R. With these four variables E, G, H, R, we are enabled to have a wider range of changes than in simple gearing.

B and C, being intermediate gears, are not to be considered. If, as is generally the case, gear A equals gear D, we disregard them both, simply remembering that gear E (being fast on same shaft with D) makes as many revolutions as the spindle. Sometimes gear D is twice as large as gear A, then, still considering gear E as making as many revolutions as the spindle, we deal with the lead screw as having twice as many turns per inch as it measures.

SIMPLE GEARING.

Let there be: the number of teeth in the different gears expressed by their respective letters, as per Fig. 19, and

s = turns per inch to be cut,

L = turns per inch of lead screw; then

$$1. \quad \frac{s}{L} = \frac{R}{E}$$

If now one of the two gears E and R is selected, the other will be :

$$R = \frac{s E}{L} ; \quad E = \frac{L R}{s}$$

2. The two gears may be found by making

$$\left. \begin{array}{l} R = p s \\ E = p L \end{array} \right\} \text{where } p \text{ may be any number.}$$

3. The above holds good when a fractional thread is to be cut, but if the fraction is expressed in large numbers, as, for instance, $s = 2.833$ ($2\frac{833}{1000}$), we first reduce this fraction ($\frac{833}{1000}$) to lower approximate values by the process of continued fraction (see pages 43 and 44).

$$\begin{array}{r} 833) 1000 (1 \\ \underline{833} \\ 167) 833 (4 \\ \underline{668} \\ 165) 167 (1 \\ \underline{165} \\ 2) 165 (82 \\ \underline{16} \\ 5 \\ \underline{4} \\ 1) 2 (2 \\ \underline{2} \\ 0 \end{array}$$

$$\begin{array}{r} 1 \quad 4 \quad 1 \quad 82 \quad 2 \\ \hline 1 \quad 4 \quad 5 \quad 414 \quad 833 \\ 1 \quad 5 \quad 6 \quad 497 \quad 1000 \end{array}$$

$$\frac{5}{6} = .833 \text{ (nearly) and } s = 2\frac{5}{6}$$

If in this case $L = 4$, and we select $E = 48$, then, since

$$R = \frac{s E}{L} \quad R = 34$$

COMPOUND GEARING.

4. In a lathe geared compound for cutting a screw the product of the drivers (E and H, Fig. 20) multiplied by the number of turns per inch to be cut must equal the product of the driven (G and R) multiplied by the number of turns per inch of lead screw. This is expressed by

$$E H s = G R L \text{ or } \frac{E H s}{G R L} = 1$$

If three of the gears E, H, G, R have been selected, the fourth one would be either

$$E = \frac{G R L}{H s} \quad \text{or}$$

$$H = \frac{G R L}{E s} \quad \text{or}$$

$$G = \frac{E H s}{R L} \quad \text{or}$$

$$R = \frac{E H s}{G L}$$

$$s = \frac{R G L}{E H} = L \left(\frac{R G}{L E H} \right)$$

If a fractional thread is to be cut, as under "3," we reduce the fraction to lower approximate values.

EXAMPLE.—Gear for 5.2327 turns per inch, lead screw is 6 turns per inch.

$$.2327 = \frac{2327}{10000}$$

$$\begin{array}{r}
 2327 \overline{) 10000} \quad (4 \\
 \underline{9308} \\
 692 \quad (3 \\
 \underline{2076} \\
 251 \quad (2 \\
 \underline{502} \\
 190 \quad (1 \\
 \underline{190} \\
 61 \quad (3 \\
 \underline{183} \\
 7 \quad (8 \\
 \underline{56} \\
 5 \quad (1 \\
 \underline{5} \\
 2 \quad (2 \\
 \underline{4} \\
 1 \quad (2 \\
 \underline{2} \\
 0
 \end{array}$$

$$\begin{array}{cccccccccc}
 4 & 3 & 2 & 1 & 3 & 8 & 1 & 2 & 2 \\
 \hline
 1 & 3 & 7 & 10 & 37 & 306 & 343 & 992 & 2327 \\
 4 & 13 & 30 & 43 & 159 & 1315 & 1474 & 4263 & 10000
 \end{array}$$

$$\frac{10}{43} = .2327 \text{ (nearly) and } 5.2327 = 5\frac{10}{43}$$

Selecting E = 43, H = 52, R = 50, and

$$G = \frac{E H s}{R L} \text{ we have } G = \frac{43 \times 52 \times 5\frac{10}{43}}{50 \times 6} = 39$$

5. The examples so far given all deal with single thread. The pitch of a screw is the distance from centre of one thread to the centre of the next. The lead of a screw is the advance for each complete revolution. In a single thread screw the pitch is equal to the lead, while in a double thread screw the pitch is equal to one-half the lead ; in a triple thread screw equal to one-third the lead, etc.

If we have to gear a lathe for a many-threaded screw (double, triple, quadruple, etc.), we simply ascertain the lead, and deal with the lead as we would with the pitch in a single thread screw, *i. e.*, we divide one inch by it, to obtain the number of threads for which we have to gear our lathe.

EXAMPLE.—Gear for double thread screw, lead = .4654. Number of turns per inch to be geared for is :

$$\frac{1}{\text{Lead}} = \frac{1}{.4654} = 2.1487$$

Lead screw is four turns per inch.

As in previous examples, we reduce the fraction $.1487 = \frac{1487}{10000}$ to lower approximate values by the process of continued fraction.

From the different values received in the usual way we select :

$$\frac{11}{74} = .1487 \text{ (nearly) and } 2.1487 = 2\frac{11}{74}$$

We have therefore :

$$\begin{aligned} s &= 2\frac{11}{74} \\ L &= 4 \\ \text{Selecting } \begin{cases} E = 74 \\ G = 30 \\ H = 40 \end{cases} \\ R &= \frac{E}{G} \frac{H}{L} s = \frac{74 \times 40 \times 2\frac{11}{74}}{30 \times 4} = 53 \end{aligned}$$

NOTE.—In using any but the original fraction we commit an error. This error can be found by reducing the approximate fraction used to a decimal fraction, and comparing it with the original fraction. In the above example the original fraction is

$$\frac{11}{74} = \frac{.1487}{.14864} \text{ and } \text{Error} = .00006 \text{ inch in lead.}$$

In cutting a multiple screw, after having cut one thread, the question arises how to move the thread tool the correct amount for cutting the next thread.

In cutting double, triple, etc., threads, if in simple or compound gearing the number of teeth in gear E is divisible by 2, 3, etc., we so divide the teeth; then leaving the carriage at rest we bring gear E out of mesh and move it forward one division, whereby the spindle will assume the correct position.

When E is not divisible we find how many turns (V) of gear R are made to each full turn of the spindle. Dividing this number by 2 for double, by 3 for triple thread, etc., we advance R so many turns and fractions of a turn, being careful to leave the spindle at rest.

For compound gearing :

$$V = \frac{E H}{G R}$$

When the gear D is twice as large as the gear A (as explained in fifth paragraph, page 52), the formula would be

$$V = \frac{E H}{2 G R}$$

If in simple gearing both E and R are not divisible, one remedy would be to gear the lathe compound; or the face-plate may be accurately divided in two, three or more slots, and all that is then necessary is to move the dog from one slot to another, the carriage remaining stationary.

COMPARATIVE SIZES OF GEAR TEETH.

INVOLUTE.

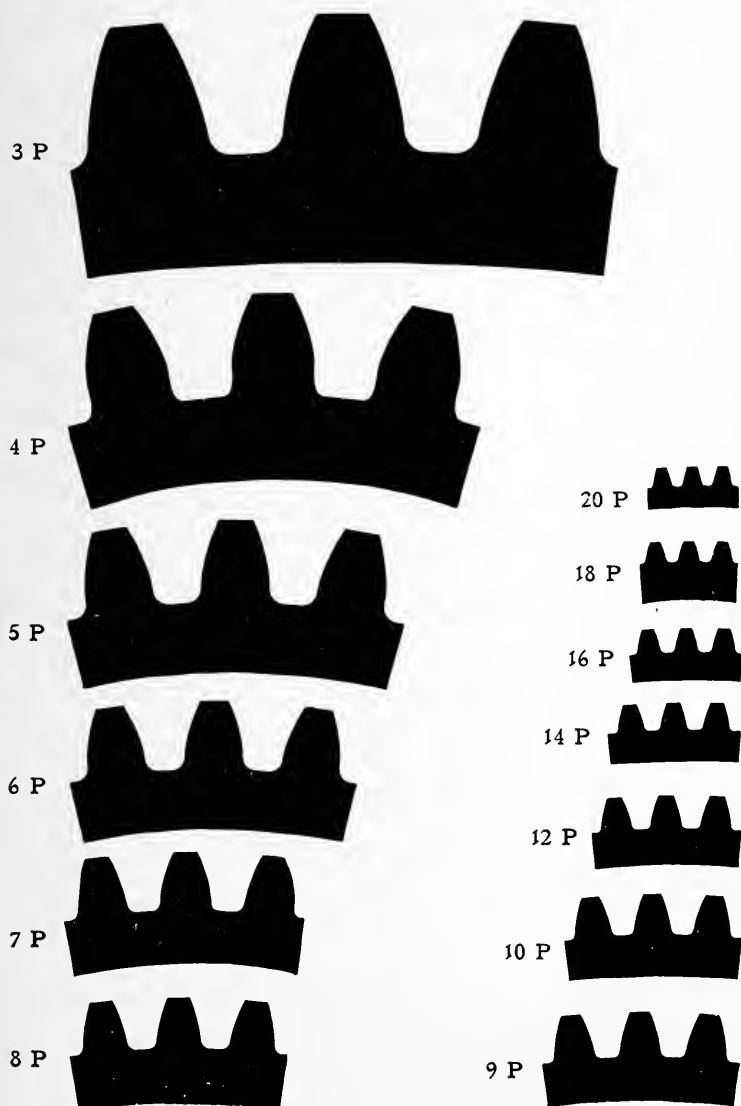
*Fig. 21.*

Table of Tooth Parts.

TABLE OF TOOTH PARTS.

CIRCULAR PITCH IN FIRST COLUMN.

Circular Pitch.	Threads or Teeth per inch Linear.	Diametral Pitch.	Thickness of Tooth on Pitch Line.	Addendum and Module.	Working Depth of Tooth.	Depth of Space below Pitch Line.	Whole Depth of Tooth.	Width of Thread-Tool at End.	Width of Thread at Top.
P'	$\frac{1''}{P'}$	P	t	s	D''	s+f	D''+f	P'X.31	P'X.335
2	$\frac{1}{2}$	1.5708	1.0000	.6366	1.2732	.7366	1.3732	.6200	.6700
$1\frac{7}{8}$	$\frac{8}{15}$	1.6755	.9375	.5968	1.1937	.6906	1.2874	.5813	.6281
$1\frac{3}{4}$	$\frac{4}{7}$	1.7952	.8750	.5570	1.1141	.6445	1.2016	.5425	.5863
$1\frac{5}{8}$	$\frac{8}{13}$	1.9333	.8125	.5173	1.0345	.5985	1.1158	.5038	.5444
$1\frac{1}{2}$	$\frac{2}{3}$	2.0944	.7500	.4775	.9549	.5525	1.0299	.4650	.5025
$1\frac{7}{16}$	$\frac{16}{23}$	2.1855	.7187	.4576	.9151	.5294	.9870	.4456	.4816
$1\frac{3}{8}$	$\frac{8}{11}$	2.2848	.6875	.4377	.8754	.5064	.9441	.4262	.4606
$1\frac{1}{3}$	$\frac{3}{4}$	2.3562	.6666	.4244	.8488	.4910	.9154	.4133	.4466
$1\frac{5}{16}$	$\frac{16}{21}$	2.3936	.6562	.4178	.8356	.4834	.9012	.4069	.4397
$1\frac{1}{4}$	$\frac{4}{5}$	2.5133	.6250	.3979	.7958	.4604	.8583	.3875	.4188
$1\frac{3}{16}$	$\frac{16}{19}$	2.6456	.5937	.3780	.7560	.4374	.8156	.3681	.3978
$1\frac{1}{8}$	$\frac{8}{9}$	2.7925	.5625	.3581	.7162	.4143	.7724	.3488	.3769
$1\frac{1}{16}$	$\frac{16}{17}$	2.9568	.5312	.3382	.6764	.3913	.7295	.3294	.3559
1	1	3.1416	.5000	.3183	.6366	.3683	.6866	.3100	.3350
$\frac{15}{16}$	$1\frac{1}{15}$	3.3510	.4687	.2984	.5968	.3453	.6437	.2906	.3141
$\frac{7}{8}$	$1\frac{1}{7}$	3.5904	.4375	.2785	.5570	.3223	.6007	.2713	.2931
$\frac{13}{16}$	$1\frac{3}{13}$	3.8666	.4062	.2586	.5173	.2993	.5579	.2519	.2722
$\frac{4}{5}$	$1\frac{1}{4}$	3.9270	.4000	.2546	.5092	.2946	.5492	.2480	.2680
$\frac{3}{4}$	$1\frac{1}{3}$	4.1888	.3750	.2387	.4775	.2762	.5150	.2325	.2513
$\frac{11}{16}$	$1\frac{5}{11}$	4.5696	.3437	.2189	.4377	.2532	.4720	.2131	.2303
$\frac{2}{3}$	$1\frac{1}{2}$	4.7124	.3333	.2122	.4244	.2455	.4577	.2066	.2233
$\frac{5}{8}$	$1\frac{3}{5}$	5.0265	.3125	.1989	.3979	.2301	.4291	.1938	.2094
$\frac{3}{5}$	$1\frac{2}{3}$	5.2360	.3000	.1910	.3820	.2210	.4120	.1860	.2010
$\frac{4}{7}$	$1\frac{3}{4}$	5.4978	.2857	.1819	.3638	.2105	.3923	.1771	.1914
$\frac{9}{16}$	$1\frac{7}{9}$	5.5851	.2812	.1790	.3581	.2071	.3862	.1744	.1884

TABLE OF TOOTH PARTS.—*Continued.*

CIRCULAR PITCH IN FIRST COLUMN.

Circular Pitch.	Threads or Teeth per inch Linear.	Diametral Pitch.	Thickness of Tooth on Pitch Line.	Addendum and Module.	Working Depth of Tooth.	Depth of Space below Pitch Line.	Whole Depth of Tooth.	Width of Thread-Tool at End.	Width of Thread at Top.
P'	$\frac{1''}{P'}$	P	t	$s \approx$	D''	$s+f$	D'+f.	P'X.31	P'X.335
$\frac{1}{2}$	2	6.2832	.2500	.1592	.3183	.1842	.3433	.1550	.1675
$\frac{4}{9}$	$2\frac{1}{4}$	7.0685	.2222	.1415	.2830	.1637	.3052	.1378	.1489
$\frac{7}{16}$	$2\frac{2}{7}$	7.1808	.2187	.1393	.2785	.1611	.3003	.1356	.1466
$\frac{3}{7}$	$2\frac{1}{3}$	7.3304	.2143	.1364	.2728	.1578	.2942	.1328	.1436
$\frac{2}{5}$	$2\frac{1}{2}$	7.8540	.2000	.1273	.2546	.1473	.2746	.1240	.1340
$\frac{3}{8}$	$2\frac{2}{3}$	8.3776	.1875	.1194	.2387	.1381	.2575	.1163	.1256
$\frac{4}{11}$	$2\frac{3}{4}$	8.6394	.1818	.1158	.2313	.1340	.2498	.1127	.1218
$\frac{1}{3}$	3	9.4248	.1666	.1061	.2122	.1228	.2289	.1033	.1117
$\frac{5}{16}$	$3\frac{1}{5}$	10.0531	.1562	.0995	.1989	.1151	.2146	.0969	.1047
$\frac{3}{10}$	$3\frac{1}{3}$	10.4719	.1500	.0955	.1910	.1105	.2060	.0930	.1005
$\frac{2}{7}$	$3\frac{1}{2}$	10.9956	.1429	.0909	.1819	.1052	.1962	.0886	.0957
$\frac{1}{4}$	4	12.5664	.1250	.0796	.1591	.0921	.1716	.0775	.0838
$\frac{2}{9}$	$4\frac{1}{2}$	14.1372	.1111	.0707	.1415	.0818	.1526	.0689	.0744
$\frac{1}{5}$	5	15.7080	.1000	.0637	.1273	.0737	.1373	.0620	.0670
$\frac{3}{16}$	$5\frac{1}{3}$	16.7552	.0937	.0597	.1194	.0690	.1287	.0581	.0628
$\frac{2}{11}$	$5\frac{1}{2}$	17.2788	.0909	.0579	.1158	.0670	.1249	.0564	.0609
$\frac{1}{6}$	6	18.8496	.0833	.0531	.1061	.0614	.1144	.0517	.0558
$\frac{2}{13}$	$6\frac{1}{2}$	20.4203	.0769	.0489	.0978	.0566	.1055	.0477	.0515
$\frac{1}{7}$	7	21.9911	.0714	.0455	.0910	.0526	.0981	.0443	.0479
$\frac{2}{15}$	$7\frac{1}{2}$	23.5619	.0666	.0425	.0850	.0492	.0917	.0414	.0446
$\frac{1}{8}$	8	25.1327	.0625	.0398	.0796	.0460	.0858	.0388	.0419
$\frac{1}{9}$	9	28.2743	.0555	.0354	.0707	.0409	.0763	.0344	.0372
$\frac{1}{10}$	10	31.4159	.0500	.0318	.0637	.0368	.0687	.0310	.0335
$\frac{1}{16}$	16	50.2655	.0312	.0199	.0398	.0230	.0429	.0194	.0209
$\frac{1}{20}$	20	62.8318	.0250	.0159	.0318	.0184	.0343	.0155	.0167

TABLE OF TOOTH PARTS.

DIAMETRAL PITCH IN FIRST COLUMN.

Diametral Pitch.	Circular Pitch.	Thickness of Tooth on Pitch Line.	Addendum and Module.	Working Depth of Tooth.	Depth of Space below Pitch Line.	Whole Depth of Tooth.
P	P'	<i>t</i>	<i>s</i>	D''	<i>s</i> + <i>f</i> .	D''+ <i>f</i> .
$\frac{1}{2}$	6.2832	3.1416	2.0000	4.0000	2.3142	4.3142
$\frac{3}{4}$	4.1888	2.0944	1.3333	2.6666	1.5428	2.8761
1	3.1416	1.5708	1.0000	2.0000	1.1571	2.1571
$1\frac{1}{4}$	2.5133	1.2566	.8000	1.6000	.9257	1.7257
$1\frac{1}{2}$	2.0944	1.0472	.6666	1.3333	.7714	1.4381
$1\frac{3}{4}$	1.7952	.8976	.5714	1.1429	.6612	1.2326
2	1.5708	.7854	.5000	1.0000	.5785	1.0785
$2\frac{1}{4}$	1.3963	.6981	.4444	.8888	.5143	.9587
$2\frac{1}{2}$	1.2566	.6283	.4000	.8000	.4628	.8628
$2\frac{3}{4}$	1.1424	.5712	.3636	.7273	.4208	.7844
3	1.0472	.5236	.3333	.6666	.3857	.7190
$3\frac{1}{2}$.8976	.4488	.2857	.5714	.3306	.6163
4	.7854	.3927	.2500	.5000	.2893	.5393
5	.6283	.3142	.2000	.4000	.2314	.4314
6	.5236	.2618	.1666	.3333	.1928	.3595
7	.4488	.2244	.1429	.2857	.1653	.3081
8	.3927	.1963	.1250	.2500	.1446	.2696
9	.3491	.1745	.1111	.2222	.1286	.2397
10	.3142	.1571	.1000	.2000	.1157	.2157
11	.2856	.1428	.0909	.1818	.1052	.1961
12	.2618	.1309	.0833	.1666	.0964	.1798
13	.2417	.1208	.0769	.1538	.0890	.1659
14	.2244	.1122	.0714	.1429	.0826	.1541

TABLE OF TOOTH PARTS—*Continued.*

DIAMETRAL PITCH IN FIRST COLUMN.

Diametral Pitch.	Circular Pitch.	Thickness of Tooth on Pitch Line.	Addendum and Module.	Working Depth of Tooth.	Depth of Space below Pitch Line.	Whole Depth of Tooth.
P.	P'.	<i>t.</i>	<i>s.</i>	D''.	<i>s+f.</i>	D''+f.
15	.2094	.1047	.0666	.1333	.0771	.1438
16	.1963	.0982	.0625	.1250	.0723	.1348
17	.1848	.0924	.0588	.1176	.0681	.1269
18	.1745	.0873	.0555	.1111	.0643	.1198
19	.1653	.0827	.0526	.1053	.0609	.1135
20	.1571	.0785	.0500	.1000	.0579	.1079
22	.1428	.0714	.0455	.0909	.0526	.0980
24	.1309	.0654	.0417	.0833	.0482	.0898
26	.1208	.0604	.0385	.0769	.0445	.0829
28	.1122	.0561	.0357	.0714	.0413	.0770
30	.1047	.0524	.0333	.0666	.0386	.0719
32	.0982	.0491	.0312	.0625	.0362	.0674
34	.0924	.0462	.0294	.0588	.0340	.0634
36	.0873	.0436	.0278	.0555	.0321	.0599
38	.0827	.0413	.0263	.0526	.0304	.0568
40	.0785	.0393	.0250	.0500	.0289	.0539
42	.0748	.0374	.0238	.0476	.0275	.0514
44	.0714	.0357	.0227	.0455	.0263	.0490
46	.0683	.0341	.0217	.0435	.0252	.0469
48	.0654	.0327	.0208	.0417	.0241	.0449
50	.0628	.0314	.0200	.0400	.0231	.0431
56	.0561	.0280	.0178	.0357	.0207	.0385
60	.0524	.0262	.0166	.0333	.0193	.0360

Tables Giving Chordal Thickness of
Gear Teeth and
Distance from Chord to Top of Tooth.

Tables Giving Chordal Thickness of Gear Teeth (t'') and Distance from Chord to Top of Tooth (s'').

The tables give the chordal thickness of teeth and the distance from the chord to the top of the tooth for gears of 1 diametral pitch and 1" circular pitch respectively.

To obtain t'' and s'' for any diametral pitch, divide the figures given in the table for 1 diametral pitch by the required diametral pitch.

EXAMPLE—Find t'' and s'' for a gear 5 diametral pitch, 23 teeth.

$$1.5696 \div 5 = .3139 = t''$$

$$1.0268 \div 5 = .2054 = s''$$

1 DIAMETRAL PITCH			
No. of Teeth.	No. of Cutter.	t''	s''
8		1.5607	1.0768
9		1.5628	1.0684
10		1.5643	1.0616
11		1.5654	1.0559
12	8	1.5663	1.0514
13	$7\frac{1}{2}$	1.5670	1.0474
14	7	1.5675	1.0440
15	$6\frac{1}{2}$	1.5679	1.0411
17	6	1.5686	1.0362
19	$5\frac{1}{2}$	1.5690	1.0324
21	5	1.5694	1.0294
23	$4\frac{1}{2}$	1.5696	1.0268
26	4	1.5698	1.0237
30	$3\frac{1}{2}$	1.5701	1.0208
35	3	1.5702	1.0176
42	$2\frac{1}{2}$	1.5704	1.0147
55	2	1.5706	1.0112
80	$1\frac{1}{2}$	1.5707	1.0077
135	1	1.5708	1.0046

To obtain t'' and s'' for any circular pitch, multiply the figures given in the table for 1" circular pitch by the required circular pitch.

EXAMPLE—Find t'' and s'' for a $\frac{3}{4}$ " circular pitch gear with 15 teeth.

$$.4991 \times \frac{3}{4} = .3743 = t''$$

$$.3314 \times \frac{3}{4} = .2486 = s''$$

1 CIRCULAR PITCH			
No. of Teeth.	No. of Cutter.	t''	s''
8		.4968	.3428
9		.4975	.3401
10		.4979	.3379
11		.4983	.3361
12	8	.4986	.3347
13	$7\frac{1}{2}$.4988	.3334
14	7	.4990	.3323
15	$6\frac{1}{2}$.4991	.3314
17	6	.4993	.3298
19	$5\frac{1}{2}$.4995	.3286
21	5	.4996	.3277
23	$4\frac{1}{2}$.4997	.3268
26	4	.4997	.3258
30	$3\frac{1}{2}$.4998	.3249
35	3	.4998	.3239
42	$2\frac{1}{2}$.4999	.3230
55	2	.5000	.3219
80	$1\frac{1}{2}$.5000	.3208
135	1	.5000	.3198

These tables are intended to be used for spur gears only. They can, however, be used for bevel gears by selecting t'' according to the number of teeth in the bevel gear and selecting s'' according to the number of teeth in a spur gear having a radius corresponding to the back cone radius of the bevel gear.

Table Giving Diameter Increments.

To use the following table for finding the outside diameters of Bevel Gears with axes at right angles, divide the figures given opposite the required numbers of teeth by the diametral pitch (P) and add to the pitch diameter, using the upper figure in the space for the gear and the lower for the pinion.

EXAMPLE.—Required, the outside diameters of a pair of bevel gears, 10 P, 35 T into 23 T. Referring to the table, the diameter increments are found to be for the gear 1.10 and for the pinion 1.67.

$1.10 \div 10 = .110$; 3.5 pitch diameter $+ .110 = 3.610$ outside diameter of gear.

$1.67 \div 10 = .167$; 2.3 pitch diameter $+ .167 = 2.467$ outside diameter of pinion.

DIAMETER INCREMENT.

GEAR

	72	71	70	69	68	67	66	65	64	63	62	61	60	59	58	57
PINION	.33 1.97	.33 1.97	.34 1.97	.34 1.97	.35 1.97	.35 1.97	.36 1.97	.36 1.97	.37 1.97	.37 1.96	.38 1.96	.39 1.96	.39 1.96	.40 1.96	.41 1.96	.41 1.96
	.36 1.97	.36 1.97	.37 1.97	.37 1.97	.38 1.96	.38 1.96	.39 1.96	.39 1.96	.40 1.96	.40 1.96	.41 1.96	.42 1.95	.42 1.95	.43 1.95	.44 1.95	.44 1.95
	.38 1.96	.39 1.96	.39 1.96	.40 1.96	.40 1.96	.41 1.96	.42 1.96	.42 1.95	.43 1.95	.43 1.95	.44 1.95	.45 1.95	.45 1.95	.46 1.95	.47 1.94	.48 1.94
	.41 1.96	.41 1.96	.42 1.95	.42 1.95	.43 1.95	.44 1.95	.44 1.95	.45 1.95	.46 1.95	.46 1.95	.47 1.94	.48 1.94	.48 1.94	.49 1.94	.50 1.94	.51 1.94
	.43 1.95	.44 1.95	.45 1.95	.45 1.95	.46 1.95	.46 1.95	.47 1.94	.48 1.94	.48 1.94	.49 1.94	.50 1.93	.51 1.93	.52 1.93	.52 1.93	.53 1.93	.54 1.93
	.46 1.95	.47 1.95	.47 1.94	.48 1.94	.48 1.94	.49 1.94	.50 1.93	.51 1.93	.51 1.93	.52 1.93	.53 1.93	.54 1.92	.55 1.92	.55 1.92	.56 1.92	.57 1.92
	.48 1.94	.49 1.94	.50 1.94	.50 1.93	.51 1.93	.52 1.93	.53 1.93	.53 1.93	.54 1.93	.55 1.92	.56 1.92	.57 1.92	.57 1.92	.58 1.91	.59 1.91	.60 1.91
	.51 1.93	.52 1.93	.52 1.93	.53 1.93	.54 1.93	.55 1.92	.55 1.92	.56 1.92	.57 1.92	.58 1.91	.59 1.91	.59 1.91	.60 1.91	.61 1.90	.62 1.90	.63 1.90
	.54 1.93	.54 1.93	.55 1.92	.55 1.92	.56 1.92	.57 1.92	.58 1.91	.59 1.91	.60 1.91	.61 1.91	.62 1.90	.63 1.90	.64 1.89	.65 1.89	.66 1.89	.66 1.89
	.56 1.92	.57 1.92	.57 1.92	.58 1.91	.59 1.91	.60 1.91	.61 1.91	.62 1.90	.63 1.90	.64 1.89	.65 1.89	.66 1.89	.67 1.88	.68 1.88	.68 1.88	.70 1.87
	.58 1.91	.59 1.91	.60 1.91	.61 1.91	.62 1.90	.63 1.90	.64 1.89	.65 1.89	.66 1.89	.67 1.88	.68 1.88	.69 1.88	.70 1.87	.71 1.87	.72 1.87	.72 1.87
	.61 1.91	.62 1.90	.62 1.90	.63 1.90	.64 1.89	.65 1.89	.66 1.89	.67 1.88	.68 1.88	.69 1.88	.70 1.87	.71 1.87	.72 1.87	.73 1.86	.74 1.86	.75 1.85
	.63 1.90	.64 1.89	.65 1.89	.66 1.89	.67 1.88	.68 1.88	.69 1.88	.70 1.87	.71 1.87	.72 1.87	.73 1.86	.74 1.86	.75 1.85	.76 1.85	.77 1.85	.78 1.84
	.66 1.89	.67 1.88	.67 1.88	.68 1.88	.69 1.87	.70 1.87	.71 1.87	.72 1.86	.73 1.86	.74 1.85	.75 1.85	.76 1.84	.77 1.84	.78 1.83	.79 1.83	.80 1.83
	.68 1.88	.69 1.88	.70 1.87	.71 1.87	.72 1.86	.73 1.86	.74 1.85	.75 1.85	.76 1.84	.77 1.84	.78 1.83	.79 1.83	.80 1.82	.81 1.82	.82 1.81	.83 1.81
	.70 1.87	.71 1.87	.72 1.86	.73 1.86	.74 1.85	.75 1.85	.76 1.84	.77 1.84	.78 1.83	.79 1.83	.80 1.82	.81 1.82	.82 1.81	.83 1.81	.84 1.80	.86 1.80
	.72 1.86	.73 1.86	.74 1.85	.75 1.85	.76 1.85	.77 1.84	.78 1.84	.79 1.83	.80 1.83	.81 1.82	.82 1.82	.83 1.81	.84 1.81	.85 1.80	.86 1.80	.88 1.80
	.75 1.86	.76 1.85	.77 1.85	.78 1.84	.78 1.84	.79 1.83	.80 1.83	.82 1.82	.83 1.82	.84 1.81	.85 1.81	.86 1.80	.87 1.80	.88 1.79	.89 1.79	.91 1.78
	.77 1.85	.78 1.84	.79 1.84	.80 1.83	.81 1.83	.82 1.83	.83 1.82	.84 1.82	.85 1.81	.86 1.81	.87 1.80	.88 1.79	.89 1.79	.91 1.78	.92 1.78	.93 1.77
	.79 1.84	.80 1.83	.81 1.83	.82 1.82	.83 1.82	.84 1.81	.85 1.81	.86 1.80	.87 1.79	.88 1.79	.89 1.78	.91 1.78	.92 1.77	.93 1.77	.94 1.76	.96 1.76
	.81 1.83	.82 1.82	.83 1.81	.84 1.81	.85 1.80	.86 1.80	.87 1.79	.88 1.79	.89 1.78	.91 1.78	.92 1.77	.93 1.77	.94 1.76	.95 1.76	.97 1.75	.98 1.74
	.83 1.82	.84 1.81	.85 1.81	.86 1.80	.87 1.80	.88 1.79	.89 1.79	.91 1.78	.92 1.78	.93 1.77	.94 1.77	.95 1.76	.96 1.75	.98 1.75	.99 1.74	1.00 1.73
	.85 1.81	.86 1.80	.87 1.80	.88 1.79	.89 1.79	.91 1.78	.92 1.78	.93 1.77	.94 1.77	.95 1.76	.96 1.75	.97 1.74	.99 1.73	1.00 1.73	1.01 1.72	1.02 1.71
	.87 1.80	.88 1.79	.89 1.79	.90 1.78	.92 1.78	.93 1.77	.94 1.77	.95 1.76	.96 1.75	.97 1.75	.98 1.74	1.00 1.73	1.01 1.73	1.02 1.72	1.03 1.71	1.05 1.70
	.89 1.79	.90 1.78	.91 1.78	.93 1.77	.94 1.77	.95 1.76	.96 1.75	.97 1.75	.98 1.74	.99 1.74	1.00 1.73	1.02 1.72	1.03 1.72	1.04 1.71	1.05 1.71	1.07 1.69
	.91 1.78	.92 1.77	.93 1.77	.95 1.76	.96 1.76	.97 1.75	.98 1.74	.99 1.74	1.00 1.73	1.01 1.72	1.03 1.72	1.04 1.71	1.05 1.71	1.06 1.70	1.08 1.69	1.09 1.68
	.93 1.77	.94 1.76	.95 1.76	.97 1.75	.98 1.75	.99 1.74	1.00 1.73	1.01 1.73	1.02 1.72	1.03 1.71	1.05 1.71	1.06 1.70	1.07 1.69	1.08 1.68	1.10 1.67	1.11 1.66
	.95 1.76	.96 1.75	.97 1.74	.98 1.74	.99 1.73	1.01 1.73	1.02 1.72	1.03 1.71	1.04 1.71	1.05 1.70	1.06 1.69	1.08 1.68	1.09 1.67	1.10 1.66	1.12 1.65	1.13 1.64
	.97 1.75	.97 1.74	.99 1.73	1.00 1.73	1.01 1.72	1.03 1.72	1.04 1.71	1.05 1.70	1.06 1.70	1.07 1.69	1.08 1.68	1.10 1.67	1.11 1.66	1.12 1.65	1.14 1.64	1.15 1.63
	.99 1.74	1.00 1.73	1.01 1.73	1.02 1.72	1.03 1.71	1.04 1.71	1.06 1.70	1.07 1.69	1.08 1.68	1.09 1.68	1.10 1.67	1.12 1.66	1.13 1.65	1.14 1.64	1.15 1.63	1.17 1.62
	1.01 1.73	1.02 1.72	1.03 1.72	1.04 1.71	1.05 1.70	1.06 1.69	1.07 1.68	1.09 1.68	1.10 1.67	1.11 1.66	1.12 1.66	1.13 1.65	1.15 1.64	1.16 1.63	1.17 1.62	1.19 1.61

For bevel gears with axes at right angles only.

DIAMETER INCREMENT.—(Continued.)

GEAR

PINION

	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42
12	.42 1.96	.43 1.95	.43 1.95	.44 1.95	.45 1.95	.46 1.95	.47 1.94	.48 1.94	.48 1.94	.49 1.94	.50 1.94	.52 1.93	.53 1.93	.54 1.93	.55 1.92
13	.45 1.95	.46 1.95	.47 1.94	.48 1.94	.48 1.94	.49 1.94	.50 1.94	.51 1.93	.52 1.93	.53 1.93	.54 1.92	.56 1.92	.57 1.92	.58 1.91	.59 1.91
14	.48 1.94	.49 1.94	.50 1.94	.51 1.93	.52 1.93	.53 1.93	.54 1.93	.55 1.92	.56 1.92	.57 1.92	.58 1.91	.59 1.91	.61 1.91	.62 1.90	.63 1.90
15	.52 1.93	.53 1.93	.54 1.93	.54 1.92	.55 1.92	.56 1.92	.57 1.92	.59 1.91	.60 1.91	.61 1.91	.62 1.90	.63 1.90	.65 1.89	.66 1.89	.67 1.88
16	.55 1.92	.56 1.92	.57 1.92	.58 1.91	.59 1.91	.60 1.91	.61 1.90	.62 1.90	.63 1.90	.64 1.89	.66 1.89	.67 1.88	.68 1.88	.70 1.87	.71 1.87
17	.58 1.91	.59 1.91	.60 1.91	.61 1.90	.62 1.90	.63 1.90	.64 1.89	.66 1.89	.67 1.89	.68 1.88	.69 1.88	.71 1.87	.72 1.87	.74 1.86	.75 1.85
18	.61 1.90	.62 1.90	.63 1.90	.64 1.89	.65 1.89	.67 1.89	.68 1.88	.69 1.88	.70 1.87	.72 1.87	.73 1.86	.74 1.86	.76 1.85	.77 1.84	.79 1.84
19	.64 1.89	.65 1.89	.66 1.89	.67 1.88	.69 1.88	.70 1.87	.71 1.87	.72 1.86	.74 1.86	.75 1.85	.76 1.85	.78 1.84	.79 1.84	.81 1.83	.82 1.82
20	.67 1.88	.68 1.88	.69 1.88	.71 1.87	.72 1.87	.73 1.86	.74 1.86	.76 1.85	.77 1.85	.78 1.84	.80 1.83	.81 1.83	.83 1.82	.84 1.81	.86 1.81
21	.70 1.87	.71 1.87	.72 1.86	.74 1.86	.75 1.85	.76 1.85	.77 1.84	.79 1.84	.80 1.83	.82 1.83	.83 1.82	.85 1.81	.86 1.80	.88 1.80	.89 1.79
22	.73 1.86	.74 1.86	.75 1.85	.77 1.85	.78 1.84	.79 1.84	.81 1.83	.82 1.82	.83 1.82	.85 1.81	.86 1.80	.88 1.80	.89 1.79	.91 1.78	.93 1.77
23	.76 1.85	.77 1.85	.78 1.84	.80 1.83	.81 1.83	.82 1.82	.84 1.82	.85 1.81	.86 1.80	.88 1.80	.89 1.79	.91 1.78	.93 1.77	.94 1.76	.96 1.75
24	.79 1.84	.80 1.83	.81 1.83	.83 1.82	.84 1.82	.85 1.81	.87 1.80	.88 1.79	.89 1.78	.91 1.78	.93 1.77	.94 1.76	.96 1.76	.97 1.75	.99 1.74
25	.82 1.83	.83 1.82	.84 1.81	.85 1.81	.87 1.80	.88 1.80	.89 1.79	.91 1.78	.92 1.77	.94 1.77	.95 1.76	.97 1.75	.99 1.74	1.01 1.73	1.02 1.72
26	.84 1.81	.85 1.81	.87 1.80	.88 1.80	.89 1.79	.91 1.78	.92 1.77	.94 1.77	.95 1.76	.97 1.75	.98 1.74	1.00 1.73	1.01 1.72	1.03 1.71	1.05 1.70
27	.87 1.80	.88 1.80	.89 1.79	.91 1.78	.92 1.78	.94 1.77	.95 1.76	.97 1.75	.98 1.74	1.00 1.73	1.01 1.72	1.03 1.71	1.05 1.70	1.06 1.69	1.08 1.68
28	.89 1.79	.91 1.78	.92 1.78	.93 1.77	.95 1.76	.96 1.75	.98 1.75	.99 1.74	1.01 1.73	1.02 1.72	1.04 1.71	1.06 1.70	1.07 1.69	1.09 1.68	1.11 1.66
29	.92 1.78	.93 1.77	.95 1.76	.96 1.75	.97 1.75	.99 1.74	.99 1.73	1.00 1.72	1.02 1.71	1.03 1.70	1.05 1.69	1.08 1.68	1.10 1.67	1.12 1.66	1.14 1.65
30	.94 1.76	.96 1.76	.98 1.74	.99 1.74	1.00 1.73	1.01 1.72	1.01 1.71	1.03 1.71	1.04 1.70	1.06 1.69	1.08 1.68	1.09 1.66	1.11 1.65	1.13 1.64	1.16 1.63
31	.97 1.75	.98 1.74	1.00 1.73	1.01 1.72	1.02 1.72	1.04 1.71	1.05 1.70	1.07 1.69	1.09 1.68	1.10 1.67	1.12 1.66	1.13 1.65	1.15 1.63	1.17 1.62	1.19 1.61
32	.99 1.74	1.01 1.73	1.02 1.72	1.03 1.71	1.04 1.71	1.06 1.69	1.08 1.68	1.09 1.67	1.11 1.66	1.13 1.65	1.14 1.64	1.16 1.63	1.18 1.62	1.19 1.60	1.21 1.59
33	1.02 1.72	1.03 1.71	1.04 1.71	1.06 1.70	1.08 1.69	1.09 1.68	1.10 1.67	1.12 1.66	1.13 1.65	1.15 1.64	1.17 1.63	1.18 1.61	1.20 1.60	1.22 1.59	1.24 1.57
34	1.04 1.71	1.05 1.70	1.07 1.69	1.08 1.68	1.09 1.67	1.11 1.66	1.12 1.65	1.14 1.64	1.16 1.63	1.17 1.62	1.19 1.61	1.21 1.59	1.22 1.58	1.24 1.57	1.26 1.55
35	1.06 1.70	1.07 1.69	1.09 1.68	1.10 1.67	1.12 1.66	1.13 1.65	1.15 1.64	1.17 1.63	1.18 1.62	1.19 1.60	1.21 1.59	1.23 1.58	1.25 1.57	1.26 1.55	1.28 1.54
36	1.08 1.68	1.10 1.67	1.11 1.66	1.12 1.65	1.14 1.64	1.15 1.63	1.17 1.62	1.18 1.61	1.19 1.60	1.21 1.59	1.23 1.57	1.25 1.56	1.27 1.55	1.28 1.53	1.30 1.52
37	1.10 1.67	1.12 1.66	1.13 1.65	1.14 1.64	1.16 1.63	1.17 1.62	1.19 1.61	1.21 1.60	1.22 1.58	1.24 1.57	1.25 1.56	1.27 1.55	1.29 1.53	1.30 1.52	1.32 1.50
38	1.12 1.66	1.14 1.65	1.15 1.64	1.16 1.63	1.18 1.61	1.20 1.60	1.21 1.59	1.23 1.58	1.24 1.57	1.26 1.56	1.27 1.54	1.29 1.53	1.31 1.51	1.32 1.50	1.34 1.48
39	1.14 1.64	1.16 1.63	1.17 1.62	1.19 1.61	1.20 1.60	1.21 1.59	1.23 1.58	1.25 1.57	1.26 1.55	1.28 1.54	1.29 1.53	1.31 1.51	1.33 1.50	1.34 1.48	1.36 1.47
40	1.16 1.63	1.18 1.62	1.19 1.61	1.20 1.59	1.22 1.57	1.23 1.56	1.25 1.55	1.26 1.54	1.28 1.52	1.29 1.51	1.31 1.49	1.33 1.48	1.35 1.46	1.36 1.45	1.38 1.44
41	1.18 1.61	1.20 1.60	1.21 1.59	1.22 1.58	1.24 1.57	1.25 1.56	1.27 1.55	1.28 1.53	1.30 1.52	1.31 1.51	1.33 1.49	1.35 1.48	1.36 1.46	1.38 1.45	1.40 1.43
42	1.20 1.60	1.21 1.59	1.23 1.58	1.24 1.57	1.26 1.56	1.27 1.54	1.29 1.53	1.30 1.52	1.32 1.51	1.33 1.49	1.35 1.48	1.36 1.46	1.38 1.45	1.40 1.43	1.41 1.41

For bevel gears with axes at right angles only.

DIAMETER INCREMENT.—(Continued.)

GEAR

	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27
PINION	.56 1.92	.58 1.92	.59 1.91	.61 1.91	.63 1.90	.65 1.90	.65 1.89	.67 1.88	.68 1.88	.70 1.87	.72 1.87	.74 1.86	.76 1.85	.79 1.84	.81 1.83
	.60 1.91	.61 1.90	.63 1.90	.65 1.89	.66 1.89	.68 1.88	.70 1.87	.71 1.87	.73 1.86	.75 1.85	.77 1.84	.80 1.83	.82 1.82	.84 1.81	.87 1.80
	.65 1.89	.66 1.89	.67 1.88	.69 1.88	.71 1.87	.72 1.86	.74 1.86	.76 1.85	.78 1.84	.80 1.83	.82 1.82	.85 1.81	.87 1.80	.89 1.79	.92 1.78
	.69 1.88	.70 1.87	.72 1.87	.74 1.86	.75 1.85	.77 1.85	.79 1.84	.81 1.83	.83 1.82	.85 1.81	.87 1.80	.89 1.79	.92 1.78	.94 1.77	.97 1.75
	.73 1.86	.74 1.86	.76 1.85	.77 1.85	.79 1.84	.81 1.83	.83 1.82	.85 1.81	.88 1.80	.89 1.79	.91 1.77	.94 1.75	.97 1.75	.99 1.74	1.02 1.72
	.77 1.85	.78 1.84	.79 1.83	.81 1.83	.83 1.82	.86 1.81	.88 1.80	.89 1.79	.91 1.77	.94 1.76	.96 1.75	.99 1.74	1.01 1.73	1.04 1.71	1.07 1.69
	.80 1.83	.82 1.82	.84 1.81	.86 1.81	.88 1.80	.89 1.79	.91 1.78	.93 1.77	.94 1.76	.98 1.74	1.01 1.73	1.03 1.72	1.06 1.70	1.08 1.68	1.11 1.66
	.84 1.81	.86 1.81	.88 1.80	.89 1.79	.91 1.78	.95 1.77	.97 1.76	.99 1.75	.99 1.73	1.02 1.72	1.04 1.70	1.07 1.69	1.10 1.67	1.12 1.66	1.15 1.64
	.88 1.80	.89 1.79	.91 1.78	.93 1.77	.95 1.76	.97 1.75	.99 1.74	1.01 1.72	1.04 1.71	1.06 1.70	1.08 1.68	1.11 1.66	1.14 1.64	1.16 1.63	1.19 1.61
	.91 1.78	.93 1.77	.94 1.76	.97 1.75	.99 1.74	1.01 1.73	1.03 1.72	1.05 1.70	1.07 1.69	1.10 1.67	1.12 1.65	1.14 1.64	1.17 1.62	1.20 1.60	1.23 1.58
	.95 1.76	.96 1.75	.98 1.74	1.00 1.73	1.02 1.72	1.04 1.71	1.06 1.69	1.09 1.68	1.11 1.66	1.13 1.65	1.16 1.63	1.18 1.61	1.21 1.59	1.24 1.57	1.26 1.55
	.98 1.74	1.00 1.73	1.01 1.72	1.04 1.71	1.06 1.70	1.08 1.68	1.10 1.67	1.12 1.66	1.14 1.64	1.17 1.62	1.19 1.61	1.21 1.59	1.24 1.57	1.27 1.55	1.30 1.52
	1.01 1.72	1.03 1.71	1.05 1.70	1.07 1.69	1.08 1.68	1.11 1.66	1.13 1.65	1.15 1.63	1.17 1.62	1.20 1.60	1.23 1.58	1.25 1.56	1.28 1.54	1.30 1.52	1.33 1.49
	1.04 1.71	1.06 1.70	1.08 1.68	1.10 1.67	1.12 1.65	1.14 1.64	1.16 1.63	1.18 1.61	1.20 1.59	1.23 1.58	1.26 1.56	1.28 1.54	1.31 1.52	1.33 1.49	1.36 1.47
	1.07 1.69	1.09 1.68	1.11 1.66	1.13 1.65	1.15 1.64	1.17 1.62	1.19 1.61	1.21 1.59	1.24 1.57	1.26 1.55	1.28 1.53	1.31 1.51	1.34 1.49	1.36 1.47	1.39 1.44
	1.10 1.67	1.12 1.66	1.14 1.64	1.15 1.63	1.18 1.62	1.20 1.60	1.22 1.58	1.24 1.57	1.27 1.54	1.29 1.53	1.31 1.51	1.34 1.49	1.36 1.46	1.39 1.44	1.41 1.41
	1.13 1.65	1.14 1.64	1.16 1.62	1.19 1.61	1.21 1.59	1.23 1.58	1.25 1.56	1.27 1.54	1.29 1.53	1.32 1.51	1.34 1.48	1.36 1.46	1.39 1.44	1.41 1.41	
	1.15 1.63	1.17 1.62	1.19 1.60	1.21 1.59	1.23 1.57	1.26 1.56	1.28 1.54	1.30 1.52	1.32 1.50	1.34 1.48	1.37 1.46	1.39 1.44	1.41 1.41		
	1.18 1.61	1.20 1.60	1.22 1.59	1.24 1.57	1.26 1.55	1.28 1.54	1.30 1.52	1.32 1.50	1.34 1.48	1.37 1.46	1.39 1.44	1.41 1.41			
	1.21 1.59	1.23 1.58	1.25 1.57	1.26 1.55	1.28 1.53	1.31 1.51	1.33 1.50	1.35 1.48	1.37 1.46	1.39 1.44	1.41 1.41				
	1.23 1.58	1.25 1.56	1.27 1.54	1.29 1.53	1.31 1.51	1.33 1.50	1.35 1.48	1.37 1.46	1.39 1.44	1.41 1.41					
	1.25 1.56	1.27 1.54	1.29 1.53	1.31 1.51	1.33 1.49	1.35 1.48	1.37 1.45	1.39 1.43	1.41 1.41						
	1.28 1.54	1.30 1.52	1.31 1.51	1.33 1.49	1.35 1.48	1.37 1.45	1.39 1.43	1.41 1.41							
	1.30 1.52	1.32 1.50	1.34 1.49	1.35 1.48	1.38 1.45	1.39 1.44	1.41 1.41								
	1.32 1.50	1.34 1.49	1.36 1.47	1.38 1.45	1.40 1.43	1.41 1.41									
	1.34 1.49	1.36 1.47	1.38 1.45	1.40 1.43	1.41 1.41										
	1.36 1.47	1.38 1.45	1.40 1.43	1.41 1.41											
	1.38 1.45	1.40 1.43	1.41 1.41												
	1.40 1.43	1.41 1.41													
	1.41 1.41														

For bevel gears with axes at right angles only.

DIAMETER INCREMENT.—(Continued.)

		GEAR														
		26	25	24	23	22	21	20	19	18	17	16	15	14	13	12
PINION	12	.84 1.82	.87 1.80	.89 1.79	.93 1.77	.96 1.76	.99 1.74	1.03 1.71	1.07 1.69	1.11 1.66	1.15 1.63	1.20 1.60	1.25 1.56	1.30 1.52	1.36 1.47	1.41 1.41
	13	.89 1.79	.92 1.77	.95 1.76	.98 1.74	1.02 1.72	1.05 1.70	1.09 1.68	1.13 1.65	1.17 1.62	1.21 1.59	1.26 1.55	1.31 1.51	1.36 1.47	1.41 1.41	
	14	.95 1.76	.98 1.75	1.01 1.73	1.04 1.71	1.07 1.69	1.11 1.66	1.15 1.64	1.19 1.61	1.23 1.58	1.27 1.54	1.32 1.50	1.36 1.46	1.41 1.41		
	15	1.00 1.73	1.03 1.71	1.06 1.70	1.09 1.68	1.13 1.65	1.16 1.63	1.20 1.60	1.24 1.57	1.28 1.54	1.32 1.50	1.37 1.46	1.41 1.41			
	16	1.05 1.70	1.08 1.68	1.11 1.66	1.14 1.64	1.18 1.62	1.21 1.59	1.25 1.56	1.29 1.53	1.33 1.49	1.37 1.46	1.41 1.41				
	17	1.09 1.67	1.12 1.65	1.16 1.63	1.19 1.61	1.22 1.58	1.26 1.55	1.30 1.52	1.33 1.49	1.37 1.45	1.41 1.41					
	18	1.14 1.64	1.17 1.62	1.20 1.60	1.23 1.57	1.27 1.55	1.30 1.52	1.34 1.49	1.38 1.45	1.41 1.41						
	19	1.18 1.61	1.21 1.59	1.24 1.57	1.27 1.54	1.31 1.51	1.34 1.48	1.38 1.45	1.41 1.41							
	20	1.22 1.59	1.25 1.56	1.28 1.54	1.31 1.51	1.35 1.48	1.38 1.45	1.41 1.41								
	21	1.26 1.56	1.29 1.53	1.32 1.50	1.35 1.48	1.38 1.45	1.41 1.41									
	22	1.29 1.53	1.32 1.50	1.35 1.47	1.38 1.45	1.41 1.41										
	23	1.33 1.50	1.35 1.47	1.38 1.44	1.41 1.41											
	24	1.36 1.47	1.39 1.44	1.41 1.41												
	25	1.39 1.44	1.41 1.41													
	26	1.41 1.41														

For bevel gears with axes at right angles only.



TABLES FOR ANGLES OF EDGE AND ANGLES OF FACE.

The following tables have been computed for convenience in calculating data for bevel gears with axes at right angle. They *do not* hold good for bevel gears with axes at any other angle.

To use the tables the number of teeth in gear and pinion must be known.

Having located the number of teeth in the gear on the horizontal line of figures at the top of the table, and the number of teeth in the pinion on the vertical line of figures on the left-hand side, we follow the two columns to the square formed by their intersections.

The two angles found in the same square are the respective angles for gear and pinion. The tables are so arranged that the angle belonging to the gear is always placed above the angle for the pinion.

The cutting angle for a gear or pinion is equal to the angle of face of its mate as given in the following tables.

ANGLE OF EDGE.

GEAR

	72	71	70	69	68	67	66	65	64	63	62	61	60	59	58	57
12	80°33' 9°27'	80°25' 9°35'	80°16' 9°44'	80°8' 9°52'	79°59' 10°1'	79°51' 10°9'	79°42' 10°18'	79°32' 10°28'	79°23' 10°37'	79°13' 10°47'	79°3' 10°57'	78°52' 11°8'	78°41' 11°19'	78°30' 11°30'	78°19' 11°41'	78°7' 11°53'
13	79°46' 10°14'	79°37' 10°23'	79°29' 10°31'	79°20' 10°40'	79°11' 10°49'	79°1' 10°59'	78°51' 11°9'	78°41' 11°19'	78°31' 11°29'	78°20' 11°40'	78°9' 11°51'	77°58' 12°2'	77°46' 12°14'	77°34' 12°26'	77°22' 12°38'	77°9' 12°51'
14	79°0' 11°0'	78°51' 11°9'	78°41' 11°19'	78°32' 11°28'	78°22' 11°35'	78°11' 11°49'	78°1' 11°59'	77°51' 12°9'	77°40' 12°20'	77°28' 12°32'	77°17' 12°43'	77°5' 12°55'	76°52' 13°8'	76°39' 13°21'	76°26' 13°34'	76°12' 13°48'
15	78°14' 11°46'	78°4' 11°36'	77°54' 12°6'	77°44' 12°16'	77°34' 12°26'	77°23' 12°37'	77°12' 12°48'	77°0' 13°0'	76°48' 13°12'	76°36' 13°24'	76°24' 13°36'	75°58' 13°49'	75°44' 14°2'	75°30' 14°16'	75°15' 14°30'	75°0' 14°45'
16	77°28' 12°32'	77°18' 12°42'	77°7' 12°53'	76°57' 13°3'	76°45' 13°15'	76°34' 13°26'	76°22' 13°38'	76°10' 14°2'	75°58' 14°15'	75°45' 14°28'	75°32' 14°42'	75°18' 14°56'	75°4' 15°11'	74°49' 15°25'	74°35' 15°41'	74°19' 15°54'
17	76°43' 13°17'	76°32' 13°28'	76°21' 13°39'	76°10' 13°50'	75°58' 14°2'	75°45' 14°14'	75°33' 14°27'	75°21' 14°39'	75°8' 14°52'	74°54' 15°6'	74°40' 15°20'	74°25' 15°35'	74°11' 15°49'	73°56' 16°4'	73°40' 16°20'	73°24' 16°36'
18	75°58' 14°2'	75°46' 14°14'	75°35' 14°25'	75°23' 14°36'	75°10' 14°50'	74°58' 15°2'	74°45' 15°15'	74°31' 15°29'	74°17' 15°43'	74°3' 15°57'	73°49' 16°11'	73°33' 16°27'	73°18' 16°42'	73°2' 16°58'	72°45' 17°15'	72°29' 17°31'
19	75°13' 14°47'	75°1' 14°59'	74°49' 15°11'	74°36' 15°24'	74°23' 15°37'	74°10' 15°50'	73°56' 16°4'	73°42' 16°18'	73°28' 16°32'	73°15' 16°47'	72°58' 17°2'	72°42' 17°18'	72°26' 17°34'	72°9' 17°51'	71°52' 18°8'	71°34' 18°26'
20	74°29' 15°31'	74°16' 15°44'	73°53' 15°57'	73°39' 16°10'	73°25' 16°23'	73°9' 16°42'	72°54' 16°51'	72°39' 17°6'	72°23' 17°21'	72°7' 17°37'	71°51' 17°53'	71°34' 18°9'	71°16' 18°26'	70°59' 18°44'	70°40' 19°1'	70°20' 19°20'
21	73°45' 16°15'	73°32' 16°28'	73°18' 16°42'	73°4' 16°56'	72°50' 17°10'	72°36' 17°24'	72°21' 17°39'	72°6' 17°54'	71°50' 18°10'	71°34' 18°26'	71°17' 18°42'	71°0' 19°0'	70°43' 19°17'	70°24' 19°36'	70°6' 19°54'	69°46' 20°14'
22	73°1' 16°59'	72°47' 17°13'	72°33' 17°27'	72°19' 17°41'	72°4' 17°56'	71°49' 18°11'	71°34' 18°26'	71°18' 18°42'	70°45' 18°58'	70°28' 19°15'	70°10' 19°30'	69°52' 19°46'	69°34' 20°3'	69°13' 20°27'	68°54' 20°47'	68°34' 21°6'
23	72°17' 17°43'	72°3' 17°57'	71°49' 18°11'	71°34' 18°26'	71°19' 18°41'	71°3' 18°57'	70°47' 19°13'	70°30' 19°30'	70°14' 19°46'	69°57' 20°3'	69°39' 20°20'	69°20' 20°40'	69°2' 20°58'	68°42' 21°18'	68°22' 21°35'	68°2' 21°58'
24	71°34' 18°26'	71°19' 18°41'	71°5' 18°55'	70°49' 19°11'	70°34' 19°26'	70°17' 19°43'	69°44' 19°59'	69°26' 20°16'	69°9' 20°34'	68°51' 20°51'	68°31' 21°9'	68°10' 21°29'	67°52' 21°48'	67°31' 22°8'	67°10' 22°29'	66°48' 22°50'
25	70°51' 19°9'	70°36' 19°24'	70°21' 19°39'	70°5' 19°55'	69°49' 20°11'	69°32' 20°28'	69°15' 20°45'	68°57' 21°3'	68°40' 21°20'	68°21' 21°39'	68°3' 21°57'	67°43' 22°17'	67°23' 22°37'	67°2' 22°58'	66°41' 23°19'	66°19' 23°41'
26	70°9' 19°51'	69°53' 20°7'	69°37' 20°23'	69°21' 20°39'	68°48' 20°56'	68°30' 21°12'	68°12' 21°29'	67°54' 21°48'	67°34' 22°6'	67°13' 22°26'	66°55' 22°45'	66°34' 23°5'	66°14' 23°26'	65°53' 23°47'	65°31' 24°9'	65°29' 24°31'
27	69°27' 20°33'	69°10' 20°50'	68°54' 21°6'	68°38' 21°22'	68°20' 21°40'	68°3' 21°57'	67°45' 22°15'	67°26' 22°34'	67°8' 22°52'	66°48' 23°12'	66°28' 23°32'	66°7' 23°53'	65°46' 24°14'	65°25' 24°35'	65°2' 24°58'	64°39' 25°21'
28	68°45' 21°15'	68°29' 21°31'	68°12' 21°48'	67°55' 22°5'	67°37' 22°23'	67°19' 22°41'	66°42' 22°59'	66°22' 23°18'	66°2' 23°38'	65°42' 23°58'	65°22' 24°18'	65°2' 24°39'	64°59' 25°1'	64°37' 25°23'	64°14' 25°46'	63°52' 26°10'
29	68°4' 21°56'	67°47' 22°13'	67°30' 22°30'	67°12' 22°48'	66°54' 23°6'	66°36' 23°24'	66°17' 23°43'	65°57' 24°3'	65°36' 24°23'	65°16' 24°44'	64°55' 25°5'	64°34' 25°26'	64°12' 25°48'	63°50' 26°10'	63°26' 26°34'	62°58' 26°58'
30	67°23' 22°37'	67°6' 22°54'	66°48' 23°12'	66°30' 23°30'	66°12' 23°48'	65°52' 24°7'	65°33' 24°27'	65°14' 24°57'	64°53' 25°28'	64°32' 25°50'	64°9' 26°11'	63°49' 26°34'	63°26' 26°57'	63°3' 27°21'	62°39' 27°46'	62°14' 27°46'
31	66°42' 23°18'	66°25' 23°35'	66°6' 23°52'	65°48' 24°12'	65°29' 24°31'	65°10' 24°50'	64°50' 25°10'	64°30' 25°30'	64°9' 25°51'	63°48' 26°12'	63°26' 26°34'	63°3' 26°57'	62°40' 27°20'	62°18' 27°42'	61°53' 28°7'	61°28' 28°32'
32	66°2' 23°58'	65°44' 24°16'	65°26' 24°34'	65°7' 24°53'	64°48' 25°12'	64°28' 25°32'	64°8' 25°52'	63°47' 26°13'	63°26' 26°34'	63°4' 26°56'	62°42' 27°18'	62°19' 27°41'	61°56' 28°4'	61°32' 28°28'	61°7' 28°53'	60°41' 29°19'
33	65°23' 24°37'	65°4' 24°56'	64°45' 25°15'	64°26' 25°34'	64°7' 25°53'	63°47' 26°13'	63°26' 26°34'	63°5' 26°55'	62°43' 27°17'	62°21' 27°39'	61°38' 28°2'	61°15' 28°25'	60°52' 28°49'	60°28' 29°13'	59°37' 29°39'	59°11' 29°56'
34	64°43' 25°17'	64°25' 25°35'	64°5' 25°53'	63°46' 26°14'	63°26' 26°34'	63°5' 26°55'	62°43' 27°15'	62°23' 27°37'	62°1' 27°59'	61°38' 28°22'	61°15' 28°45'	60°52' 29°8'	60°28' 29°32'	59°37' 29°57'	59°11' 30°23'	58°44' 30°49'
35	64°5' 25°55'	63°45' 26°15'	63°26' 26°34'	63°6' 26°54'	62°46' 27°14'	62°25' 27°35'	62°4' 27°56'	61°42' 28°18'	61°19' 28°41'	60°57' 29°3'	60°34' 29°27'	60°9' 29°51'	59°45' 30°15'	59°19' 30°39'	58°53' 31°7'	58°27' 31°33'
36	63°26' 26°34'	63°7' 26°53'	62°47' 27°13'	62°27' 27°33'	62°6' 27°54'	61°45' 28°15'	61°23' 28°37'	61°1' 28°59'	60°38' 29°22'	60°15' 29°45'	59°51' 30°9'	59°27' 30°33'	58°53' 30°58'	58°28' 31°23'	57°53' 31°50'	57°43' 32°17'
37	62°48' 27°12'	62°28' 27°32'	62°8' 27°52'	61°28' 28°12'	61°7' 28°33'	60°44' 28°55'	60°21' 29°16'	59°58' 29°39'	59°35' 30°2'	59°10' 30°25'	58°46' 31°14'	58°21' 31°40'	57°54' 32°6'	57°28' 32°32'	56°51' 32°59'	56°19' 33°25'
38	62°11' 27°49'	61°51' 28°9'	61°30' 28°30'	61°9' 28°51'	60°48' 29°12'	60°26' 29°34'	59°54' 29°56'	59°31' 30°19'	58°54' 30°42'	58°30' 31°6'	58°5' 31°30'	57°53' 31°55'	57°39' 32°21'	57°13' 32°47'	56°46' 33°14'	56°19' 33°41'
39	61°33' 28°27'	61°13' 28°47'	60°53' 29°7'	60°31' 29°29'	60°10' 29°50'	59°48' 30°12'	59°25' 30°35'	59°2' 30°58'	58°39' 31°21'	58°14' 31°46'	57°50' 32°10'	57°24' 32°36'	56°58' 33°2'	56°32' 33°54'	56°6' 34°21'	55°37' 34°48'
40	60°57' 29°3'	60°36' 29°24'	60°15' 29°45'	59°53' 30°7'	59°32' 30°28'	59°10' 30°50'	58°47' 31°13'	58°24' 31°36'	58°0' 32°0'	57°35' 32°25'	57°10' 32°50'	56°44' 33°16'	56°19' 33°41'	55°52' 34°18'	55°24' 34°45'	54°57' 35°3'
41	60°20' 29°40'	60°0' 30°0'	59°39' 30°21'	58°55' 30°43'	58°32' 31°5'	58°9' 31°28'	57°32' 31°51'	57°1' 32°15'	56°45' 32°39'	56°19' 33°3'	55°53' 33°38'	55°27' 34°34'	54°59' 34°48'	54°30' 35°34'	54°1' 35°51'	53°37' 36°24'
42	59°45' 30°15'	59°24' 30°36'	58°40' 30°57'	58°18' 31°20'	57°55' 31°42'	57°32' 32°5'	56°45' 32°28'	56°19' 32°52'	55°53' 33°17'	55°27' 33°41'	54°59' 34°7'	54°30' 34°33'	53°52' 35°0'	53°24' 35°27'	52°55' 35°55'	52°26' 36°23'

For Bevel Gears with axes at right angles.

Angle for gear above, for pinion below.

ANGLE OF EDGE.

GEAR

	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42
12	77°54' 12°6'	77°42' 12°18'	77°25' 12°32'	77°15' 12°45'	77°0' 13°0'	76°46' 13°14'	76°30' 13°30'	76°14' 13°46'	75°58' 14°2'	75°41' 14°19'	75°23' 14°37'	75°4' 14°56'	74°45' 15°15'	74°25' 15°35'	74°3' 15°57'
13	76°56' 13°4'	76°42' 13°18'	76°28' 13°32'	76°13' 13°47'	75°55' 14°2'	75°42' 14°18'	75°26' 14°34'	75°8' 14°52'	74°51' 15°9'	74°32' 15°28'	74°13' 15°47'	73°53' 16°7'	73°32' 16°28'	73°11' 16°49'	72°48' 17°12'
14	75°58' 14°2'	75°43' 14°17'	75°28' 14°32'	75°12' 14°48'	74°56' 15°4'	74°39' 15°21'	74°21' 15°39'	74°3' 15°57'	73°44' 16°16'	73°25' 16°35'	73°4' 16°56'	72°43' 17°17'	72°21' 17°39'	71°58' 18°2'	71°34' 18°26'
15	75°0' 15°0'	74°44' 15°16'	74°29' 15°31'	74°12' 15°48'	73°55' 16°5'	73°37' 16°23'	73°18' 16°42'	72°59' 17°1'	72°39' 17°21'	72°18' 17°42'	71°56' 18°4'	71°34' 18°26'	71°10' 18°50'	70°46' 19°14'	70°21' 19°39'
16	74°3' 15°57'	73°47' 16°13'	73°30' 16°30'	73°12' 16°48'	72°54' 17°6'	72°35' 17°16'	72°15' 17°45'	71°55' 18°5'	71°34' 18°26'	71°12' 18°48'	70°49' 19°11'	70°26' 19°34'	70°1' 19°59'	69°35' 20°25'	69°9' 20°51'
17	73°7' 16°53'	72°49' 17°11'	72°31' 17°29'	72°13' 17°47'	71°54' 18°6'	71°34' 18°36'	71°13' 18°47'	70°52' 19°8'	70°30' 19°30'	70°7' 19°53'	69°43' 20°17'	69°17' 20°43'	68°52' 21°8'	68°26' 21°34'	67°58' 22°2'
18	72°11' 17°49'	71°53' 18°7'	71°34' 18°26'	71°15' 18°45'	70°54' 19°6'	70°33' 19°16'	70°12' 19°47'	69°50' 20°10'	69°26' 20°34'	69°3' 20°57'	68°38' 21°22'	68°12' 21°48'	67°45' 22°15'	67°17' 22°43'	66°48' 23°12'
19	71°15' 18°45'	70°57' 19°1'	70°37' 19°23'	70°17' 19°43'	69°56' 20°4'	69°34' 20°26'	69°12' 20°48'	68°48' 21°12'	68°25' 21°35'	68°59' 22°1'	68°34' 22°26'	68°8' 22°54'	67°36' 23°22'	66°10' 23°50'	65°39' 24°21'
20	70°21' 19°39'	70°1' 19°59'	69°41' 20°19'	69°19' 20°39'	68°57' 21°3'	68°35' 21°25'	68°12' 21°48'	67°48' 22°12'	67°23' 22°37'	66°57' 23°2'	66°30' 23°30'	66°2' 23°58'	65°33' 24°27'	64°37' 24°57'	64°32' 25°28'
21	69°26' 20°34'	69°6' 20°54'	68°45' 21°15'	68°23' 21°37'	68°0' 22°0'	67°37' 22°23'	67°13' 22°47'	66°48' 23°12'	66°22' 23°38'	65°55' 24°5'	65°28' 24°32'	64°59' 25°1'	64°29' 25°31'	63°53' 26°2'	63°26' 26°34'
22	68°33' 21°27'	68°12' 21°48'	67°50' 22°10'	67°27' 22°33'	67°4' 22°56'	66°40' 23°20'	66°15' 23°45'	65°49' 24°11'	65°23' 24°37'	64°55' 25°5'	64°26' 25°34'	63°57' 26°3'	63°26' 26°34'	62°54' 27°1'	62°21' 27°39'
23	67°41' 22°19'	67°18' 22°42'	66°55' 23°5'	66°32' 23°28'	66°8' 23°52'	65°44' 24°16'	65°18' 24°42'	64°51' 25°9'	64°24' 25°36'	63°55' 26°5'	63°26' 26°34'	62°56' 27°4'	62°24' 27°36'	61°52' 28°3'	61°18' 28°42'
24	66°48' 23°12'	66°26' 23°34'	66°2' 23°58'	65°38' 24°22'	65°14' 24°46'	64°48' 25°12'	64°22' 25°38'	63°54' 26°6'	63°26' 26°34'	62°57' 27°3'	62°27' 27°33'	61°56' 28°4'	61°23' 29°10'	60°50' 29°45'	60°15' 30°14'
25	65°57' 24°3'	65°33' 24°27'	65°9' 24°51'	64°45' 25°15'	64°20' 25°40'	63°53' 26°6'	63°26' 26°34'	62°58' 27°2'	62°29' 27°53'	61°59' 28°1'	61°29' 28°31'	60°57' 29°3'	60°24' 29°36'	59°50' 30°10'	59°14' 30°46'
26	65°6' 24°34'	64°42' 25°18'	64°18' 25°42'	63°52' 26°6'	63°26' 26°34'	62°59' 27°1'	62°31' 27°29'	62°3' 27°57'	61°33' 28°27'	60°31' 28°57'	59°59' 29°29'	59°25' 30°1'	58°50' 30°35'	58°14' 31°10'	57°16' 31°46'
27	64°16' 25°44'	63°51' 25°44'	63°26' 26°34'	62°59' 27°0'	62°34' 27°26'	62°6' 27°54'	61°38' 28°22'	60°38' 28°52'	59°33' 29°22'	58°31' 29°53'	57°35' 30°28'	56°32' 30°58'	55°28' 31°32'	54°28' 32°7'	53°16' 32°44'
28	63°26' 26°34'	62°59' 27°24'	62°36' 27°48'	62°1' 28°12'	61°42' 28°36'	61°14' 29°0'	60°45' 29°26'	60°15' 29°51'	59°45' 30°15'	58°47' 30°47'	57°43' 31°13'	56°34' 31°53'	55°28' 32°28'	54°25' 33°4'	53°11' 33°41'
29	62°37' 27°23'	62°12' 27°48'	61°45' 28°15'	61°19' 28°41'	60°51' 29°9'	60°23' 29°37'	59°53' 30°7'	59°23' 30°37'	58°52' 31°8'	58°19' 31°41'	57°46' 32°4'	57°12' 32°48'	56°37' 33°28'	55°0' 34°0'	53°23' 34°37'
30	61°49' 28°11'	61°23' 28°37'	60°57' 29°3'	60°29' 29°31'	59°59' 29°59'	59°29' 30°28'	58°58' 30°58'	58°26' 31°28'	57°53' 32°0'	57°21' 32°33'	56°48' 33°7'	56°14' 33°41'	55°43' 34°17'	54°58' 34°55'	53°52' 35°32'
31	61°2' 28°35'	60°36' 29°24'	60°6' 29°54'	59°41' 30°19'	59°12' 30°48'	58°42' 31°18'	58°12' 31°48'	57°41' 32°19'	57°8' 32°52'	56°36' 33°24'	56°1' 33°59'	55°26' 34°34'	54°50' 35°10'	54°12' 35°48'	53°34' 36°26'
32	60°15' 29°45'	59°48' 30°12'	59°21' 30°39'	58°52' 31°3'	58°34' 31°26'	57°54' 32°6'	57°23' 32°37'	56°52' 33°8'	56°19' 33°41'	55°45' 34°15'	55°11' 34°49'	54°35' 35°25'	53°58' 36°2'	53°21' 36°39'	52°14' 37°18'
33	59°29' 30°31'	59°2' 30°58'	58°34' 31°26'	58°3' 31°55'	57°36' 32°24'	56°39' 32°54'	55°34' 33°26'	54°30' 33°58'	53°30' 34°30'	52°36' 35°4'	51°41' 35°39'	50°47' 36°15'	49°52' 36°52'	48°57' 37°31'	47°7' 38°9'
34	58°44' 31°16'	58°10' 31°44'	57°45' 32°12'	57°19' 32°41'	56°49' 33°11'	56°19' 33°41'	55°47' 34°13'	55°15' 34°45'	54°41' 35°19'	53°53' 35°53'	53°24' 36°28'	52°44' 37°4'	52°3' 37°42'	51°30' 38°20'	50°12' 39°0'
35	58°0' 32°0'	57°32' 32°28'	57°3' 32°57'	56°33' 33°27'	55°33' 33°57'	54°33' 34°28'	53°33' 35°0'	52°33' 35°32'	51°47' 36°7'	51°12' 36°40'	50°35' 37°16'	49°56' 37°53'	49°17' 38°30'	48°32' 39°7'	47°37' 39°48'
36	57°16' 33°44'	56°48' 33°12'	56°19' 33°41'	55°49' 34°11'	55°18' 34°42'	54°47' 35°13'	54°15' 35°45'	53°42' 36°18'	53°8' 36°52'	52°33' 37°38'	51°57' 38°13'	51°20' 38°48'	50°43' 39°25'	50°4' 39°56'	49°24' 40°36'
37	56°32' 33°28'	56°4' 33°56'	55°35' 34°25'	54°35' 34°55'	53°35' 35°26'	52°35' 35°56'	51°35' 36°27'	50°35' 36°58'	49°35' 37°28'	48°35' 38°0'	47°35' 38°31'	46°35' 39°3'	45°35' 39°28'	44°35' 40°3'	43°35' 41°3'
38	55°51' 34°9'	55°21' 34°39'	54°52' 35°3'	54°23' 35°37'	53°51' 35°39'	53°18' 36°42'	52°46' 37°14'	52°12' 37°48'	51°38' 38°22'	50°63' 38°57'	49°27' 39°33'	48°27' 40°11'	47°27' 40°49'	46°27' 41°28'	45°27' 42°8'
39	55°9' 34°51'	54°39' 35°21'	54°10' 35°50'	53°39' 36°21'	53°7' 36°53'	52°36' 37°24'	51°36' 37°57'	50°36' 38°31'	49°36' 39°41'	48°36' 40°15'	47°36' 40°49'	46°36' 41°23'	45°36' 42°1'	44°36' 42°53'	43°36' 43°33'
40	54°28' 35°32'	53°58' 36°2'	53°28' 36°32'	52°58' 37°2'	52°28' 37°34'	51°54' 38°6'	51°20' 38°40'	50°46' 39°14'	49°54' 39°48'	49°12' 40°24'	48°30' 41°1'	47°48' 41°38'	46°48' 42°16'	45°48' 42°55'	44°48' 43°36'
41	53°48' 36°12'	53°17' 36°43'	52°48' 37°12'	52°17' 37°44'	51°45' 38°15'	51°12' 38°48'	50°39' 39°21'	49°57' 39°55'	49°15' 40°30'	48°33' 41°6'	47°51' 41°43'	47°10' 42°20'	46°28' 42°59'	45°46' 43°38'	44°46' 44°19'
42	53°3' 36°52'	52°38' 37°22'	52°8' 37°52'	51°36' 38°24'	50°44' 38°56'	49°52' 39°28'	49°5' 40°2'	48°58' 40°36'	48°11' 41°11'	47°24' 41°47'	46°37' 42°31'	45°50' 43°4'	45°10' 43°40'	44°20' 44°20'	45°

For Bevel Gears with axes at right angles.

For gear above, for pinion below.

ANGLE OF EDGE.

GEAR

	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	
PINION	12	73°41' 16°19'	73°18' 16°42'	72°54' 17°6'	72°28' 17°32'	72°2' 17°58'	71°34' 18°25'	71°5' 18°55'	70°34' 19°26'	70°1' 19°59'	69°26' 20°34'	68°50' 21°10'	68°12' 21°48'	67°31' 22°29'	66°48' 23°12'	66°2' 23°58'
	13	72°25' 17°35'	71°59' 18°1'	71°34' 18°26'	71°7' 18°53'	70°39' 19°21'	70°9' 19°51'	69°37' 20°23'	69°5' 20°55'	68°30' 21°30'	67°53' 22°7'	67°15' 22°45'	66°34' 23°26'	65°51' 24°9'	65°6' 24°54'	64°17' 25°43'
	14	71°9' 18°51'	70°43' 19°17'	70°15' 19°45'	69°46' 20°14'	69°16' 20°44'	68°45' 21°15'	68°12' 21°48'	67°37' 22°23'	67°0' 23°0'	66°23' 23°37'	65°42' 24°18'	64°59' 25°1'	64°14' 25°46'	63°26' 26°34'	62°36' 27°24'
	15	69°54' 20°6'	69°26' 20°34'	68°58' 21°2'	68°28' 21°32'	67°56' 22°4'	67°23' 22°37'	66°48' 23°12'	66°12' 23°48'	65°33' 24°27'	64°53' 25°7'	64°10' 25°50'	63°26' 26°34'	62°39' 27°21'	61°49' 28°11'	60°57' 29°3'
	16	68°41' 21°19'	68°12' 21°48'	67°42' 22°18'	67°10' 22°50'	66°37' 23°23'	66°3' 23°58'	65°26' 24°34'	64°48' 25°12'	64°8' 25°52'	63°26' 26°34'	62°42' 27°18'	61°56' 28°4'	61°7' 28°53'	60°15' 29°45'	59°21' 30°39'
	17	67°29' 22°31'	66°58' 23°2'	66°27' 23°33'	65°54' 24°6'	65°19' 24°41'	64°43' 25°17'	64°6' 25°54'	63°26' 26°34'	62°45' 27°15'	62°1' 27°59'	61°15' 28°45'	60°28' 29°32'	59°37' 30°23'	58°44' 31°16'	57°48' 32°12'
	18	66°18' 23°42'	65°46' 24°14'	65°14' 24°46'	64°39' 25°21'	64°4' 25°56'	63°26' 26°34'	62°47' 27°13'	62°6' 27°54'	61°23' 28°37'	60°38' 29°22'	59°51' 30°9'	59°2' 30°58'	58°10' 31°50'	57°16' 32°44'	56°19' 33°41'
	19	65°8' 24°52'	64°36' 25°24'	64°2' 25°58'	63°42' 26°34'	62°49' 27°11'	62°10' 27°50'	61°30' 28°30'	60°48' 29°12'	60°4' 29°56'	59°18' 30°42'	58°30' 31°30'	57°39' 32°21'	56°46' 33°14'	55°51' 34°9'	54°52' 35°8'
	20	64°0' 26°0'	63°26' 26°34'	62°51' 27°9'	62°14' 27°46'	61°37' 28°23'	60°57' 29°3'	60°15' 29°45'	59°32' 30°28'	58°47' 31°13'	58°0' 32°0'	57°10' 32°50'	56°19' 33°41'	55°24' 34°36'	54°28' 35°32'	53°28' 36°32'
	21	62°53' 27°7'	62°18' 27°42'	61°42' 28°18'	61°4' 28°56'	60°25' 29°35'	59°45' 30°15'	59°2' 30°58'	58°18' 31°42'	57°32' 32°28'	56°43' 33°17'	55°53' 34°7'	55°0' 35°0'	54°5' 35°55'	53°7' 36°53'	52°8' 37°52'
	22	61°47' 28°13'	61°11' 28°49'	60°34' 29°26'	59°56' 30°4'	59°15' 30°45'	58°34' 31°26'	57°51' 32°9'	57°6' 32°54'	56°19' 33°41'	55°29' 34°31'	54°38' 35°22'	53°45' 36°15'	52°49' 37°11'	51°50' 38°10'	50°49' 39°11'
	23	60°42' 29°18'	60°6' 29°54'	59°28' 30°32'	58°49' 31°11'	58°8' 31°52'	57°25' 32°33'	56°41' 33°19'	55°55' 34°5'	55°7' 34°53'	54°18' 35°42'	53°26' 36°34'	52°31' 37°29'	51°35' 38°25'	50°36' 39°24'	49°34' 40°26'
	24	59°39' 30°21'	58°52' 30°58'	58°23' 31°37'	57°44' 32°16'	57°2' 32°58'	56°19' 33°41'	55°33' 34°27'	54°47' 35°13'	53°58' 36°2'	53°8' 36°52'	52°15' 37°45'	51°20' 38°40'	50°23' 39°37'	49°24' 40°36'	48°22' 41°38'
	25	58°38' 31°22'	58°0' 32°0'	57°20' 32°40'	56°40' 33°20'	55°57' 34°3'	55°13' 34°47'	54°28' 35°32'	53°40' 36°20'	52°51' 37°9'	52°0' 38°0'	51°7' 38°53'	50°12' 39°48'	49°14' 40°46'	48°14' 41°46'	47°12' 42°48'
	26	57°37' 32°23'	56°58' 33°2'	56°19' 33°41'	55°37' 34°23'	54°54' 35°6'	54°10' 35°50'	53°24' 36°36'	52°36' 37°24'	51°46' 38°14'	50°54' 39°6'	50°1' 39°59'	49°5' 40°55'	48°7' 41°53'	47°0' 42°53'	46°5' 43°55'
	27	56°33' 33°22'	55°59' 34°1'	55°18' 34°42'	54°36' 35°24'	53°53' 36°7'	53°7' 36°53'	52°21' 37°39'	51°33' 38°27'	50°43' 39°17'	49°51' 40°9'	48°57' 41°3'	48°0' 42°0'	47°3' 42°57'	46°2' 43°58'	45°
	28	55°40' 34°20'	55°0' 35°0'	54°19' 35°41'	53°37' 36°23'	52°53' 37°7'	52°8' 37°52'	51°20' 38°40'	50°32' 39°28'	49°41' 40°19'	48°49' 41°11'	47°55' 42°5'	46°58' 43°2'	46°0' 44°0'	45°	
	29	54°44' 35°16'	54°3' 35°57'	53°22' 36°38'	52°39' 37°21'	51°55' 38°5'	51°9' 38°51'	50°21' 39°39'	49°32' 40°28'	48°41' 41°19'	47°49' 42°11'	46°54' 43°6'	45°58' 44°2'	45°		
	30	53°48' 36°12'	53°7' 36°53'	52°26' 37°34'	51°42' 38°18'	50°58' 39°2'	50°12' 39°48'	49°24' 40°36'	48°35' 41°25'	47°43' 42°17'	46°51' 43°9'	45°56' 44°4'	45°			
	31	52°54' 37°6'	52°13' 37°47'	51°31' 38°29'	50°48' 39°12'	50°2' 39°58'	49°16' 40°44'	48°28' 41°32'	47°39' 42°21'	46°47' 43°13'	45°54' 44°6'	45°				
	32	52°2' 37°58'	51°20' 38°40'	50°38' 39°22'	49°54' 40°6'	49°9' 40°51'	48°22' 41°38'	47°34' 42°26'	46°44' 43°16'	45°53' 44°7'	45°					
	33	51°10' 38°50'	50°29' 39°31'	49°46' 40°14'	49°2' 40°58'	48°16' 41°44'	47°29' 42°31'	46°41' 43°19'	45°51' 44°9'	45°						
	34	50°20' 39°40'	49°38' 40°22'	48°55' 41°5'	48°11' 41°49'	47°25' 42°35'	46°38' 43°22'	45°50' 44°10'	45°							
	35	49°31' 40°29'	48°48' 41°12'	48°5' 41°55'	47°21' 42°39'	46°35' 43°25'	45°48' 44°12'	45°								
	36	48°43' 41°17'	48°0' 42°0'	47°17' 42°43'	46°33' 43°27'	45°47' 44°13'	45°									
	37	47°56' 42°4'	47°14' 42°46'	46°30' 43°30'	45°46' 44°14'	45°										
	38	47°10' 42°50'	46°28' 43°32'	45°45' 44°15'	45°											
	39	46°26' 43°34'	45°43' 44°17'	45°												
	40	45°42' 44°18'	45°													
	41	45°														

For Bevel Gears with axes at right angles.
Angle for gear above, for pinion below.

For Bevel Gears with axes at right angles.
Angle for gear above, for pinion below.

ANGLE OF EDGE.

GEAR

		GEAR														
		26	25	24	23	22	21	20	19	18	17	16	15	14	13	12
PINION	12	05°14' 24°46'	04°22' 25°38'	03°26' 26°34'	02°27' 27°33'	01°23' 28°37'	00°15' 29°45'	59°2' 30°58'	57°44' 32°16'	56°19' 33°41'	54°47' 35°13'	53°7' 36°53'	51°20' 38°40'	49°24' 40°36'	47°17' 42°43'	45°
	13	03°26' 26°34'	02°31' 27°39'	01°33' 28°27'	00°31' 29°29'	59°25' 30°35'	58°14' 31°46'	56°58' 33°2'	55°37' 34°23'	54°10' 35°50'	52°36' 37°24'	50°54' 39°6'	49°5' 40°55'	47°7' 42°53'	45°	
	14	01°42' 28°18'	00°45' 29°15'	59°45' 30°15'	58°40' 31°20'	57°32' 32°28'	56°19' 33°41'	55°0' 35°0'	53°37' 36°23'	52°8' 37°52'	50°32' 39°28'	48°48' 41°12'	46°58' 43°2'	45°		
	15	00°1' 20°50'	59°2' 30°58'	58°0' 32°0'	56°53' 33°7'	55°43' 34°17'	54°28' 35°32'	53°7' 36°53'	51°42' 38°18'	50°12' 39°48'	48°35' 41°25'	46°51' 43°9'	45°			
	16	58°23' 31°37'	57°23' 32°37'	56°19' 33°41'	55°11' 34°49'	53°58' 36°2'	52°42' 37°18'	51°20' 38°40'	49°54' 40°6'	48°22' 41°38'	46°44' 43°16'	45°				
	17	56°49' 33°11'	55°47' 34°13'	54°41' 35°19'	53°32' 36°28'	52°18' 37°42'	51°0' 39°0'	49°38' 40°22'	48°11' 41°49'	46°38' 43°22'	45°					
	18	55°18' 34°42'	54°15' 35°45'	53°7' 36°53'	51°57' 38°3'	50°43' 39°17'	49°24' 40°36'	48°0' 42°0'	46°33' 43°27'	45°						
	19	53°51' 36°9'	52°46' 37°14'	51°38' 38°22'	50°26' 39°34'	49°11' 40°49'	47°52' 42°3'	46°28' 43°32'	45°							
	20	52°26' 37°34'	51°20' 38°40'	50°12' 39°48'	48°59' 41°1'	47°43' 42°17'	46°24' 43°36'	45°								
	21	51°4' 38°56'	49°58' 40°2'	48°48' 41°12'	47°36' 42°24'	46°20' 43°40'	45°									
	22	49°46' 40°14'	48°39' 41°21'	47°29' 42°31'	46°16' 43°44'	45°										
	23	48°30' 41°30'	47°23' 42°37'	46°13' 43°47'	45°											
	24	47°17' 42°43'	46°10' 43°50'	45°												
	25	46°7' 43°53'	45°													
	26	45°														

For Bevel Gears with axes at right angles.
Angle for gear above, for pinion below.

ANGLE OF FACE.

GEAR

	72	71	70	69	68	67	66	65	64	63	62	61	60	59	58	57
PINION	12	7°53' 78°39'	8° 78°50'	8°7' 78°39'	8°14' 78°30'	8°21' 78°19'	8°28' 78°10'	8°35' 77°59'	8°43' 77°47'	8°51' 77°37'	8°59' 77°25'	9°7' 77°13'	9°17' 77°1'	9°26' 76°48'	9°35' 76°35'	9°45' 76°23'
	13	8°40' 79°12'	8°48' 79°2'	8°54' 79°32'	9° 79°42'	9°3' 79°31'	9°10' 79°20'	9°18' 79°8'	9°26' 78°56'	9°35' 78°45'	9°43' 78°32'	9°52' 78°19'	10°1' 78°7'	10°11' 77°53'	10°21' 77°39'	10°33' 77°26'
	14	9°26' 79°26'	9°34' 79°16'	9°42' 79°4'	9°50' 78°54'	9°59' 78°43'	10°8' 78°30'	10°16' 78°18'	10°25' 78°7'	10°35' 77°55'	10°45' 77°45'	10°54' 77°32'	11°5' 77°19'	11°16' 76°55'	11°27' 76°41'	11°39' 76°28'
	15	10°12' 76°40'	10°21' 76°29'	10°30' 76°18'	10°38' 76°6'	10°47' 75°55'	10°57' 75°43'	11°6' 75°30'	11°16' 75°16'	11°27' 75°3'	11°37' 74°49'	11°47' 74°35'	11°59' 74°21'	12°11' 74°7'	12°22' 73°50'	12°35' 73°35'
	16	10°59' 75°55'	11°7' 75°43'	11°17' 75°31'	11°26' 75°20'	11°37' 75°7'	11°46' 74°54'	11°56' 74°40'	12°7' 74°27'	12°17' 74°13'	12°29' 73°59'	12°40' 73°44'	12°52' 73°28'	13°5' 73°13'	13°18' 72°56'	13°30' 72°40'
	17	11°44' 75°10'	11°54' 74°58'	12°4' 74°46'	12°13' 74°33'	12°24' 74°20'	12°34' 74°5'	12°46' 73°52'	12°56' 73°38'	13°7' 73°23'	13°21' 73°9'	13°32' 72°52'	13°45' 72°35'	13°59' 72°21'	14°11' 72°3'	14°20' 71°45'
	18	12°29' 74°25'	12°40' 74°12'	12°50' 74°0'	13° 73°46'	13°12' 73°32'	13°23' 73°19'	13°34' 73°4'	13°47' 72°49'	13°59' 72°33'	14°12' 72°18'	14°24' 72°2'	14°38' 71°48'	14°52' 71°28'	15°6' 71°10'	15°21' 70°51'
	19	13°14' 73°10'	13°25' 73°27'	13°36' 73°14'	13°48' 73°0'	14° 72°46'	14°11' 72°31'	14°24' 72°16'	14°36' 72°0'	14°49' 71°45'	15°2' 71°28'	15°15' 71°10'	15°30' 70°54'	15°44' 70°39'	15°59' 70°25'	16°13' 69°59'
	20	13°59' 72°57'	14°11' 72°43'	14°23' 72°29'	14°34' 72°14'	14°46' 72°0'	15°4' 71°45'	15°11' 71°29'	15°25' 71°13'	15°39' 70°56'	15°52' 70°38'	16°7' 70°21'	16°21' 70°3'	16°37' 69°45'	16°53' 69°25'	17°9' 68°46'
	21	14°43' 72°13'	14°55' 71°59'	15°8' 71°44'	15°21' 71°29'	15°33' 71°13'	15°46' 70°58'	15°59' 70°41'	16°13' 70°25'	16°28' 70°8'	16°42' 69°50'	16°58' 69°32'	17°13' 69°13'	17°28' 68°54'	17°46' 68°34'	18°2' 68°14'
	22	15°27' 71°29'	15°40' 71°14'	15°53' 70°59'	16°6' 70°44'	16°20' 70°28'	16°33' 70°11'	16°47' 69°55'	17°2' 69°33'	17°16' 69°20'	17°31' 69°6'	17°49' 68°53'	18°3' 68°34'	18°20' 68°14'	18°37' 67°52'	18°56' 67°27'
	23	16°12' 70°46'	16°24' 70°30'	16°38' 70°16'	16°51' 70°0'	17°5' 69°43'	17°20' 69°26'	17°34' 69°8'	17°50' 68°50'	18°5' 68°33'	18°20' 68°14'	18°36' 67°54'	18°54' 67°34'	19°10' 67°15'	19°28' 66°52'	19°48' 66°32'
	24	16°55' 70°3'	17°7' 69°47'	17°22' 69°32'	17°37' 69°15'	17°51' 68°59'	18°5' 68°40'	18°21' 68°23'	18°37' 68°5'	18°53' 67°45'	19°9' 67°27'	19°26' 67°6'	19°44' 66°46'	20°1' 66°25'	20°19' 66°3'	20°39' 65°18'
	25	17°39' 69°21'	17°52' 69°4'	18°6' 68°48'	18°21' 68°31'	18°36' 68°14'	18°51' 67°56'	19°5' 67°37'	19°24' 67°18'	19°40' 67°0'	19°57' 66°40'	20°14' 66°20'	20°32' 66°0'	20°51' 65°38'	21°10' 65°14'	21°30' 64°28'
	26	18°21' 68°39'	18°30' 68°22'	18°51' 68°5'	19°2' 67°45'	19°22' 67°30'	19°37' 67°13'	19°53' 66°53'	20°10' 66°34'	20°26' 66°14'	20°43' 65°53'	21°2' 65°32'	21°21' 65°11'	22° 64°49'	22°20' 64°26'	22°41' 64°2'
	27	19°3' 67°57'	19°19' 67°41'	19°34' 67°22'	19°49' 67°0'	20°6' 66°46'	20°22' 66°28'	20°38' 66°8'	20°56' 65°45'	21°13' 65°29'	21°32' 65°8'	21°50' 64°46'	22°10' 64°24'	22°29' 64°1'	22°49' 63°39'	23°10' 62°49'
	28	19°46' 67°16'	20°1' 66°39'	20°17' 66°22'	20°32' 66°4'	20°50' 66°44'	21°6' 66°25'	21°23' 66°5'	21°41' 66°44'	22° 66°24'	22°21' 66°12'	22°37' 65°51'	22°56' 65°38'	23°17' 65°25'	23°38' 65°12'	23°59' 64°58'
	29	20°27' 66°35'	20°43' 66°17'	20°59' 66°0'	21°16' 65°40'	21°33' 65°21'	21°50' 65°2'	22°3' 64°42'	22°27' 64°21'	22°45' 63°59'	23°5' 63°37'	23°25' 63°15'	23°42' 62°52'	24°4' 62°28'	24°29' 62°5'	24°48' 61°40'
	30	21°9' 65°55'	21°25' 65°37'	21°42' 65°18'	22°5' 64°58'	22°15' 64°39'	22°34' 64°13'	22°52' 63°50'	23°10' 63°35'	23°28' 63°16'	23°46' 62°54'	24°5' 62°30'	24°30' 62°7'	24°51' 61°43'	25°36' 61°15'	25°59' 60°34'
	31	21°50' 65°14'	22°6' 64°56'	22°24' 64°36'	22°41' 64°17'	22°59' 63°57'	23°17' 63°37'	23°35' 63°15'	23°55' 62°52'	24°14' 62°32'	24°34' 62°10'	24°54' 61°46'	25°17' 61°23'	25°35' 61°0'	25°58' 60°34'	26°22' 60°3'
	32	22°31' 64°35'	22°45' 64°16'	23°4' 63°56'	23°23' 63°37'	23°40' 63°18'	23°58' 62°55'	24°18' 62°34'	24°38' 62°12'	24°58' 61°50'	25°18' 61°26'	25°39' 61°3'	25°59' 60°41'	26°23' 60°15'	26°45' 59°49'	27°9' 59°25'
	33	23°10' 63°56'	23°28' 63°36'	23°46' 63°16'	24°4' 62°56'	24°22' 62°36'	24°41' 62°15'	25°1' 61°53'	25°21' 61°31'	25°42' 61°8'	26°2' 60°44'	26°24' 60°20'	26°45' 59°55'	27°9' 59°31'	27°31' 59°5'	27°56' 58°11'
	34	23°51' 63°17'	24°8' 62°57'	24°27' 62°37'	24°44' 62°16'	25°4' 61°56'	25°23' 61°33'	25°42' 61°12'	26°3' 60°49'	26°24' 60°26'	26°46' 60°2'	27°29' 59°37'	27°52' 59°13'	28°16' 58°54'	28°40' 58°22'	29°5' 57°54'
	35	24°29' 62°39'	24°48' 62°18'	25°6' 61°58'	25°25' 61°37'	25°44' 61°16'	26°4' 60°54'	26°24' 60°32'	26°45' 60°9'	27°8' 59°44'	27°28' 59°22'	28°3' 58°56'	28°13' 58°31'	28°36' 58°6'	29°25' 57°39'	29°50' 56°44'
	36	25°9' 62°1'	25°27' 61°21'	25°45' 61°0'	26°5' 60°39'	26°24' 60°16'	26°45' 60°3'	27°5' 59°51'	27°20' 59°28'	27°45' 59°5'	28°10' 58°50'	28°35' 58°27'	28°56' 58°3'	29°20' 57°54'	29°43' 57°30'	30°9' 56°1'
	37	25°47' 61°23'	26°6' 60°41'	26°25' 60°20'	26°44' 60°0'	27°4' 59°55'	27°25' 59°35'	27°45' 59°13'	28°7' 58°49'	28°29' 58°25'	28°51' 58°1'	29°5' 57°35'	29°38' 57°10'	30°2' 56°42'	30°27' 56°15'	31°08' 55°20'
	38	26°25' 60°47'	26°44' 60°26'	27°4' 60°4'	27°24' 59°42'	27°44' 59°20'	28°4' 58°58'	28°26' 58°34'	28°47' 58°9'	29°9' 57°45'	29°33' 57°21'	29°55' 56°55'	30°20' 56°30'	30°44' 56°2'	31°15' 55°33'	31°35' 54°49'
	39	27°3' 60°9'	27°22' 59°48'	27°42' 59°28'	28°2' 59°4'	28°22' 58°42'	28°43' 58°19'	29°5' 57°55'	29°27' 57°31'	29°49' 57°7'	30°33' 56°41'	31°17' 56°16'	31°11' 55°49'	31°20' 55°22'	31°54' 54°54'	32°43' 54°28'
	40	27°40' 59°34'	28°2' 58°30'	28°20' 58°10'	28°41' 57°50'	29°1' 57°42'	29°21' 57°17'	29°43' 56°54'	30°6' 56°28'	30°28' 56°2'	31°17' 55°37'	31°12' 55°10'	32°0' 54°44'	32°41' 54°15'	33°13' 53°46'	33°57' 53°18'
	41	28°17' 58°57'	28°37' 58°15'	28°57' 57°55'	29°18' 57°32'	29°39' 57°9'	30°1' 56°40'	30°22' 56°15'	30°45' 55°51'	31°9' 55°31'	31°33' 55°11'	32°20' 54°32'	32°46' 54°3'	33°12' 53°36'	33°39' 52°57'	34°6' 52°38'
	42	28°52' 58°22'	29°12' 57°39'	29°33' 57°15'	29°55' 56°52'	30°16' 56°28'	30°38' 56°4'	31° 55°39'	31°23' 55°13'	31°47' 54°48'	32°10' 54°21'	32°35' 53°54'	33° 53°26'	33°32' 52°55'	34°19' 52°29'	34°46' 52°

For Bevel Gears with axes at right angles.

Angle for gear above, for pinion below.

ANGLE OF FACE.

GEAR

	53	55	54	53	52	51	50	49	48	47	46	45	44	43	42
12	16°6'	16°16'	16°28'	16°39'	16°52'	11°3'	11°15'	11°30'	11°43'	11°58'	12°13'	12°29'	12°45'	13°1'	13°19'
13	75°54'	75°40'	75°24'	75°9'	74°52'	74°37'	74°15'	73°58'	73°39'	73°20'	72°59'	72°37'	72°15'	71°51'	71°25'
14	11°4'	11°10'	11°28'	11°42'	11°54'	12°8'	12°30'	12°37'	12°51'	13°7'	13°23'	13°40'	13°58'	14°10'	14°35'
15	74°56'	74°49'	74°24'	74°8'	73°50'	73°32'	73°12'	72°53'	72°33'	72°11'	71°49'	71°26'	71°2'	70°38'	70°11'
16	12°2'	12°16'	12°29'	12°43'	12°57'	13°11'	13°26'	13°42'	13°59'	14°15'	14°33'	14°51'	15°10'	15°30'	15°51'
17	73°58'	73°42'	73°25'	73°7'	72°49'	72°29'	72°8'	71°48'	71°27'	71°5'	70°41'	70°17'	69°52'	69°26'	68°59'
18	13°1'	13°16'	13°28'	13°43'	13°59'	14°14'	14°30'	14°47'	15°5'	15°23'	15°42'	16°1'	16°22'	16°43'	17°5'
19	73°1'	72°44'	72°26'	72°7'	71°49'	71°28'	71°6'	70°45'	70°23'	69°59'	69°34'	69°9'	68°42'	68°15'	67°47'
20	13°59'	14°13'	14°28'	14°44'	15°1'	15°17'	15°35'	15°52'	16°11'	16°30'	16°50'	17°10'	17°32'	17°56'	18°18'
21	72°5'	71°47'	71°28'	71°8'	70°49'	70°27'	70°5'	69°42'	69°19'	68°54'	68°38'	68°2'	67°34'	67°6'	66°36'
22	14°57'	15°11'	15°28'	15°44'	16°1'	16°18'	16°37'	16°55'	17°15'	17°36'	17°57'	18°20'	18°43'	19°6'	19°31'
23	71°9'	70°49'	70°30'	70°10'	69°26'	69°3'	68°39'	68°15'	67°50'	67°23'	66°54'	66°27'	65°58'	65°27'	64°52'
24	15°52'	16°7'	16°26'	16°42'	17°1'	17°20'	17°39'	17°58'	18°20'	18°41'	19°3'	19°27'	19°50'	20°15'	20°42'
25	70°14'	69°53'	69°34'	69°12'	68°49'	68°26'	68°3'	67°38'	67°12'	66°47'	66°19'	65°51'	65°20'	64°50'	64°18'
26	16°49'	17°2'	17°23'	17°41'	18°'	18°22'	18°40'	19°1'	19°22'	19°46'	20°8'	20°34'	20°59'	21°24'	21°52'
27	69°39'	68°58'	68°37'	68°15'	67°52'	67°29'	67°4'	66°37'	66°12'	65°44'	65°16'	64°46'	64°15'	63°44'	63°10'
28	17°14'	18°4'	18°19'	18°40'	19°'	19°20'	19°41'	20°2'	20°25'	20°49'	21°13'	21°39'	22°5'	22°32'	23°'
29	68°26'	68°3'	67°41'	67°18'	66°54'	66°30'	66°5'	65°35'	65°11'	64°43'	64°13'	63°43'	63°11'	62°38'	62°4'
30	18°39'	18°57'	19°16'	19°37'	19°58'	20°19'	20°41'	21°3'	21°27'	21°52'	22°17'	22°43'	23°10'	23°38'	24°8'
31	67°9'	67°9'	66°6'	66°23'	65°53'	65°33'	65°7'	64°39'	64°11'	63°42'	63°13'	62°44'	62°8'	61°34'	61°0'
32	19°32'	19°52'	20°12'	20°33'	20°55'	21°17'	21°40'	22°3'	22°17'	22°53'	23°19'	23°46'	24°15'	24°44'	25°14'
33	66°38'	66°16'	65°52'	65°27'	65°3'	64°37'	64°10'	63°41'	63°13'	62°43'	62°11'	61°40'	61°7'	60°32'	59°56'
34	20°25'	20°47'	21°8'	21°29'	21°52'	22°13'	22°37'	23°2'	23°27'	23°54'	24°21'	24°49'	25°18'	25°48'	26°18'
35	65°47'	65°23'	64°58'	64°33'	64°8'	63°41'	63°13'	62°44'	62°15'	61°44'	61°13'	60°41'	60°6'	59°31'	58°54'
36	21°19'	21°39'	22°1'	22°24'	22°46'	23°10'	23°36'	24°'	24°26'	24°53'	25°21'	25°49'	26°20'	26°51'	27°23'
37	64°55'	64°31'	64°5'	63°40'	63°14'	62°46'	62°19'	61°48'	61°15'	60°47'	60°15'	59°41'	59°6'	58°31'	57°53'
38	22°11'	22°33'	22°56'	23°18'	23°41'	24°7'	24°32'	24°57'	25°24'	25°52'	26°20'	26°50'	27°21'	27°52'	28°26'
39	64°5'	63°39'	63°14'	62°48'	62°21'	61°53'	61°24'	60°53'	60°22'	59°50'	59°18'	58°44'	58°9'	57°32'	56°54'
40	23°3'	23°25'	23°47'	24°13'	24°36'	25°1'	25°28'	25°53'	26°21'	26°49'	27°19'	27°49'	28°21'	28°54'	29°27'
41	63°15'	62°49'	62°23'	61°36'	61°28'	60°59'	60°30'	59°59'	59°27'	58°55'	58°21'	57°47'	57°11'	56°34'	55°55'
42	23°53'	24°16'	24°40'	25°5'	25°29'	25°55'	26°22'	26°48'	27°17'	27°46'	28°16'	28°47'	29°19'	29°52'	30°27'
43	62°25'	61°58'	61°32'	61°5'	60°37'	60°7'	59°38'	59°5'	58°33'	58°'	57°26'	56°51'	56°15'	55°38'	54°59'
44	24°44'	25°7'	25°31'	25°56'	26°22'	26°48'	27°15'	27°43'	28°12'	28°42'	29°12'	29°43'	30°16'	30°50'	31°25'
45	61°36'	61°9'	60°43'	60°14'	59°46'	59°16'	58°45'	58°13'	57°42'	57°8'	56°32'	55°57'	55°20'	54°42'	54°3'
46	25°33'	25°57'	26°22'	26°47'	27°14'	27°40'	28°8'	28°36'	29°5'	29°37'	30°8'	30°40'	31°13'	31°48'	32°23'
47	60°47'	60°21'	59°52'	59°25'	58°56'	58°26'	57°54'	57°22'	56°49'	56°15'	55°40'	55°4'	54°27'	53°45'	53°9'
48	26°22'	26°47'	27°12'	27°38'	28°4'	28°32'	29°'	29°28'	29°58'	30°31'	31°2'	31°34'	32°3'	32°44'	33°19'
49	60°'	59°33'	59°6'	58°36'	58°6'	57°36'	57°4'	56°32'	55°58'	55°24'	54°48'	54°12'	53°34'	52°54'	52°15'
50	27°10'	27°34'	28°3'	28°27'	28°54'	29°23'	29°51'	30°20'	30°52'	31°22'	31°55'	32°29'	33°2'	33°39'	34°15'
51	59°14'	58°46'	58°15'	57°49'	57°18'	56°47'	56°15'	55°42'	55°8'	54°34'	53°57'	53°21'	52°42'	52°3'	51°23'
52	27°58'	28°23'	28°49'	29°17'	29°33'	30°12'	30°42'	31°10'	31°42'	32°14'	32°46'	33°21'	33°56'	34°31'	35°8'
53	58°28'	57°59'	57°31'	57°1'	56°41'	56°'	55°28'	54°54'	54°20'	53°44'	53°8'	52°31'	51°52'	51°13'	50°32'
54	28°45'	29°10'	29°37'	30°5'	30°32'	31°1'	31°31'	32°1'	32°32'	33°4'	33°38'	34°12'	34°47'	35°24'	36°'
55	57°43'	57°14'	56°45'	56°15'	55°49'	55°13'	54°39'	54°5'	53°32'	52°56'	52°20'	51°42'	51°3'	50°22'	49°41'
56	29°31'	29°57'	30°24'	30°51'	31°20'	31°49'	32°19'	32°50'	33°22'	33°54'	34°28'	35°6'	35°38'	36°15'	36°53'
57	56°59'	56°29'	56°'	55°29'	54°58'	54°27'	53°53'	53°20'	52°44'	52°8'	51°32'	50°50'	50°14'	49°35'	48°53'
58	30°15'	30°42'	31°10'	31°38'	32°7'	32°36'	33°7'	33°39'	34°10'	34°42'	35°17'	35°51'	36°27'	37°5'	37°42'
59	56°15'	55°46'	55°16'	54°44'	54°13'	53°53'	53°7'	52°34'	51°58'	51°32'	50°45'	50°17'	49°27'	48°47'	48°6'
60	31°3'	31°27'	31°55'	32°23'	32°53'	33°23'	33°53'	34°25'	34°57'	35°31'	36°5'	36°41'	37°16'	37°53'	38°32'
61	55°32'	55°53'	56°31'	56°1'	55°28'	54°57'	54°23'	53°40'	53°13'	52°37'	49°59'	49°21'	48°42'	48°1'	47°20'
62	31°45'	32°12'	32°40'	33°8'	33°38'	34°9'	34°40'	35°12'	35°43'	36°18'	36°51'	37°27'	38°4'	38°42'	39°20'
63	54°49'	54°20'	53°50'	53°18'	52°46'	52°13'	51°40'	51°4'	50°29'	49°52'	49°15'	48°37'	47°56'	47°16'	46°34'
64	32°27'	32°56'	33°24'	33°52'	34°22'	34°54'	35°24'	35°57'	36°29'	37°3'	37°38'	38°14'	38°51'	39°28'	40°7'
65	54°9'	53°38'	53°8'	52°35'	52°4'	51°30'	50°56'	50°21'	49°45'	49°9'	48°32'	47°52'	47°13'	46°32'	45°51'
66	33°10'	33°39'	34°7'	34°36'	35°7'	35°37'	36°9'	36°41'	37°15'	37°48'	38°24'	39°'	39°36'	40°13'	40°53'
67	53°28'	52°57'	52°27'	51°54'	51°21'	50°49'	50°15'	49°39'	49°3'	48°26'	47°48'	47°10'	46°30'	45°49'	45°7'
68	33°52'	34°21'	34°50'	35°18'	35°49'	36°20'	36°53'	37°25'	37°58'	38°33'	39°8'	39°44'	40°20'	40°55'	41°37'
69	52°48'	52°17'	51°46'	51°14'	50°41'	50°8'	49°33'	48°57'	48°22'	47°45'	47°6'	46°28'	45°45'	45°8'	44°25'
70	34°33'	35°3'	35°31'	36°1'	36°31'	37°3'	37°35'	38°7'	38°11'	39°16'	39°51'	40°27'	41°5'	41°42'	42°22'
71	52°9'	51°37'	51°7'	50°33'	50°1'	49°27'	48°53'	48°17'	47°41'	47°4'	46°25'	45°47'	45°7'	44°26'	43°44'
72	35°14'	35°43'	36°12'	36°42'	37°13'	37°44'	38°17'	38°49'	39°23'	39°58'	40°34'	41°9'	41°47'	42°26'	43°4'
73	51°30'	50°59'	50°28'	49°54'	49°21'	48°48'	48°13'	47°37'	47°1'	46°24'	45°46'	45°7'	44°27'	43°46'	

For Bevel Gears with axes at right angles.

Angle for gear above, for pinion below.

ANGLE OF FACE.

GEAR

PINION

	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27
12	13°37' 70°59'	13°57' 70°33'	14°18' 70°6'	14°39' 69°35'	15°1' 69°5'	15°24' 68°32'	15°49' 67°59'	16°15' 67°23'	16°43' 66°45'	17°13' 66°5'	17°43' 65°23'	18°15' 64°39'	18°51' 63°53'	19°27' 63°3'	20°5' 62°9'
13	14°55' 69°45'	15°17' 69°15'	15°39' 68°47'	16°1' 68°15'	16°25' 67°43'	16°51' 67°9'	17°19' 66°33'	17°46' 65°56'	18°16' 65°16'	18°48' 64°34'	19°21' 63°51'	19°57' 63°5'	20°32' 62°14'	21°11' 61°23'	21°54' 60°28'
14	16°13' 68°31'	16°34' 68°0'	16°59' 67°29'	17°24' 66°56'	17°50' 66°22'	18°17' 65°47'	18°45' 65°9'	19°16' 64°30'	19°48' 63°48'	20°20' 63°6'	20°56' 62°20'	21°34' 61°32'	22°13' 60°41'	22°55' 59°47'	23°38' 58°50'
15	17°28' 67°16'	17°53' 66°45'	18°18' 66°14'	18°44' 65°40'	19°11' 65°3'	19°40' 64°26'	20°11' 63°49'	20°44' 63°8'	21°18' 62°24'	21°53' 61°39'	22°31' 60°51'	23°10' 60°2'	23°51' 59°9'	24°35' 58°13'	25°20' 57°14'
16	18°42' 66°4'	19°9' 65°33'	19°35' 64°59'	20°3' 64°23'	20°32' 63°46'	21°3' 63°7'	21°36' 62°28'	22°9' 61°45'	22°45' 61°01'	23°22' 60°14'	24°1' 59°25'	24°42' 58°34'	25°26' 57°40'	26°12' 56°42'	27°1' 55°43'
17	19°56' 64°54'	20°24' 64°20'	20°51' 63°45'	21°21' 63°9'	21°53' 62°31'	22°24' 61°9'	22°57' 60°25'	23°33' 59°40'	24°10' 58°58'	24°50' 58°1'	25°31' 57°10'	26°14' 56°13'	26°59' 55°15'	27°47' 54°13'	28°37' 53°13'
18	21°9' 63°45'	21°37' 63°9'	22°6' 62°34'	22°38' 61°56'	23°9' 61°17'	23°43' 60°35'	24°18' 59°52'	24°56' 59°8'	25°34' 58°20'	26°15' 57°31'	26°57' 56°39'	27°42' 55°46'	28°29' 54°49'	29°18' 53°50'	30°9' 52°47'
19	22°20' 62°36'	22°49' 62°1'	23°20' 61°24'	23°52' 60°44'	24°26' 60°4'	25°1' 59°21'	25°37' 58°37'	26°15' 57°51'	26°56' 57°4'	27°38' 56°14'	28°22' 55°22'	29°8' 54°26'	29°56' 53°28'	30°43' 52°28'	31°40' 51°24'
20	23°30' 61°30'	24°1' 60°53'	24°32' 60°14'	25°6' 59°34'	25°40' 58°54'	26°16' 58°10'	26°55' 57°25'	27°34' 56°38'	28°15' 55°49'	28°58' 54°58'	29°44' 54°4'	30°31' 53°9'	31°21' 52°9'	32°13' 51°9'	33°8' 50°4'
21	24°39' 60°25'	25°10' 59°46'	25°43' 59°17'	26°18' 58°26'	26°53' 57°43'	27°30' 57°0'	28°10' 55°26'	28°50' 54°36'	29°32' 53°43'	30°17' 52°50'	31°4' 51°52'	31°52' 50°28'	32°43' 49°29'	33°36' 48°30'	34°31' 47°27'
22	25°46' 59°20'	26°19' 58°41'	26°53' 58°1'	27°27' 57°19'	28°5' 56°35'	28°43' 55°51'	29°22' 55°4'	30°5' 54°17'	30°48' 53°26'	31°34' 52°32'	32°22' 51°38'	33°11' 50°41'	34°3' 49°41'	34°57' 48°37'	35°54' 47°32'
23	26°52' 58°16'	27°26' 57°38'	28°0' 56°56'	28°36' 56°14'	29°14' 55°30'	29°53' 54°43'	30°35' 53°57'	31°18' 53°8'	32°1' 52°15'	32°48' 51°24'	33°36' 50°28'	34°27' 49°29'	35°20' 48°30'	36°15' 47°27'	37°12' 46°20'
24	27°57' 57°15'	28°31' 56°35'	29°7' 55°53'	29°43' 55°11'	30°22' 54°26'	31°2' 53°40'	31°45' 52°51'	32°28' 52°2'	33°14' 51°10'	34°1' 50°5'	34°50' 49°20'	35°42' 48°22'	36°35' 47°21'	37°30' 46°18'	38°28' 45°12'
25	28°59' 56°15'	29°34' 55°34'	30°12' 54°52'	30°49' 54°9'	31°29' 53°23'	32°10' 52°36'	32°52' 51°48'	33°37' 50°57'	34°23' 50°5'	35°11' 49°11'	36°0' 48°14'	36°52' 47°16'	37°47' 46°15'	38°43' 45°11'	39°41' 44°5'
26	30°1' 55°15'	30°38' 54°34'	31°14' 53°52'	31°54' 53°8'	32°34' 52°22'	33°15' 51°35'	33°58' 50°46'	34°45' 49°55'	35°31' 49°3'	36°19' 48°7'	37°10' 47°12'	38°2' 46°12'	38°56' 45°10'	39°53' 44°7'	40°52' 43°2'
27	31°3' 54°19'	31°39' 53°37'	32°18' 52°54'	32°57' 52°9'	33°37' 51°23'	34°20' 50°34'	35°3' 49°45'	35°49' 48°55'	36°36' 48°2'	37°25' 47°9'	38°16' 46°10'	39°10' 45°10'	40°4' 44°10'	41°1' 43°5'	42° 42°
28	32°2' 53°22'	32°39' 52°39'	33°18' 51°56'	33°57' 51°11'	34°39' 50°25'	35°21' 49°31'	36°7' 48°47'	36°52' 47°56'	37°40' 47°30'	38°29' 46°58'	39°21' 46°7'	40°15' 45°11'	41°9' 44°11'	42°7' 43°9'	
29	32°59' 52°27'	33°33' 51°44'	34°17' 51°1'	34°58' 50°16'	35°39' 49°29'	36°23' 48°41'	37°8' 47°50'	37°54' 46°58'	38°42' 46°4'	39°32' 45°10'	40°24' 44°12'	41°18' 43°14'	42°13' 42°13'		
30	33°57' 51°33'	34°36' 50°50'	35°15' 50°7'	35°56' 49°20'	36°38' 48°34'	37°21' 47°45'	38°7' 46°55'	38°53' 46°3'	39°43' 45°9'	40°32' 44°14'	41°25' 43°17'	42°18' 42°18'			
31	34°53' 50°41'	35°31' 49°57'	36°11' 49°13'	36°52' 48°28'	37°35' 47°39'	38°20' 46°52'	39°5' 46°1'	39°52' 45°10'	40°41' 44°15'	41°32' 43°20'	42°23' 42°23'				
32	35°46' 49°50'	36°27' 49°7'	37°6' 48°22'	37°48' 47°36'	38°31' 46°49'	39°15' 45°59'	40°1' 45°9'	40°49' 44°17'	41°38' 43°24'	42°28' 42°28'					
33	36°39' 48°59'	37°19' 48°17'	38°0' 47°32'	38°42' 46°46'	39°26' 45°58'	40°0' 45°8'	40°56' 44°18'	41°44' 43°26'	42°33' 42°33'						
34	37°32' 48°12'	38°11' 47°27'	38°53' 46°43'	39°35' 45°57'	40°18' 45°8'	41°4' 44°20'	41°49' 43°29'	42°37' 42°37'							
35	38°22' 47°24'	39°3' 46°39'	39°44' 45°54'	40°26' 45°8'	41°10' 44°20'	41°55' 43°31'	42°41' 42°41'								
36	39°11' 46°37'	39°52' 45°52'	40°34' 45°8'	41°15' 44°21'	42°0' 43°34'	42°45' 42°45'									
37	40°0' 45°52'	40°40' 45°8'	41°22' 44°22'	42°5' 43°37'	42°48' 42°48'										
38	40°47' 45°7'	41°28' 44°24'	42°9' 43°39'	42°52' 42°52'											
39	41°32' 44°24'	42°14' 43°40'	42°56' 42°56'												
40	42°18' 43°42'	42°58' 42°58'													
41	43°2' 43°2'														

For Bevel Gears with axes at right angles.

Angle for gear above, for pinion below.

ANGLE OF FACE.

GEAR

	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12
12	20°46' 61°14'	21°31' 60°15'	22°18' 59°10'	23°8' 58°2'	24°3' 56°49'	25°2' 55°32'	26°3' 54°7'	27°11' 52°39'	28°25' 51°3'	29°43' 49°17'	31°11' 47°25'	32°44' 45°24'	34°26' 43°14'	36°16' 40°50'	38°17'
13	22°37' 59°29'	23°26' 58°28'	24°15' 57°21'	25°9' 56°11'	26°6' 54°56'	27°8' 53°36'	28°14' 52°10'	29°25' 50°39'	30°42' 49°2'	32°4' 47°16'	33°34' 45°22'	35°10' 43°20'	36°55' 41°9'	38°48'	
14	24°25' 57°49'	25°16' 56°46'	26°8' 55°38'	27°5' 54°25'	28°4' 53°8'	29°9' 51°47'	30°20' 50°20'	31°33' 48°47'	32°52' 47°8'	34°18' 45°12'	35°50' 43°26'	37°28' 41°24'	39°15'		
15	26°11' 56°13'	27°3' 55°7'	27°58' 53°58'	28°58' 52°44'	30°0' 51°26'	31°6' 50°2'	32°19' 48°33'	33°36' 47°0'	34°56' 45°20'	36°23' 43°33'	37°57' 41°39'	39°38'			
16	27°52' 54°38'	28°45' 53°31'	29°43' 52°21'	30°44' 51°6'	31°50' 49°46'	32°58' 48°22'	34°12' 46°52'	35°31' 45°19'	36°54' 43°38'	38°23' 41°51'	39°57'				
17	29°30' 53°3'	30°26' 52°0'	31°26' 50°48'	32°28' 49°32'	33°35' 48°11'	34°47' 46°47'	36°0' 45°16'	37°21' 43°43'	38°45' 42°1'	40°15'					
18	31°5' 51°41'	32°2' 50°32'	33°4' 49°18'	34°8' 48°2'	35°15' 46°41'	36°28' 45°16'	37°45' 43°45'	39°5' 42°11'	40°31'						
19	33°36' 50°18'	33°36' 49°8'	34°38' 47°54'	35°49' 46°36'	36°53' 45°15'	38°6' 43°50'	39°24' 42°20'	40°45'							
20	34°5' 48°57'	35°6' 47°46'	36°8' 46°32'	37°16' 45°14'	38°26' 43°52'	39°39' 42°27'	40°57'								
21	35°31' 47°39'	36°32' 46°28'	37°37' 45°13'	38°44' 43°56'	39°54' 42°34'	41°8'									
22	36°52' 46°24'	37°55' 45°13'	39°0' 43°58'	40°8' 42°40'	41°19'										
23	38°12' 45°12'	39°15' 44°1'	40°20' 42°46'	41°28'											
24	39°29' 44°3'	40°32' 42°52'	41°38'												
25	40°43' 42°57'	41°46'													
26	41°53'														

For Bevel Gears with axes at right angles.

Angle for gear above, for pinion below.

Table for Selecting Cutters for Bevel Gears.

SELECTION OF CUTTERS.

The following tables are for use in selecting cutters for cutting bevel gears. The various numbers of teeth in gear and pinion are given and at the intersection of the two columns will be found the numbers of the cutters required.

EXAMPLE.—Required cutters for a pair of bevel gears, 8 pitch; gear 24 teeth, pinion 12 teeth.

In column at left of table, page 86, will be found 24 teeth and in column at top 12 teeth; at the intersection of these two columns will be found the numbers of the cutters, in this case No. 3 for the gear and No. 8 for the pinion.

CUTTERS FOR USE IN CUTTING BEVEL GEARS.

PINION.

	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
12	7-7																		
13	6-7	6-6																	
14	5-7	6-6	6-6																
15	5-7	5-6	5-6	5-5															
16	4-7	5-7	5-6	5-6	5-5														
17	4-7	4-7	4-6	5-6	5-5	5-5													
18	4-7	4-7	4-6	4-6	4-5	4-5	5-5												
19	3-7	4-7	4-6	4-6	4-6	4-5	4-5	4-4											
20	3-7	3-7	4-6	4-6	4-6	4-5	4-5	4-4	4-4										
21	3-8	3-7	3-7	3-6	4-6	4-5	4-5	4-5	4-4	4-4									
22	3-8	3-7	3-7	3-6	3-6	3-5	4-5	4-5	4-4	4-4	4-4								
23	3-8	3-7	3-7	3-6	3-6	3-5	3-5	3-5	3-4	4-4	4-4	4-4							
24	3-8	3-7	3-7	3-6	3-6	3-6	3-5	3-5	3-4	3-4	3-4	4-4	4-4						
25	2-8	2-7	3-7	3-6	3-6	3-6	3-5	3-5	3-5	3-4	3-4	3-4	4-4	3-3					
26	2-8	2-7	3-7	3-6	3-6	3-6	3-5	3-5	3-5	3-4	3-4	3-4	3-4	3-3	3-3				
27	2-8	2-7	2-7	2-6	3-6	3-6	3-5	3-5	3-5	3-4	3-4	3-4	3-4	3-4	3-3	3-3			
28	2-8	2-7	2-7	2-6	2-6	3-6	3-5	3-5	3-5	3-4	3-4	3-4	3-4	3-4	3-3	3-3	3-3		
29	2-8	2-7	2-7	2-7	2-6	2-6	3-5	3-5	3-5	3-4	3-4	3-4	3-4	3-4	3-3	3-3	3-3	3-3	
30	2-8	2-7	2-7	2-7	2-6	2-6	2-5	2-5	3-5	3-5	3-4	3-4	3-4	3-4	3-4	3-3	3-3	3-3	3-3
31	2-8	2-7	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	3-4	3-4	3-4	3-4	3-4	3-3	3-3	3-3	3-3
32	2-8	2-7	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-4	2-4	3-4	3-4	3-4	3-3	3-3	3-3	3-3
33	2-8	2-8	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-4	2-4	2-4	3-4	3-4	3-4	3-3	3-3	3-3
34	2-8	2-8	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	3-4	3-3	3-3	3-3
35	2-8	2-8	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-4	2-3	3-3
36	2-8	2-8	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-3	2-3
37	2-8	2-8	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-3	2-3
38	2-8	2-8	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-3	2-3
39	2-8	2-8	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-3	2-3
40	1-8	2-8	2-7	2-7	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-3	2-3
41	1-8	1-8	2-7	2-7	2-6	2-6	2-6	2-6	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-3	2-3
42	1-8	1-8	2-7	2-7	2-6	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-3	2-3
43	1-8	1-8	1-7	2-7	2-6	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-3
44	1-8	1-8	1-7	1-7	2-6	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4	2-3
45	1-8	1-8	1-7	1-7	1-6	2-6	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-3
46	1-8	1-8	1-7	1-7	1-7	2-6	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-3
47	1-8	1-8	1-7	1-7	1-7	1-6	2-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-3
48	1-8	1-8	1-7	1-7	1-7	1-6	1-6	2-6	2-6	2-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-3
49	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	2-6	2-6	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-3
50	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	2-6	2-6	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-3
51	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	2-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4
52	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	2-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4
53	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	2-5	2-4	2-4	2-4	2-4	2-4	2-4
54	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	2-4	2-4	2-4	2-4	2-4	2-4
55	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	2-4	2-4	2-4	2-4	2-4

For Bevel Gears with axes at right angles.

Number of cutter for gear given first, followed by number for pinion.

CUTTERS FOR USE IN CUTTING BEVEL GEARS.

(Continued.)

PINION.

	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
56	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	2-4	2-4	2-4	2-4	2-4
57	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	2-4	2-4	2-4	2-4
58	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	2-4	2-4	2-4
59	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	2-4	2-4
60	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	2-4
61	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
62	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-
63	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
64	1-8	1-8	1-7	1-7	1-6	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
65	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
66	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
67	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
68	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
69	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
70	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
71	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
72	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
73	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
74	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
75	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
76	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
77	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
78	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
79	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
80	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
81	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
82	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
83	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
84	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
85	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
86	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
87	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
88	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
89	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
90	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
91	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
92	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
93	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
94	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
95	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
96	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
97	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
98	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
99	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4
100	1-8	1-8	1-7	1-7	1-7	1-6	1-6	1-6	1-6	1-5	1-5	1-5	1-5	1-4	1-4	1-4	1-4	1-4	1-4

For Bevel Gears with axes at right angles.

Number of cutter for gear given first, followed by number for pinion.



Table for the Solution of Right Angled Triangles.

SOLUTION OF TRIANGLES BY NATURAL LINES.

PARTS GIVEN.	PARTS TO BE FOUND.				
	ANGLE.	ADJ. SIDE.	OPP. SIDE.	HYPOTH.	OPP. ANG.
Opp. and Hyp.	$\text{Sin.} = \frac{\text{Opp.}}{\text{Hyp.}}$	$\sqrt{\text{Hyp.}^2 - \text{Opp.}^2}$			$\text{Cos.} = \frac{\text{Opp.}}{\text{Hyp.}}$
Opp. and Adj.	$\text{Tan.} = \frac{\text{Opp.}}{\text{Adj.}}$			$\sqrt{\text{Opp.}^2 + \text{Adj.}^2}$	$\text{Cot.} = \frac{\text{Opp.}}{\text{Adj.}}$
Adj. and Hyp.	$\text{Cos.} = \frac{\text{Adj.}}{\text{Hyp.}}$		$\sqrt{\text{Hyp.}^2 - \text{Adj.}^2}$		$\text{Sin.} = \frac{\text{Adj.}}{\text{Hyp.}}$
Ang. and Opp.		$\text{Opp.} \times \text{Cot.}$		$\text{Opp.} \div \text{Sin.}$	$90^\circ - \text{Ang.}$
Ang. and Adj.			$\text{Adj.} \times \text{Tang.}$	$\text{Adj.} \div \text{Cos.}$	$90^\circ - \text{Ang.}$
Ang. and Hyp.		$\text{Hyp.} \times \text{Cos.}$	$\text{Hyp.} \times \text{Sin.}$		$90^\circ - \text{Ang.}$

ABBREVIATIONS USED.

Opp. = Opposite side.
Adj. = Adjacent side.
Hyp. = Hypothenuse.
Ang. = Angle.

Sin. = Sine.
Tan. = Tangent.
Cos. = Cosine.
Cot. = Cotangent.



Natural Sines and Cosines
Natural Tangents and Cotangents

COURTESY OF
THE INTERNATIONAL CORRESPONDENCE SCHOOLS,
SCRANTON, PA.

NATURAL SINES AND COSINES

/	0°		1°		2°		3°		4°		/
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.00000	1.	.01745	.99985	.03490	.99939	.05234	.99863	.06976	.99756	60
1	.00029	1.	.01774	.99984	.03519	.99938	.05263	.99861	.07005	.99754	59
2	.00058	1.	.01803	.99984	.03548	.99937	.05292	.99860	.07034	.99752	58
3	.00087	1.	.01832	.99983	.03577	.99936	.05321	.99858	.07063	.99750	57
4	.00116	1.	.01862	.99983	.03606	.99935	.05350	.99857	.07092	.99748	56
5	.00145	1.	.01891	.99982	.03635	.99934	.05379	.99855	.07121	.99746	55
6	.00175	1.	.01920	.99982	.03664	.99933	.05408	.99854	.07150	.99744	54
7	.00204	1.	.01949	.99981	.03693	.99932	.05437	.99852	.07179	.99742	53
8	.00233	1.	.01978	.99980	.03723	.99931	.05466	.99851	.07208	.99740	52
9	.00262	1.	.02007	.99980	.03752	.99930	.05495	.99849	.07237	.99738	51
10	.00291	1.	.02036	.99979	.03781	.99929	.05524	.99847	.07266	.99736	50
11	.00320	.99999	.02065	.99979	.03810	.99927	.05553	.99846	.07295	.99734	49
12	.00349	.99999	.02094	.99978	.03839	.99926	.05582	.99844	.07324	.99731	48
13	.00378	.99999	.02123	.99977	.03868	.99925	.05611	.99842	.07353	.99729	47
14	.00407	.99999	.02152	.99977	.03897	.99924	.05640	.99841	.07382	.99727	46
15	.00436	.99999	.02181	.99976	.03926	.99923	.05669	.99839	.07411	.99725	45
16	.00465	.99999	.02211	.99976	.03955	.99922	.05698	.99838	.07440	.99723	44
17	.00495	.99999	.02240	.99975	.03984	.99921	.05727	.99836	.07469	.99721	43
18	.00524	.99999	.02269	.99974	.04013	.99919	.05756	.99834	.07498	.99719	42
19	.00553	.99998	.02298	.99974	.04042	.99918	.05785	.99833	.07527	.99716	41
20	.00582	.99998	.02327	.99973	.04071	.99917	.05814	.99831	.07556	.99714	40
21	.00611	.99998	.02356	.99972	.04100	.99916	.05844	.99829	.07585	.99712	39
22	.00640	.99998	.02385	.99972	.04129	.99915	.05873	.99827	.07614	.99710	38
23	.00669	.99998	.02414	.99971	.04159	.99913	.05902	.99826	.07643	.99708	37
24	.00698	.99998	.02443	.99970	.04188	.99912	.05931	.99824	.07672	.99705	36
25	.00727	.99997	.02472	.99969	.04217	.99911	.05960	.99822	.07701	.99703	35
26	.00756	.99997	.02501	.99969	.04246	.99910	.05989	.99821	.07730	.99701	34
27	.00785	.99997	.02530	.99968	.04275	.99909	.06018	.99819	.07759	.99699	33
28	.00814	.99997	.02559	.99967	.04304	.99907	.06047	.99817	.07788	.99696	32
29	.00843	.99996	.02588	.99966	.04333	.99906	.06076	.99815	.07817	.99694	31
30	.00873	.99996	.02618	.99966	.04362	.99905	.06105	.99813	.07846	.99692	30
31	.00902	.99996	.02647	.99965	.04391	.99904	.06134	.99812	.07875	.99690	29
32	.00931	.99996	.02676	.99964	.04420	.99902	.06163	.99810	.07904	.99687	28
33	.00960	.99995	.02705	.99963	.04449	.99901	.06192	.99808	.07933	.99685	27
34	.00989	.99995	.02734	.99963	.04478	.99900	.06221	.99806	.07962	.99683	26
35	.01018	.99995	.02763	.99962	.04507	.99898	.06250	.99804	.07991	.99680	25
36	.01047	.99995	.02792	.99961	.04536	.99897	.06279	.99803	.08020	.99678	24
37	.01076	.99994	.02821	.99960	.04565	.99896	.06308	.99801	.08049	.99676	23
38	.01105	.99994	.02850	.99959	.04594	.99894	.06337	.99799	.08078	.99673	22
39	.01134	.99994	.02879	.99959	.04623	.99893	.06366	.99797	.08107	.99671	21
40	.01164	.99993	.02908	.99958	.04653	.99892	.06395	.99795	.08136	.99668	20
41	.01193	.99993	.02938	.99957	.04682	.99890	.06424	.99793	.08165	.99666	19
42	.01222	.99993	.02967	.99956	.04711	.99889	.06453	.99792	.08194	.99664	18
43	.01251	.99992	.02996	.99955	.04740	.99888	.06482	.99790	.08223	.99661	17
44	.01280	.99992	.03025	.99954	.04769	.99886	.06511	.99788	.08252	.99659	16
45	.01309	.99991	.03054	.99953	.04798	.99885	.06540	.99786	.08281	.99657	15
46	.01338	.99991	.03083	.99952	.04827	.99883	.06569	.99784	.08310	.99654	14
47	.01367	.99991	.03112	.99952	.04856	.99882	.06598	.99782	.08339	.99652	13
48	.01396	.99990	.03141	.99951	.04885	.99881	.06627	.99780	.08368	.99649	12
49	.01425	.99990	.03170	.99950	.04914	.99879	.06656	.99778	.08397	.99647	11
50	.01454	.99989	.03199	.99949	.04943	.99878	.06685	.99776	.08426	.99644	10
51	.01483	.99989	.03228	.99948	.04972	.99876	.06714	.99774	.08455	.99642	9
52	.01513	.99989	.03257	.99947	.05001	.99875	.06743	.99772	.08484	.99639	8
53	.01542	.99988	.03286	.99946	.05030	.99873	.06773	.99770	.08513	.99637	7
54	.01571	.99988	.03316	.99945	.05059	.99872	.06802	.99768	.08542	.99635	6
55	.01600	.99987	.03345	.99944	.05088	.99870	.06831	.99766	.08571	.99632	5
56	.01629	.99987	.03374	.99943	.05117	.99869	.06860	.99764	.08600	.99630	4
57	.01658	.99986	.03403	.99942	.05146	.99867	.06889	.99762	.08629	.99627	3
58	.01687	.99986	.03432	.99941	.05175	.99866	.06918	.99760	.08658	.99625	2
59	.01716	.99985	.03461	.99940	.05205	.99864	.06947	.99758	.08687	.99622	1
60	.01745	.99985	.03490	.99939	.05234	.99863	.06976	.99756	.08716	.99619	0
/	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	/
	89°		88°		87°		86°		85°		

/	5°		6°		7°		8°		9°		/
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.08716	.99619	.10453	.99452	.12187	.99255	.13917	.99027	.15643	.98769	60
1	.08745	.99617	.10482	.99449	.12216	.99251	.13946	.99023	.15672	.98764	59
2	.08774	.99614	.10511	.99446	.12245	.99248	.13975	.99019	.15701	.98760	58
3	.08803	.99612	.10540	.99443	.12274	.99244	.14004	.99015	.15730	.98755	57
4	.08831	.99609	.10569	.99440	.12302	.99240	.14033	.99011	.15758	.98751	56
5	.08860	.99607	.10597	.99437	.12331	.99237	.14061	.99006	.15787	.98746	55
6	.08889	.99604	.10626	.99434	.12360	.99233	.14090	.99002	.15816	.98741	54
7	.08918	.99602	.10655	.99431	.12389	.99230	.14119	.98998	.15845	.98737	53
8	.08947	.99599	.10684	.99428	.12418	.99226	.14148	.98994	.15873	.98732	52
9	.08976	.99596	.10713	.99424	.12447	.99222	.14177	.98990	.15902	.98728	51
10	.09005	.99594	.10742	.99421	.12476	.99219	.14205	.98986	.15931	.98723	50
11	.09034	.99591	.10771	.99418	.12504	.99215	.14234	.98982	.15959	.98718	49
12	.09063	.99588	.10800	.99415	.12533	.99211	.14263	.98978	.15988	.98714	48
13	.09092	.99586	.10829	.99412	.12562	.99208	.14292	.98973	.16017	.98709	47
14	.09121	.99583	.10858	.99409	.12591	.99204	.14320	.98969	.16046	.98704	46
15	.09150	.99580	.10887	.99406	.12620	.99200	.14349	.98965	.16074	.98700	45
16	.09179	.99578	.10916	.99402	.12649	.99197	.14378	.98961	.16103	.98695	44
17	.09208	.99575	.10945	.99399	.12678	.99193	.14407	.98957	.16132	.98690	43
18	.09237	.99572	.10974	.99396	.12706	.99189	.14436	.98953	.16160	.98686	42
19	.09266	.99570	.11002	.99393	.12735	.99186	.14464	.98948	.16189	.98681	41
20	.09295	.99567	.11031	.99390	.12764	.99182	.14493	.98944	.16218	.98676	40
21	.09324	.99564	.11060	.99386	.12793	.99178	.14522	.98940	.16246	.98671	39
22	.09353	.99562	.11089	.99383	.12822	.99175	.14551	.98936	.16275	.98667	38
23	.09382	.99559	.11118	.99380	.12851	.99171	.14580	.98931	.16304	.98662	37
24	.09411	.99556	.11147	.99377	.12880	.99167	.14608	.98927	.16333	.98657	36
25	.09440	.99553	.11176	.99374	.12908	.99163	.14637	.98923	.16361	.98652	35
26	.09469	.99551	.11205	.99370	.12937	.99160	.14666	.98919	.16390	.98648	34
27	.09498	.99548	.11234	.99367	.12966	.99156	.14695	.98914	.16419	.98643	33
28	.09527	.99545	.11263	.99364	.12995	.99152	.14723	.98910	.16447	.98638	32
29	.09556	.99542	.11291	.99360	.13024	.99148	.14752	.98906	.16476	.98633	31
30	.09585	.99540	.11320	.99357	.13053	.99144	.14781	.98902	.16505	.98629	30
31	.09614	.99537	.11349	.99354	.13081	.99141	.14810	.98897	.16533	.98624	29
32	.09642	.99534	.11378	.99351	.13110	.99137	.14838	.98893	.16562	.98619	28
33	.09671										

NATURAL SINES AND COSINES'

°	15°		16°		17°		18°		19°		°
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.25882	.96593	.27564	.96126	.29237	.95630	.30902	.95106	.32557	.94552	60
1	.25910	.96585	.27592	.96118	.29265	.95622	.30929	.95097	.32584	.94542	59
2	.25938	.96578	.27620	.96110	.29293	.95613	.30957	.95088	.32612	.94533	58
3	.25966	.96570	.27648	.96102	.29321	.95605	.30985	.95079	.32639	.94523	57
4	.25994	.96562	.27676	.96094	.29348	.95596	.31012	.95070	.32667	.94514	56
5	.26022	.96555	.27704	.96086	.29376	.95588	.31040	.95061	.32694	.94504	55
6	.26050	.96547	.27731	.96078	.29404	.95579	.31068	.95052	.32722	.94495	54
7	.26079	.96540	.27759	.96070	.29432	.95571	.31095	.95043	.32749	.94485	53
8	.26107	.96532	.27787	.96062	.29460	.95562	.31123	.95033	.32777	.94476	52
9	.26135	.96524	.27815	.96054	.29487	.95554	.31151	.95024	.32804	.94466	51
10	.26163	.96517	.27843	.96046	.29515	.95545	.31178	.95015	.32832	.94457	50
11	.26191	.96509	.27871	.96037	.29543	.95536	.31206	.95006	.32859	.94447	49
12	.26219	.96502	.27899	.96029	.29571	.95528	.31233	.94997	.32887	.94438	48
13	.26247	.96494	.27927	.96021	.29599	.95519	.31261	.94988	.32914	.94428	47
14	.26275	.96486	.27955	.96013	.29626	.95511	.31289	.94979	.32942	.94418	46
15	.26303	.96479	.27983	.96005	.29654	.95502	.31316	.94970	.32969	.94409	45
16	.26331	.96471	.28011	.95997	.29682	.95493	.31344	.94961	.32997	.94399	44
17	.26359	.96463	.28039	.95989	.29710	.95485	.31372	.94952	.33024	.94390	43
18	.26387	.96456	.28067	.95981	.29737	.95476	.31399	.94943	.33051	.94380	42
19	.26415	.96448	.28095	.95972	.29765	.95467	.31427	.94933	.33079	.94370	41
20	.26443	.96440	.28123	.95964	.29793	.95459	.31454	.94924	.33106	.94361	40
21	.26471	.96433	.28150	.95956	.29821	.95450	.31482	.94915	.33134	.94351	39
22	.26500	.96425	.28178	.95948	.29849	.95441	.31510	.94906	.33161	.94342	38
23	.26528	.96417	.28206	.95940	.29876	.95433	.31537	.94897	.33189	.94332	37
24	.26556	.96410	.28234	.95931	.29904	.95424	.31565	.94888	.33216	.94322	36
25	.26584	.96402	.28262	.95923	.29932	.95415	.31593	.94878	.33244	.94313	35
26	.26612	.96394	.28290	.95915	.29960	.95407	.31620	.94869	.33271	.94303	34
27	.26640	.96386	.28318	.95907	.29987	.95398	.31648	.94860	.33298	.94293	33
28	.26668	.96379	.28346	.95898	.30015	.95389	.31675	.94851	.33326	.94284	32
29	.26696	.96371	.28374	.95890	.30043	.95380	.31703	.94842	.33353	.94274	31
30	.26724	.96363	.28402	.95882	.30071	.95372	.31730	.94832	.33381	.94264	30
31	.26752	.96355	.28429	.95874	.30098	.95363	.31758	.94823	.33408	.94254	29
32	.26780	.96347	.28457	.95865	.30126	.95354	.31786	.94814	.33436	.94245	28
33	.26808	.96340	.28485	.95857	.30154	.95345	.31813	.94805	.33463	.94235	27
34	.26836	.96332	.28513	.95849	.30182	.95337	.31841	.94795	.33490	.94225	26
35	.26864	.96324	.28541	.95841	.30209	.95328	.31868	.94786	.33518	.94215	25
36	.26892	.96316	.28569	.95832	.30237	.95319	.31896	.94777	.33545	.94206	24
37	.26920	.96308	.28597	.95824	.30265	.95310	.31923	.94768	.33573	.94196	23
38	.26948	.96301	.28625	.95816	.30292	.95301	.31951	.94759	.33600	.94186	22
39	.26976	.96293	.28652	.95807	.30320	.95293	.31979	.94749	.33627	.94176	21
40	.27004	.96285	.28680	.95799	.30348	.95284	.32006	.94740	.33655	.94167	20
41	.27032	.96277	.28708	.95791	.30376	.95275	.32034	.94730	.33682	.94157	19
42	.27060	.96269	.28736	.95782	.30403	.95266	.32061	.94721	.33710	.94147	18
43	.27088	.96261	.28764	.95774	.30431	.95257	.32089	.94712	.33737	.94137	17
44	.27116	.96253	.28792	.95766	.30459	.95248	.32116	.94702	.33764	.94127	16
45	.27144	.96246	.28820	.95757	.30486	.95240	.32144	.94693	.33792	.94118	15
46	.27172	.96238	.28847	.95749	.30514	.95231	.32171	.94684	.33819	.94108	14
47	.27200	.96230	.28875	.95740	.30542	.95222	.32199	.94674	.33846	.94098	13
48	.27228	.96222	.28903	.95732	.30570	.95213	.32227	.94665	.33874	.94088	12
49	.27256	.96214	.28931	.95724	.30597	.95204	.32254	.94656	.33901	.94078	11
50	.27284	.96206	.28959	.95715	.30625	.95195	.32282	.94646	.33929	.94068	10
51	.27312	.96198	.28987	.95707	.30653	.95186	.32309	.94637	.33956	.94058	9
52	.27340	.96190	.29015	.95698	.30680	.95177	.32337	.94627	.33983	.94049	8
53	.27368	.96182	.29042	.95690	.30708	.95168	.32364	.94618	.34011	.94039	7
54	.27396	.96174	.29070	.95681	.30736	.95159	.32392	.94609	.34038	.94029	6
55	.27424	.96166	.29098	.95673	.30763	.95150	.32419	.94599	.34065	.94019	5
56	.27452	.96158	.29126	.95664	.30791	.95142	.32447	.94590	.34093	.94009	4
57	.27480	.96150	.29154	.95656	.30819	.95133	.32474	.94580	.34120	.93999	3
58	.27508	.96142	.29182	.95647	.30846	.95124	.32502	.94571	.34147	.93989	2
59	.27536	.96134	.29210	.95639	.30874	.95115	.32529	.94561	.34175	.93979	1
60	.27564	.96126	.29237	.95630	.30902	.95106	.32557	.94552	.34202	.93969	0
°	15°		16°		17°		18°		19°		°
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
74°			73°		72°		71°		70°		

NATURAL SINES AND COSINES

/	20°		21°		22°		23°		24°		/
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.34202	.93969	.35837	.93358	.37461	.92718	.39073	.92050	.40674	.91355	60
1	.34229	.93959	.35864	.93348	.37488	.92707	.39100	.92039	.40700	.91343	59
2	.34257	.93949	.35891	.93337	.37515	.92697	.39127	.92028	.40727	.91331	58
3	.34284	.93939	.35918	.93327	.37542	.92686	.39153	.92016	.40753	.91319	57
4	.34311	.93929	.35945	.93316	.37569	.92675	.39180	.92005	.40780	.91307	56
5	.34339	.93919	.35973	.93306	.37595	.92664	.39207	.91994	.40806	.91295	55
6	.34366	.93909	.36000	.93295	.37622	.92653	.39234	.91982	.40833	.91283	54
7	.34393	.93899	.36027	.93285	.37649	.92642	.39260	.91971	.40860	.91272	53
8	.34421	.93889	.36054	.93274	.37676	.92631	.39287	.91959	.40886	.91260	52
9	.34448	.93879	.36081	.93264	.37703	.92620	.39314	.91948	.40913	.91248	51
10	.34475	.93869	.36108	.93253	.37730	.92609	.39341	.91936	.40939	.91236	50
11	.34503	.93859	.36135	.93243	.37757	.92598	.39367	.91925	.40966	.91224	49
12	.34530	.93849	.36162	.93232	.37784	.92587	.39394	.91914	.40992	.91212	48
13	.34557	.93839	.36190	.93222	.37811	.92576	.39421	.91902	.41019	.91200	47
14	.34584	.93829	.36217	.93211	.37838	.92565	.39448	.91891	.41045	.91188	46
15	.34612	.93819	.36244	.93201	.37865	.92554	.39474	.91879	.41072	.91176	45
16	.34639	.93809	.36271	.93190	.37892	.92543	.39501	.91868	.41098	.91164	44
17	.34666	.93799	.36298	.93180	.37919	.92532	.39528	.91856	.41125	.91152	43
18	.34694	.93789	.36325	.93169	.37946	.92521	.39555	.91845	.41151	.91140	42
19	.34721	.93779	.36352	.93159	.37973	.92510	.39581	.91833	.41178	.91128	41
20	.34748	.93769	.36379	.93148	.37999	.92499	.39608	.91822	.41204	.91116	40
21	.34775	.93759	.36406	.93137	.38026	.92488	.39635	.91810	.41231	.91104	39
22	.34803	.93748	.36434	.93127	.38053	.92477	.39661	.91799	.41257	.91092	38
23	.34830	.93738	.36461	.93116	.38080	.92466	.39688	.91787	.41284	.91080	37
24	.34857	.93728	.36488	.93106	.38107	.92455	.39715	.91775	.41310	.91068	36
25	.34884	.93718	.36515	.93095	.38134	.92444	.39741	.91764	.41337	.91056	35
26	.34912	.93708	.36542	.93084	.38161	.92432	.39768	.91752	.41363	.91044	34
27	.34939	.93698	.36569	.93074	.38188	.92421	.39795	.91741	.41390	.91032	33
28	.34966	.93688	.36596	.93063	.38215	.92410	.39822	.91729	.41416	.91020	32
29	.34993	.93677	.36623	.93052	.38241	.92399	.39848	.91718	.41443	.91008	31
30	.35021	.93667	.36650	.93042	.38268	.92388	.39875	.91706	.41469	.90996	30
31	.35048	.93657	.36677	.93031	.38295	.92377	.39902	.91694	.41496	.90984	29
32	.35075	.93647	.36704	.93020	.38322	.92366	.39928	.91683	.41522	.90972	28
33	.35102	.93637	.36731	.93010	.38349	.92355	.39955	.91671	.41549	.90960	27
34	.35130	.93626	.36758	.92999	.38376	.92343	.39982	.91660	.41575	.90948	26
35	.35157	.93616	.36785	.92988	.38403	.92332	.40008	.91648	.41602	.90936	25
36	.35184	.93606	.36812	.92978	.38430	.92321	.40035	.91636	.41628	.90924	24
37	.35211	.93596	.36839	.92967	.38456	.92310	.40062	.91625	.41655	.90911	23
38	.35239	.93585	.36867	.92956	.38483	.92299	.40088	.91613	.41681	.90899	22
39	.35266	.93575	.36894	.92945	.38510	.92287	.40115	.91601	.41707	.90887	21
40	.35293	.93565	.36921	.92935	.38537	.92276	.40141	.91590	.41734	.90875	20
41	.35320	.93555	.36948	.92924	.38564	.92265	.40168	.91578	.41760	.90863	19
42	.35347	.93544	.36975	.92913	.38591	.92254	.40195	.91566	.41787	.90851	18
43	.35375	.93534	.37002	.92902	.38617	.92243	.40221	.91555	.41813	.90839	17
44	.35402	.93524	.37029	.92892	.38644	.92231	.40248	.91543	.41840	.90826	16
45	.35429	.93514	.37056	.92881	.38671	.92220	.40275	.91531	.41866	.90814	15
46	.35456	.93503	.37083	.92870	.38698	.92209	.40301	.91519	.41892	.90802	14
47	.35484	.93493	.37110	.92859	.38725	.92198	.40328	.91508	.41919	.90790	13
48	.35511	.93483	.37137	.92849	.38752	.92186	.40355	.91496	.41945	.90778	12
49	.35538	.93472	.37164	.92838	.38778	.92175	.40381	.91484	.41972	.90766	11
50	.35565	.93462	.37191	.92827	.38805	.92164	.40408	.91472	.41998	.90753	10
51	.35592	.93452	.37218	.92816	.38832	.92152	.40434	.91461	.42024	.90741	9
52	.35619	.93441	.37245	.92805	.38859	.92141	.40461	.91449	.42051	.90729	8
53	.35647	.93431	.37272	.92794	.38886	.92130	.40488	.91437	.42077	.90717	7
54	.35674	.93420	.37299	.92784	.38912	.92119	.40514	.91425	.42104	.90704	6
55	.35701	.93410	.37326	.92773	.38939	.92107	.40541	.91414	.42130	.90692	5
56	.35728	.93400	.37353	.92762	.38966	.92096	.40567	.91402	.42156	.90680	4
57	.35755	.93389	.37380	.92751	.38993	.92085	.40594	.91390	.42183	.90668	3
58	.35782	.93379	.37407	.92740	.39020	.92073	.40621	.91378	.42209	.90655	2
59	.35810	.93368	.37434	.92729	.39046	.92062	.40647	.91366	.42235	.90643	1
60	.35837	.93358	.37461	.92718	.39073	.92050	.40674	.91355	.42262	.90631	0
/	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	/
	69°		68°		67°		66°		65°		

NATURAL TANGENTS AND COTANGENTS

/	0°		1°		2°		3°		4°		/
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.00000	Infinite	.01746	57.2900	.03492	28.6363	.05241	19.0811	.06993	14.3007	60
1	.00029	3437.75	.01775	56.3506	.03521	28.3994	.05270	18.9755	.07022	14.2411	59
2	.00058	1718.87	.01804	55.4451	.03550	28.1664	.05299	18.8711	.07051	14.1821	58
3	.00087	1145.92	.01833	54.5613	.03579	27.9372	.05328	18.7678	.07080	14.1235	57
4	.00116	859.436	.01862	53.7086	.03599	27.7117	.05357	18.6656	.07110	14.0655	56
5	.00145	687.549	.01891	52.8821	.03638	27.4899	.05387	18.5645	.07139	14.0079	55
6	.00175	572.957	.01920	52.0807	.03667	27.2715	.05416	18.4645	.07168	13.9507	54
7	.00204	491.106	.01949	51.3032	.03696	27.0560	.05445	18.3655	.07197	13.8940	53
8	.00233	429.718	.01978	50.5485	.03725	26.8450	.05474	18.2677	.07227	13.8378	52
9	.00262	381.971	.02007	49.8157	.03754	26.6367	.05503	18.1708	.07256	13.7821	51
10	.00291	343.774	.02036	49.1039	.03783	26.4316	.05532	18.0750	.07285	13.7267	50
11	.00320	312.521	.02066	48.4121	.03812	26.2296	.05562	17.9802	.07314	13.6719	49
12	.00349	286.478	.02095	47.7395	.03842	26.0307	.05591	17.8863	.07344	13.6174	48
13	.00378	264.441	.02124	47.0853	.03871	25.8348	.05620	17.7934	.07373	13.5634	47
14	.00407	245.552	.02153	46.4489	.03900	25.6418	.05649	17.7015	.07402	13.5098	46
15	.00436	229.182	.02182	45.8294	.03929	25.4517	.05678	17.6106	.07431	13.4566	45
16	.00465	214.858	.02211	45.2261	.03958	25.2644	.05708	17.5205	.07461	13.4039	44
17	.00494	202.219	.02240	44.6386	.03987	25.0798	.05737	17.4314	.07490	13.3515	43
18	.00523	190.984	.02269	44.0661	.04016	24.8978	.05766	17.3432	.07519	13.2996	42
19	.00553	180.932	.02298	43.5081	.04046	24.7185	.05795	17.2558	.07548	13.2480	41
20	.00582	171.885	.02328	42.9644	.04075	24.5418	.05824	17.1693	.07578	13.1969	40
21	.00611	163.700	.02357	42.4335	.04104	24.3675	.05854	17.0837	.07607	13.1461	39
22	.00640	156.259	.02386	41.9158	.04133	24.1957	.05883	16.9990	.07636	13.0958	38
23	.00669	149.465	.02415	41.4106	.04162	24.0263	.05912	16.9150	.07665	13.0458	37
24	.00698	143.237	.02444	40.9174	.04191	23.8593	.05941	16.8319	.07695	12.9962	36
25	.00727	137.507	.02473	40.4358	.04220	23.6945	.05970	16.7496	.07724	12.9469	35
26	.00756	132.219	.02502	39.9655	.04250	23.5331	.05999	16.6681	.07753	12.8981	34
27	.00785	127.321	.02531	39.5059	.04279	23.3718	.06029	16.5874	.07782	12.8496	33
28	.00815	122.774	.02560	39.0568	.04308	23.2137	.06058	16.5075	.07812	12.8014	32
29	.00844	118.540	.02589	38.6177	.04337	23.0577	.06087	16.4283	.07841	12.7536	31
30	.00873	114.589	.02619	38.1895	.04366	22.9038	.06116	16.3499	.07870	12.7062	30
31	.00902	110.892	.02648	37.7686	.04395	22.7519	.06145	16.2722	.07899	12.6591	29
32	.00931	107.426	.02677	37.3579	.04424	22.6020	.06175	16.1952	.07929	12.6124	28
33	.00960	104.171	.02706	36.9560	.04454	22.4541	.06204	16.1190	.07958	12.5660	27
34	.00989	101.107	.02735	36.5627	.04483	22.3081	.06233	16.0435	.07987	12.5199	26
35	.01018	98.2179	.02764	36.1776	.04512	22.1640	.06262	15.9687	.08017	12.4742	25
36	.01047	95.4895	.02793	35.8006	.04541	22.0217	.06291	15.8945	.08046	12.4288	24
37	.01076	92.9085	.02822	35.4313	.04570	21.8813	.06321	15.8211	.08075	12.3838	23
38	.01105	90.4633	.02851	35.0695	.04599	21.7426	.06350	15.7483	.08104	12.3390	22
39	.01135	88.1436	.02881	34.7151	.04628	21.6056	.06379	15.6762	.08134	12.2946	21
40	.01164	85.9398	.02910	34.3678	.04658	21.4704	.06408	15.6048	.08163	12.2505	20
41	.01193	83.8435	.02939	34.0273	.04687	21.3369	.06437	15.5340	.08192	12.2067	19
42	.01222	81.8470	.02968	33.6935	.04716	21.2049	.06467	15.4638	.08221	12.1632	18
43	.01251	79.9434	.02997	33.3662	.04745	21.0747	.06496	15.3943	.08251	12.1201	17
44	.01280	78.1263	.03026	33.0452	.04774	20.9460	.06525	15.3254	.08280	12.0772	16
45	.01309	76.3900	.03055	32.7303	.04803	20.8188	.06554	15.2571	.08309	12.0346	15
46	.01338	74.7292	.03084	32.4213	.04833	20.6932	.06584	15.1893	.08339	11.9923	14
47	.01367	73.1300	.03114	32.1181	.04862	20.5691	.06613	15.1222	.08368	11.9504	13
48	.01396	71.6151	.03143	31.8205	.04891	20.4465	.06642	15.0557	.08397	11.9087	12
49	.01425	70.1533	.03172	31.5284	.04920	20.3253	.06671	14.9898	.08427	11.8673	11
50	.01455	68.7501	.03201	31.2416	.04949	20.2056	.06700	14.9244	.08456	11.8262	10
51	.01484	67.4019	.03230	30.9599	.04978	20.0872	.06730	14.8596	.08485	11.7853	9
52	.01513	66.1035	.03259	30.6833	.05007	19.9702	.06759	14.7954	.08514	11.7454	8
53	.01542	64.8580	.03288	30.4116	.05037	19.8546	.06788	14.7317	.08544	11.7045	7
54	.01571	63.6567	.03317	30.1446	.05066	19.7403	.06817	14.6685	.08573	11.6645	6
55	.01600	62.4992	.03346	29.8823	.05095	19.6273	.06847	14.6059	.08602	11.6248	5
56	.01629	61.3829	.03376	29.6245	.05124	19.5156	.06876	14.5438	.08632	11.5853	4
57	.01658	60.3058	.03405	29.3711	.05153	19.4051	.06905	14.4823	.08661	11.5461	3
58	.01687	59.2659	.03434	29.1220	.05182	19.2959	.06934	14.4212	.08690	11.5072	2
59	.01716	58.2612	.03463	28.8771	.05212	19.1879	.06963	14.3607	.08720	11.4685	1
60	.01746	57.2900	.03492	28.6363	.05241	19.0811	.06993	14.3007	.08749	11.4301	0
/	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	/
	89°		88°		87°		86°		85°		

NATURAL TANGENTS AND COTANGENTS

/	5°		6°		7°		8°		9°		/
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.08749	11.4301	.10510	9.51436	.12278	8.14435	.14054	7.11537	.15838	6.31375	60
1	.08778	11.3919	.10540	9.48781	.12308	8.12481	.14084	7.10038	.15868	6.30189	59
2	.08807	11.3540	.10569	9.46141	.12338	8.10536	.14113	7.08546	.15898	6.29007	58
3	.08837	11.3163	.10599	9.43515	.12367	8.08600	.14143	7.07059	.15928	6.27829	57
4	.08866	11.2789	.10628	9.40904	.12397	8.06674	.14173	7.05579	.15958	6.26655	56
5	.08895	11.2417	.10657	9.38307	.12426	8.04756	.14202	7.04105	.15988	6.25486	55
6	.08925	11.2048	.10687	9.35724	.12456	8.02848	.14232	7.02637	.16017	6.24321	54
7	.08954	11.1681	.10716	9.33155	.12485	8.00948	.14262	7.01174	.16047	6.23160	53
8	.08983	11.1316	.10746	9.30599	.12515	7.99058	.14291	6.99718	.16077	6.22003	52
9	.09013	11.0954	.10775	9.28058	.12544	7.97176	.14321	6.98268	.16107	6.20851	51
10	.09042	11.0594	.10805	9.25530	.12574	7.95302	.14351	6.96823	.16137	6.19703	50
11	.09071	11.0237	.10834	9.23016	.12603	7.93438	.14381	6.95385	.16167	6.18559	49
12	.09101	10.9882	.10863	9.20516	.12633	7.91582	.14410	6.93952	.16196	6.17419	48
13	.09130	10.9529	.10893	9.18028	.12662	7.89734	.14440	6.92525	.16226	6.16283	47
14	.09159	10.9178	.10922	9.15554	.12692	7.87895	.14470	6.91104	.16256	6.15151	46
15	.09189	10.8829	.10952	9.13093	.12722	7.86064	.14499	6.89688	.16286	6.14023	45
16	.09218	10.8483	.10981	9.10646	.12751	7.84242	.14529	6.88278	.16316	6.12899	44
17	.09247	10.8139	.11011	9.08211	.12781	7.82428	.14559	6.86874	.16346	6.11779	43
18	.09277	10.7797	.11040	9.05789	.12810	7.80622	.14588	6.85475	.16376	6.10664	42
19	.09306	10.7457	.11070	9.03379	.12840	7.78825	.14618	6.84082	.16405	6.09552	41
20	.09335	10.7119	.11099	9.00983	.12869	7.77035	.14648	6.82694	.16435	6.08444	40
21	.09365	10.6783	.11128	8.98598	.12899	7.75254	.14678	6.81312	.16465	6.07340	39
22	.09394	10.6450	.11158	8.96227	.12929	7.73480	.14707	6.79936	.16495	6.06240	38
23	.09423	10.6118	.11187	8.93867	.12958	7.71715	.14737	6.78564	.16525	6.05143	37
24	.09453	10.5789	.11217	8.91520	.12988	7.69957	.14767	6.77199	.16555	6.04051	36
25	.09482	10.5462	.11246	8.89185	.13017	7.68208	.14796	6.75838	.16585	6.02962	35
26	.09511	10.5136	.11276	8.86862	.13047	7.66466	.14826	6.74483	.16615	6.01878	34
27	.09541	10.4813	.11305	8.84551	.13076	7.64732	.14856	6.73133	.16645	6.00797	33
28	.09570	10.4491	.11335	8.82252	.13106	7.63005	.14886	6.71789	.16674	5.99720	32
29	.09600	10.4172	.11364	8.79964	.13136	7.61287	.14915	6.70450	.16704	5.98646	31
30	.09629	10.3854	.11394	8.77689	.13165	7.59575	.14945	6.69116	.16734	5.97576	30
31	.09658	10.3538	.11423	8.75425	.13195	7.57872	.14975	6.67787	.16764	5.96510	29
32	.09688	10.3224	.11452	8.73172	.13224	7.56176	.15005	6.66463	.16794	5.95448	28
33	.09717	10.2913	.11482	8.70931	.13254	7.54487	.15034	6.65144	.16824	5.94390	27
34	.09746	10.2602	.11511	8.68701	.13284	7.52806	.15064	6.63831	.16854	5.93335	26
35	.09776	10.2294	.11541	8.66482	.13313	7.51132	.15094	6.62523	.16884	5.92283	25
36	.09805	10.1988	.11570	8.64275	.13343	7.49465	.15124	6.61219	.16914	5.91236	24
37	.09834	10.1683	.11600	8.62078	.13372	7.47806	.15153	6.59921	.16944	5.90191	23
38	.09864	10.1381	.11629	8.59893	.13402	7.46154	.15183	6.58627	.16974	5.89151	22
39	.09893	10.1080	.11659	8.57718	.13432	7.44509	.15213	6.57339	.17004	5.88114	21
40	.09923	10.0780	.11688	8.55555	.13461	7.42871	.15243	6.56055	.17033	5.87080	20
41	.09952	10.0483	.11718	8.53402	.13491	7.41240	.15272	6.54777	.17063	5.86051	19
42	.09981	10.0187	.11747	8.51259	.13521	7.39616	.15302	6.53503	.17093	5.85024	18
43	.10011	9.98931	.11777	8.49128	.13550	7.37999	.15332	6.52234	.17123	5.84001	17
44	.10040	9.96007	.11806	8.47007	.13580	7.36389	.15362	6.50970	.17153	5.82982	16
45	.10069	9.93101	.11836	8.44896	.13609	7.34786	.15391	6.49710	.17183	5.81966	15
46	.10099	9.90211	.11865	8.42795	.13639	7.33190	.15421	6.48456	.17213	5.80953	14
47	.10128	9.87338	.11895	8.40705	.13669	7.31600	.15451	6.47206	.17243	5.79944	13
48	.10158	9.84482	.11924	8.38625	.13698	7.30018	.15481	6.45961	.17273	5.78938	12
49	.10187	9.81641	.11954	8.36555	.13728	7.28442	.15511	6.44720	.17303	5.77936	11
50	.10216	9.78817	.11983	8.34496	.13758	7.26873	.15540	6.43484	.17333	5.76937	10
51	.10246	9.76009	.12013	8.32446	.13787	7.25310	.15570	6.42253	.17363	5.75941	9
52	.10275	9.73217	.12042	8.30406	.13817	7.23754	.15600	6.41026	.17393	5.74949	8
53	.10305	9.70441	.12072	8.28376	.13846	7.22204	.15630	6.39804	.17423	5.73960	7
54	.10334	9.67680	.12101	8.26355	.13876	7.20661	.15660	6.38587	.17453	5.72974	6
55	.10363	9.64935	.12131	8.24345	.13906	7.19125	.15689	6.37374	.17483	5.71992	5
56	.10393	9.62205	.12160	8.22344	.13935	7.17594	.15719	6.36165	.17513	5.71013	4
57	.10422	9.59490	.12190	8.20352	.13965	7.16071	.15749	6.34961	.17543	5.70037	3
58	.10452	9.56791	.12219	8.18370	.13995	7.14553	.15779	6.33761	.17573	5.69064	2
59	.10481	9.54106	.12249	8.16398	.14024	7.13042	.15809	6.32566	.17603	5.68094	1
60	.10510	9.51436	.12278	8.14435	.14054	7.11537	.15838	6.31375	.17633	5.67128	0
/	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	/
	84°		83°		82°		81°		80°		

NATURAL TANGENTS AND COTANGENTS

/	10°		11°		12°		13°		14°		/
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.17633	5.67128	.19438	5.14455	.21256	4.70463	.23087	4.33148	.24933	4.01078	60
1	.17663	5.66165	.19468	5.13658	.21286	4.69791	.23117	4.32573	.24964	4.00582	59
2	.17693	5.65205	.19498	5.12862	.21316	4.69121	.23148	4.32001	.24995	4.00086	58
3	.17723	5.64248	.19529	5.12069	.21347	4.68452	.23179	4.31430	.25026	3.99592	57
4	.17753	5.63295	.19559	5.11279	.21377	4.67786	.23209	4.30860	.25056	3.99099	56
5	.17783	5.62344	.19589	5.10490	.21408	4.67121	.23240	4.30291	.25087	3.98607	55
6	.17813	5.61397	.19619	5.09704	.21438	4.66458	.23271	4.29724	.25118	3.98117	54
7	.17843	5.60452	.19649	5.08921	.21469	4.65797	.23301	4.29159	.25149	3.97627	53
8	.17873	5.59511	.19680	5.08139	.21499	4.65138	.23332	4.28595	.25180	3.97139	52
9	.17903	5.58573	.19710	5.07360	.21529	4.64480	.23363	4.28032	.25211	3.96651	51
10	.17933	5.57638	.19740	5.06584	.21560	4.63825	.23393	4.27471	.25242	3.96165	50
11	.17963	5.56706	.19770	5.05809	.21590	4.63171	.23424	4.26911	.25273	3.95680	49
12	.17993	5.55777	.19801	5.05037	.21621	4.62518	.23455	4.26352	.25304	3.95196	48
13	.18023	5.54851	.19831	5.04267	.21651	4.61863	.23485	4.25795	.25335	3.94713	47
14	.18053	5.53927	.19861	5.03499	.21682	4.61209	.23516	4.25239	.25366	3.94232	46
15	.18083	5.53007	.19891	5.02734	.21712	4.60552	.23547	4.24685	.25397	3.93751	45
16	.18113	5.52090	.19921	5.01971	.21743	4.59927	.23578	4.24132	.25428	3.93271	44
17	.18143	5.51176	.19952	5.01210	.21773	4.59283	.23608	4.23580	.25459	3.92793	43
18	.18173	5.50264	.19982	5.00451	.21804	4.58641	.23639	4.23030	.25490	3.92316	42
19	.18203	5.49356	.20012	4.99695	.21834	4.58001	.23670	4.22481	.25521	3.91839	41
20	.18233	5.48451	.20042	4.98940	.21864	4.57363	.23700	4.21933	.25552	3.91364	40
21	.18263	5.47548	.20073	4.98188	.21895	4.56726	.23731	4.21387	.25583	3.90890	39
22	.18293	5.46648	.20103	4.97438	.21925	4.56091	.23762	4.20842	.25614	3.90417	38
23	.18323	5.45751	.20133	4.96690	.21956	4.55458	.23793	4.20298	.25645	3.89945	37
24	.18353	5.44857	.20164	4.95945	.21986	4.54826	.23823	4.19756	.25676	3.89474	36
25	.18384	5.43966	.20194	4.95201	.22017	4.54196	.23854	4.19215	.25707	3.89004	35
26	.18414	5.43077	.20224	4.94460	.22047	4.53568	.23885	4.18675	.25738	3.88536	34
27	.18444	5.42192	.20254	4.93721	.22078	4.52941	.23916	4.18137	.25769	3.88068	33
28	.18474	5.41309	.20285	4.92984	.22108	4.52316	.23946	4.17600	.25800	3.87601	32
29	.18504	5.40429	.20315	4.92249	.22139	4.51693	.23977	4.17064	.25831	3.87136	31
30	.18534	5.39552	.20345	4.91516	.22169	4.51071	.24008	4.16530	.25862	3.86671	30
31	.18564	5.38677	.20376	4.90785	.22200	4.50451	.24039	4.15997	.25893	3.86208	29
32	.18594	5.37805	.20406	4.90050	.22231	4.49832	.24069	4.15465	.25924	3.85745	28
33	.18624	5.36936	.20436	4.89330	.22261	4.49215	.24100	4.14934	.25955	3.85284	27
34	.18654	5.36070	.20466	4.88605	.22292	4.48600	.24131	4.14405	.25986	3.84824	26
35	.18684	5.35206	.20497	4.87882	.22322	4.47986	.24162	4.13877	.26017	3.84364	25
36	.18714	5.34345	.20527	4.87162	.22353	4.47374	.24193	4.13350	.26048	3.83906	24
37	.18745	5.33487	.20557	4.86444	.22383	4.46764	.24223	4.12825	.26079	3.83449	23
38	.18775	5.32631	.20588	4.85727	.22414	4.46155	.24254	4.12301	.26110	3.82992	22
39	.18805	5.31778	.20618	4.85013	.22444	4.45548	.24285	4.11778	.26141	3.82537	21
40	.18835	5.30928	.20648	4.84300	.22475	4.44942	.24316	4.11256	.26172	3.82083	20
41	.18865	5.30080	.20679	4.83590	.22505	4.44338	.24347	4.10736	.26203	3.81630	19
42	.18895	5.29235	.20709	4.82882	.22536	4.43735	.24377	4.10216	.26235	3.81177	18
43	.18925	5.28393	.20739	4.82175	.22567	4.43134	.24408	4.09699	.26266	3.80726	17
44	.18955	5.27553	.20770	4.81471	.22597	4.42534	.24439	4.09182	.26297	3.80276	16
45	.18986	5.26715	.20800	4.80769	.22628	4.41936	.24470	4.08666	.26328	3.79827	15
46	.19016	5.25880	.20830	4.80068	.22658	4.41340	.24501	4.08152	.26359	3.79378	14
47	.19046	5.25048	.20861	4.79370	.22689	4.40745	.24532	4.07639	.26390	3.78931	13
48	.19076	5.24218	.20891	4.78673	.22719	4.40152	.24562	4.07127	.26421	3.78485	12
49	.19106	5.23391	.20921	4.77978	.22750	4.39560	.24593	4.06616	.26452	3.78040	11
50	.19136	5.22566	.20952	4.77286	.22781	4.38969	.24624	4.06107	.26483	3.77595	10
51	.19166	5.21744	.20982	4.76595	.22811	4.38381	.24655	4.05599	.26515	3.77152	9
52	.19197	5.20925	.21013	4.75906	.22842	4.37793	.24686	4.05092	.26546	3.76709	8
53	.19227	5.20107	.21043	4.75219	.22872	4.37207	.24717	4.04586	.26577	3.76268	7
54	.19257	5.19293	.21073	4.74534	.22903	4.36623	.24747	4.04081	.26608	3.75828	6
55	.19287	5.18480	.21104	4.73851	.22934	4.36040	.24778	4.03578	.26639	3.75388	5
56	.19317	5.17671	.21134	4.73170	.22964	4.35459	.24809	4.03076	.26670	3.74950	4
57	.19347	5.16863	.21164	4.72490	.22995	4.34879	.24840	4.02574	.26701	3.74512	3
58	.19378	5.16058	.21195	4.71813	.23026	4.34300	.24871	4.02074	.26733	3.74075	2
59	.19408	5.15256	.21225	4.71137	.23056	4.33723	.24902	4.01576	.26764	3.73640	1
60	.19438	5.14455	.21256	4.70463	.23087	4.33148	.24933	4.01078	.26795	3.73205	0
/	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	/
	79°		78°		77°		76°		75°		

NATURAL TANGENTS AND COTANGENTS

/	15°		16°		17°		18°		19°		/
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.26795	3.73205	.28675	3.48741	.30573	3.27085	.32492	3.07768	.34433	2.90421	60
1	.26826	3.72771	.28706	3.48359	.30605	3.26745	.32524	3.07464	.34465	2.90147	59
2	.26857	3.72338	.28738	3.47977	.30637	3.26406	.32556	3.07160	.34498	2.89873	58
3	.26888	3.71907	.28769	3.47596	.30669	3.26067	.32588	3.06857	.34530	2.89600	57
4	.26920	3.71476	.28800	3.47216	.30700	3.25729	.32621	3.06554	.34563	2.89327	56
5	.26951	3.71046	.28832	3.46837	.30732	3.25392	.32653	3.06252	.34596	2.89055	55
6	.26982	3.70616	.28864	3.46458	.30764	3.25055	.32685	3.05950	.34628	2.88783	54
7	.27013	3.70188	.28895	3.46080	.30796	3.24719	.32717	3.05649	.34661	2.88511	53
8	.27044	3.69761	.28927	3.45703	.30828	3.24383	.32749	3.05349	.34693	2.88240	52
9	.27076	3.69335	.28958	3.45327	.30860	3.24049	.32782	3.05049	.34726	2.87970	51
10	.27107	3.68909	.28990	3.44951	.30891	3.23714	.32814	3.04749	.34758	2.87700	50
11	.27138	3.68485	.29021	3.44576	.30923	3.23381	.32846	3.04450	.34791	2.87430	49
12	.27169	3.68061	.29053	3.44202	.30955	3.23048	.32878	3.04152	.34824	2.87161	48
13	.27201	3.67638	.29084	3.43829	.30987	3.22715	.32911	3.03854	.34856	2.86892	47
14	.27232	3.67217	.29116	3.43456	.31019	3.22384	.32943	3.03556	.34889	2.86624	46
15	.27263	3.66796	.29147	3.43084	.31051	3.22053	.32975	3.03260	.34922	2.86356	45
16	.27294	3.66376	.29179	3.42713	.31083	3.21722	.33007	3.02963	.34954	2.86089	44
17	.27326	3.65957	.29210	3.42343	.31115	3.21392	.33040	3.02667	.34987	2.85822	43
18	.27357	3.65538	.29242	3.41973	.31147	3.21063	.33072	3.02372	.35020	2.85555	42
19	.27388	3.65121	.29274	3.41604	.31178	3.20734	.33104	3.02077	.35052	2.85289	41
20	.27419	3.64705	.29305	3.41236	.31210	3.20406	.33136	3.01783	.35085	2.85020	40
21	.27451	3.64289	.29337	3.40869	.31242	3.20079	.33169	3.01489	.35118	2.84758	39
22	.27482	3.63874	.29368	3.40502	.31274	3.19752	.33201	3.01196	.35150	2.84494	38
23	.27513	3.63461	.29400	3.40136	.31306	3.19426	.33233	3.00903	.35183	2.84229	37
24	.27545	3.63048	.29432	3.39771	.31338	3.19100	.33266	3.00611	.35216	2.83965	36
25	.27576	3.62636	.29463	3.39406	.31370	3.18775	.33298	3.00319	.35248	2.83702	35
26	.27607	3.62224	.29495	3.39042	.31402	3.18451	.33330	3.00028	.35281	2.83439	34
27	.27638	3.61814	.29526	3.38679	.31434	3.18127	.33363	3.00736	.35314	2.83176	33
28	.27670	3.61405	.29558	3.38317	.31466	3.17804	.33395	3.00447	.35346	2.82912	32
29	.27701	3.60996	.29590	3.37955	.31498	3.17481	.33427	3.00158	.35379	2.82653	31
30	.27732	3.60588	.29621	3.37594	.31530	3.17159	.33460	3.00868	.35412	2.82391	30
31	.27764	3.60181	.29653	3.37234	.31562	3.16838	.33492	2.99580	.35445	2.82130	29
32	.27795	3.59775	.29685	3.36875	.31595	3.16517	.33524	2.98292	.35477	2.81870	28
33	.27826	3.59370	.29716	3.36516	.31626	3.16197	.33557	2.98004	.35510	2.81610	27
34	.27858	3.58966	.29748	3.36158	.31658	3.15877	.33589	2.97717	.35543	2.81350	26
35	.27889	3.58562	.29780	3.35800	.31690	3.15553	.33621	2.97430	.35576	2.81091	25
36	.27921	3.58160	.29811	3.35443	.31722	3.15234	.33654	2.97144	.35608	2.80833	24
37	.27952	3.57758	.29843	3.35087	.31754	3.14922	.33686	2.96858	.35641	2.80574	23
38	.27983	3.57357	.29875	3.34732	.31786	3.14605	.33718	2.96573	.35674	2.80316	22
39	.28015	3.56957	.29906	3.34377	.31818	3.14288	.33751	2.96283	.35707	2.80059	21
40	.28046	3.56557	.29938	3.34023	.31850	3.13972	.33783	2.96004	.35740	2.79802	20
41	.28077	3.56159	.29970	3.33670	.31882	3.13656	.33816	2.95721	.35772	2.79545	19
42	.28109	3.55761	.30001	3.33317	.31914	3.13341	.33848	2.95437	.35805	2.79289	18
43	.28140	3.55364	.30033	3.32965	.31946	3.13027	.33881	2.95155	.35838	2.79033	17
44	.28172	3.54968	.30065	3.32614	.31978	3.12713	.33913	2.94872	.35871	2.78778	16
45	.28203	3.54573	.30097	3.32264	.32010	3.12400	.33945	2.94591	.35904	2.78523	15
46	.28234	3.54179	.30128	3.31914	.32042	3.12087	.33978	2.94309	.35937	2.78269	14
47	.28266	3.53785	.30160	3.31565	.32074	3.11775	.34010	2.94028	.35969	2.78014	13
48	.28297	3.53393	.30192	3.31216	.32106	3.11464	.34043	2.93745	.36002	2.77761	12
49	.28329	3.53001	.30224	3.30868	.32139	3.11153	.34075	2.93463	.36035	2.77507	11
50	.28360	3.52609	.30255	3.30521	.32171	3.10842	.34108	2.93189	.36068	2.77254	10
51	.28391	3.52219	.30287	3.30174	.32203	3.10532	.34140	2.92910	.36101	2.77002	9
52	.28423	3.51829	.30319	3.29829	.32235	3.10223	.34173	2.92632	.36134	2.76750	8
53	.28454	3.51441	.30351	3.29483	.32267	3.09914	.34205	2.92354	.36167	2.76498	7
54	.28486	3.51053	.30382	3.29139	.32299	3.09606	.34238	2.92076	.36199	2.76247	6
55	.28517	3.50666	.30414	3.28795	.32331	3.09298	.34270	2.91799	.36232	2.75996	5
56	.28549	3.50279	.30446	3.28452	.32363	3.08991	.34303	2.91523	.36265	2.75744	4
57	.28580	3.49894	.30478	3.28109	.32396	3.08685	.34335	2.91246	.36298	2.75493	3
58	.28612	3.49509	.30509	3.27767	.32428	3.08379	.34368	2.90971	.36331	2.75242	2
59	.28643	3.49125	.30541	3.27426	.32460	3.08073	.34400	2.90696	.36364	2.74991	1
60	.28675	3.48741	.30573	3.27085	.32492	3.07768	.34433	2.90421	.36397	2.74748	0
/	15°		16°		17°		18°		19°		/
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	74°		73°		72°		71°		70°		

NATURAL TANGENTS AND COTANGENTS

/	20°		21°		22°		23°		24°		/
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.36397	2.74748	.38386	2.60509	.40403	2.47509	.42447	2.35585	.44523	2.24604	60
1	.36430	2.74499	.38420	2.60283	.40436	2.47302	.42482	2.35395	.44558	2.24428	59
2	.36463	2.74251	.38453	2.60057	.40470	2.47095	.42516	2.35205	.44593	2.24252	58
3	.36496	2.74004	.38487	2.59831	.40504	2.46888	.42551	2.35015	.44627	2.24077	57
4	.36529	2.73756	.38520	2.59606	.40538	2.46682	.42585	2.34825	.44662	2.23902	56
5	.36562	2.73509	.38553	2.59381	.40572	2.46476	.42619	2.34636	.44697	2.23727	55
6	.36595	2.73263	.38587	2.59156	.40606	2.46270	.42654	2.34447	.44732	2.23553	54
7	.36628	2.73017	.38620	2.58932	.40640	2.46065	.42688	2.34258	.44767	2.23378	53
8	.36661	2.72771	.38654	2.58708	.40674	2.45860	.42722	2.34069	.44802	2.23204	52
9	.36694	2.72526	.38687	2.58484	.40707	2.45655	.42757	2.33881	.44837	2.23030	51
10	.36727	2.72281	.38721	2.58261	.40741	2.45451	.42791	2.33693	.44872	2.22857	50
11	.36760	2.72036	.38754	2.58038	.40775	2.45246	.42826	2.33505	.44907	2.22683	49
12	.36793	2.71792	.38787	2.57815	.40809	2.45043	.42860	2.33317	.44942	2.22510	48
13	.36826	2.71548	.38821	2.57593	.40843	2.44839	.42894	2.33130	.44977	2.22337	47
14	.36859	2.71305	.38854	2.57371	.40877	2.44636	.42929	2.32943	.45012	2.22164	46
15	.36892	2.71062	.38888	2.57150	.40911	2.44433	.42963	2.32756	.45047	2.21992	45
16	.36925	2.70819	.38921	2.56928	.40945	2.44230	.42998	2.32570	.45082	2.21819	44
17	.36958	2.70577	.38955	2.56707	.40979	2.44027	.43032	2.32383	.45117	2.21647	43
18	.36991	2.70335	.38988	2.56487	.41013	2.43825	.43067	2.32197	.45152	2.21475	42
19	.37024	2.70094	.39022	2.56266	.41047	2.43623	.43101	2.32012	.45187	2.21304	41
20	.37057	2.69853	.39055	2.56046	.41081	2.43422	.43136	2.31826	.45222	2.21132	40
21	.37090	2.69612	.39089	2.55827	.41115	2.43220	.43170	2.31641	.45257	2.20961	39
22	.37123	2.69371	.39122	2.55608	.41149	2.43019	.43205	2.31456	.45292	2.20790	38
23	.37157	2.69131	.39156	2.55389	.41183	2.42819	.43239	2.31271	.45327	2.20619	37
24	.37190	2.68890	.39190	2.55170	.41217	2.42618	.43274	2.31086	.45362	2.20449	36
25	.37223	2.68653	.39223	2.54952	.41251	2.42418	.43308	2.30902	.45397	2.20278	35
26	.37256	2.68414	.39257	2.54734	.41285	2.42218	.43343	2.30718	.45432	2.20108	34
27	.37289	2.68175	.39290	2.54516	.41319	2.42019	.43378	2.30534	.45467	2.19938	33
28	.37322	2.67937	.39324	2.54299	.41353	2.41819	.43412	2.30351	.45502	2.19769	32
29	.37355	2.67700	.39357	2.54082	.41387	2.41620	.43447	2.30167	.45537	2.19599	31
30	.37388	2.67462	.39391	2.53865	.41421	2.41421	.43481	2.29984	.45573	2.19430	30
31	.37422	2.67225	.39425	2.53648	.41455	2.41223	.43516	2.29801	.45608	2.19261	29
32	.37455	2.66989	.39458	2.53432	.41490	2.41025	.43550	2.29619	.45643	2.19092	28
33	.37488	2.66752	.39492	2.53217	.41524	2.40827	.43585	2.29437	.45678	2.18923	27
34	.37521	2.66516	.39526	2.53001	.41558	2.40629	.43620	2.29254	.45713	2.18755	26
35	.37554	2.66281	.39559	2.52786	.41592	2.40432	.43654	2.29073	.45748	2.18587	25
36	.37588	2.66046	.39593	2.52571	.41626	2.40235	.43689	2.28891	.45784	2.18419	24
37	.37621	2.65811	.39626	2.52357	.41660	2.40038	.43724	2.28710	.45819	2.18251	23
38	.37654	2.65576	.39660	2.52142	.41694	2.39841	.43758	2.28528	.45854	2.18084	22
39	.37687	2.65342	.39694	2.51929	.41728	2.39645	.43793	2.28343	.45889	2.17916	21
40	.37720	2.65109	.39727	2.51715	.41763	2.39449	.43828	2.28167	.45924	2.17749	20
41	.37754	2.64875	.39761	2.51502	.41797	2.39253	.43862	2.27987	.45960	2.17582	19
42	.37787	2.64642	.39795	2.51289	.41831	2.39058	.43897	2.27806	.45995	2.17416	18
43	.37820	2.64410	.39829	2.51076	.41865	2.38863	.43932	2.27626	.46030	2.17249	17
44	.37853	2.64177	.39862	2.50864	.41899	2.38668	.43966	2.27447	.46065	2.17083	16
45	.37887	2.63945	.39896	2.50652	.41933	2.38473	.44001	2.27267	.46101	2.16917	15
46	.37920	2.63714	.39930	2.50440	.41968	2.38279	.44036	2.27088	.46136	2.16751	14
47	.37953	2.63483	.39963	2.50229	.42002	2.38084	.44071	2.26909	.46171	2.16585	13
48	.37986	2.63252	.39997	2.50018	.42036	2.37891	.44105	2.26730	.46206	2.16420	12
49	.38020	2.63021	.40031	2.49807	.42070	2.37697	.44140	2.26552	.46242	2.16255	11
50	.38053	2.62791	.40065	2.49597	.42105	2.37504	.44175	2.26374	.46277	2.16090	10
51	.38086	2.62561	.40098	2.49386	.42139	2.37311	.44210	2.26196	.46312	2.15925	9
52	.38120	2.62332	.40132	2.49177	.42173	2.37118	.44244	2.26018	.46348	2.15760	8
53	.38153	2.62103	.40166	2.48967	.42207	2.36925	.44279	2.25840	.46383	2.15596	7
54	.38186	2.61874	.40200	2.48758	.42242	2.36733	.44314	2.25663	.46418	2.15432	6
55	.38220	2.61646	.40234	2.48549	.42276	2.36541	.44349	2.25486	.46454	2.15268	5
56	.38253	2.61418	.40267	2.48340	.42310	2.36349	.44384	2.25309	.46489	2.15104	4
57	.38286	2.61190	.40301	2.48132	.42345	2.36158	.44418	2.25132	.46525	2.14940	3
58	.38320	2.60963	.40335	2.47924	.42379	2.35967	.44453	2.24956	.46560	2.14777	2
59	.38353	2.60736	.40369	2.47716	.42413	2.35776	.44488	2.24780	.46595	2.14614	1
60	.38386	2.60509	.40403	2.47509	.42447	2.35585	.44523	2.24604	.46631	2.14451	0
/	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	/
	69°		68°		67°		66°		65°		

/	25°		26°		27°		28°		29°		/
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.46631	2.14451	.48773	2.05030	.50953	1.96261	.53171	1.88073	.55431	1.80405	60
1	.46666	2.14488	.48809	2.04879	.50989	1.96120	.53208	1.87941	.55469	1.80281	59
2	.46702	2.14525	.48845	2.04728	.51026	1.95979	.53246	1.87809	.55507	1.80158	58
3	.46737	2.13963	.48881	2.04577	.51063	1.95838	.53283	1.87677	.55545	1.80034	57
4	.46772	2.13801	.48917	2.04426	.51099	1.95698	.53320	1.87546	.55583	1.79911	56
5	.46808	2.13639	.48953	2.04276	.51136	1.95557	.53358	1.87415	.55621	1.79788	55
6	.46843	2.13477	.48989	2.04125	.51173	1.95417	.53395	1.87283	.55659	1.79665	54
7	.46879	2.13316	.49026	2.03975	.51209	1.95277	.53432	1.87152	.55697	1.79542	53
8	.46914	2.13154	.49062	2.03825	.51246	1.95137	.53470	1.87021	.55736	1.79419	52
9	.46950	2.12993	.49098	2.03675	.51283	1.94997	.53507	1.86891	.55774	1.79296	51
10	.46985	2.12832	.49134	2.03526	.51319	1.94858	.53545	1.86760	.55812	1.79174	50
11	.47021	2.12671	.49170	2.03376	.51356	1.94718	.53582	1.86630	.55850	1.79051	49
12	.47056	2.12511	.49206	2.03227	.51393	1.94579	.53620	1.86499	.55888	1.78929	48
13	.47092	2.12350	.49242	2.03078	.51430	1.94440	.53657	1.86369	.55926	1.78807	47
14	.47128	2.12190	.49278	2.02929	.51467	1.94301	.53694	1.86239	.55964	1.78685	46
15	.47163	2.12030	.49315	2.02780	.51503	1.94162	.53732	1.86109	.56003	1.78563	45
16	.47199	2.11871	.49351	2.02631	.51540	1.94023	.53769	1.85979	.56041	1.78441	44
17	.47234	2.11711	.49387	2.02483	.51577	1.93885	.53807	1.85850	.56079	1.78319	43
18	.47270	2.11552	.49423	2.02335	.51614	1.93746	.53844	1.85720	.56117	1.78198	42
19	.47305	2.11392	.49459	2.02187	.51651	1.93608	.53882	1.85591	.56155	1.78077	41
20	.47341	2.11233	.49495	2.02039	.51688	1.93470	.53920	1.85462	.56194	1.77955	40
21	.47377	2.11075	.49532	2.01891	.51724	1.93332	.53957	1.85333	.56232	1.77834	39
22	.47412	2.10916	.49568	2.01743	.51761	1.93195	.53995	1.85204	.56270	1.77713	38
23	.47448	2.10758	.49604	2.01596	.51798	1.93057	.54032	1.85075	.56309	1.77592	37
24	.47483	2.10600	.49640	2.01449	.51835	1.92920	.54070	1.84946	.56347	1.77471	36
25	.47519	2.10442	.49677	2.01302	.51872	1.92782	.54107	1.84818	.56385	1.77351	35
26	.47555	2.10284	.49713	2.01155	.51909	1.92645	.54145	1.84689	.56424	1.77230	34
27	.47590	2.10126	.49749	2.01008	.51946	1.92508	.54183	1.84561	.56462	1.77110	33
28	.47626	2.09969	.49786	2.00862	.51983	1.92371	.54220	1.84433	.56501	1.76990	32
29	.47662	2.09811	.49822	2.00715	.52020	1.92235	.54258	1.84305	.56539	1.76869	31
30	.47698	2.09654	.49858	2.00569	.52057	1.920					

Table of Angles for Gashing Worm Wheels.

The following table gives the angle with the axis of the worm wheel to which the cutter is to be set for gashing the teeth of worm wheels when the pitch diameter and lead of the worm are known.

If the worm has a pitch diameter which is not given exactly in the table, the angle can be approximated from the nearest sizes entered so as to be well within working limits.

TABLE OF ANGLES FOR GASHING WORM WHEELS.

LEAD.	1000'	1111'	1250'	1333'	1429'	1538'	1666'	1818'	2000'	2222'	2500'	2857'	3333'	3836'	4000'	4255'	4444'	5000'	5714'	6000'	6666'	7500'	8000'	1.0000'	1.3333'	1.5000'	2.0000'	3.0000'	4.0000'	5.0000'	6.0000'	7.0000'	8.0000'	9.0000'
TURN PER INCH	10	9	8	7½	7	6½	6	5½	5	4½	4	3½	3	2¾	2⅔	2½	2¼	2	1¾	1⅔	1½	1⅓	1¼	1	¾	⅔	½	⅓	¼	⅓	¼	⅓	¼	⅓
5⁄8	2°55'	3°14'	3°38'	3°51'	4°10'	4°29'	4°51'	5°18'	5°49'	6°28'	7°16'	8°17'	9°38'	10°30'	10°49'	11°31'																		
¾	2°26'	2°42'	3°2'	3°14'	3°28'	3°44'	4°3'	4°25'	4°51'	5°23'	6°4'	6°55'	8°3'	8°46'	9°3'	9°38'	10°18'																	
7⁄8	2°5'	2°19'	2°36'	2°47'	2°58'	3°12'	3°28'	3°47'	4°10'	4°37'	5°12'	5°56'	6°55'	7°32'	7°46'	8°17'	8°52'																	
1	1°49'	2°1'	2°17'	2°26'	2°36'	2°48'	3°2'	3°19'	3°39'	4°3'	4°33'	5°12'	6°3'	6°36'	6°43'	7°15'	7°47'	8°3'																
1⅛	1°37'	1°48'	2°2'	2°10'	2°19'	2°30'	2°42'	2°57'	3°14'	3°36'	4°3'	4°37'	5°23'	5°52'	6°4'	6°27'	6°55'	7°10'																
1¼	1°28'	1°37'	1°49'	1°57'	2°5'	2°15'	2°26'	2°39'	2°55'	3°14'	3°39'	4°10'	4°51'	5°17'	5°27'	5°49'	6°14'	6°27'	7°15'															
1⅜	1°20'	1°28'	1°39'	1°46'	1°54'	2°2'	2°13'	2°25'	2°39'	2°57'	3°19'	3°47'	4°25'	4°49'	4°58'	5°17'	5°40'	5°52'	6°36'															
1½	1°13'	1°21'	1°31'	1°37'	1°44'	1°52'	2°1'	2°13'	2°26'	2°42'	3°2'	3°28'	4°3'	4°25'	4°33'	4°51'	5°12'	5°23'	6°3'	6°55'														
1⅝	1°7'	1°15'	1°24'	1°30'	1°36'	1°44'	1°52'	2°2'	2°15'	2°30'	2°43'	3°12'	3°44'	4°4'	4°12'	4°29'	4°48'	4°59'	5°36'	6°23'	6°42'													
1¾	1°2'	1°9'	1°18'	1°23'	1°29'	1°36'	1°44'	1°54'	2°5'	2°19'	2°36'	2°58'	3°28'	3°47'	3°54'	4°10'	4°27'	4°37'	5°12'	5°36'	6°14'													
1⅞	58'	1°5'	1°13'	1°18'	1°23'	1°30'	1°37'	1°46'	1°57'	2°10'	2°26'	2°47'	3°14'	3°32'	3°39'	3°53'	4°10'	4°19'	4°51'	5°32'	6°19'	6°27'												
2	55'	1°1'	1°8'	1°13'	1°18'	1°24'	1°31'	1°39'	1°49'	2°2'	2°17'	2°36'	3°2'	3°19'	3°25'	3°39'	3°54'	4°3'	4°33'	5°12'	5°27'	6°3'												
2⅛	52'	57'	1°4'	1°9'	1°14'	1°19'	1°26'	1°34'	1°43'	1°54'	2°9'	2°27'	2°52'	3°7'	3°13'	3°26'	3°40'	3°46'	4°17'	4°54'	5°8'	5°42'	6°29'											
2¼	49'	54'	1°1'	1°5'	1°9'	1°15'	1°21'	1°28'	1°37'	1°48'	2°2'	2°19'	2°42'	2°57'	3°2'	3°14'	3°28'	3°36'	4°3'	4°37'	4°51'	5°23'	6°3'											
2⅜	46'	51'	58'	1°1'	1°6'	1°11'	1°17'	1°24'	1°32'	1°42'	1°55'	2°12'	2°33'	2°47'	2°53'	3°4'	3°17'	3°25'	3°50'	4°22'	4°36'	5°6'	5°44'	6°7'										
2½	44'	49'	54'	58'	1°3'	1°7'	1°13'	1°20'	1°27'	1°37'	1°49'	2°6'	2°26'	2°39'	2°44'	2°55'	3°7'	3°14'	3°39'	4°10'	4°22'	4°51'	5°27'	5°49'										

PITCH DIAMETERS

TABLE OF ANGLES FOR GASHING WORM WHEELS.

LEAD.	.1000"	.1111"	.1250"	.1333"	.1429"	.1538"	.1666"	.1818"	.2000"	.2222"	.2500"	.2857"	.3333"	.3636"	.3750"	.4000"	.4285"	.4444"	.5000"	.5714"	.6000"	.6566"	.7500"	.8000"	1.0000"	1.3333"	1.5000"	2.0000"	3.0000"
TURNS PER INCH	10	9	8	7½	7	6½	6	5½	5	4½	4	3½	3	2¾	2⅔	2½	2⅓	2¼	2	1¾	1⅔	1½	1⅓	1¼	1	¾	⅔	½	⅓
2⅝"	42'	46'	52'	56'	1°	1°4'	1°9'	1°16'	1°23'	1°33'	1°44'	1°59'	2°19'	2°31'	2°36'	2°47'	2°59'	3°5'	3°28'	3°58'	4°10'	4°37'	5°12'	5°32'	6°55'				
2¾"	40'	44'	50'	53'	57'	1°1'	1°6'	1°12'	1°20'	1°28'	1°39'	1°54'	2°13'	2°25'	2°29'	2°39'	2°50'	3°2'	3°19'	3°47'	3°58'	4°25'	4°58'	5°17'	6°36'				
2⅞"	38'	42'	48'	51'	54'	58'	1°3'	1°9'	1°16'	1°25'	1°35'	1°49'	2°7'	2°18'	2°23'	2°32'	2°43'	3°10'	3°48'	4°13'	4°45'	5°4'	6°19'	8°24'					
3	36'	40'	46'	49'	52'	56'	1°1'	1°6'	1°13'	1°21'	1°31'	1°44'	2°2'	2°13'	2°17'	2°26'	2°36'	3°2'	3°28'	3°39'	4°3'	4°33'	4°51'	6°3'	9°3'				
3¼"	34'	38'	42'	45'	48'	52'	56'	1°1'	1°7'	1°15'	1°24'	1°36'	1°52'	2°2'	2°6'	2°14'	2°24'	3°10'	3°48'	4°13'	4°45'	5°4'	6°19'	8°24'					
3½"	32'	35'	39'	42'	45'	48'	52'	57'	1°3'	1°9'	1°18'	1°29'	1°44'	1°54'	1°57'	2°5'	2°11'	2°19'	2°36'	2°59'	3°7'	3°28'	3°54'	4°10'	5°12'	6°54'	7°46'	10°19'	
3¾"	30'	33'	36'	39'	42'	45'	48'	53'	58'	1°5'	1°13'	1°23'	1°37'	1°46'	1°49'	1°57'	2°5'	2°10'	2°26'	2°41'	3°55'	3°14'	3°39'	3°53'	4°51'	6°27'	7°15'	9°38'	
4	31'	34'	37'	39'	42'	46'	50'	55'	55'	1°1'	1°8'	1°18'	1°31'	1°39'	1°43'	1°49'	1°55'	2°2'	2°17'	2°36'	2°41'	3°2'	3°25'	3°39'	4°33'	6°4'	6°49'	9°3'	13°26'
4⅓"		32'	34'	37'	40'	43'	47'	52'	57'	1°4'	1°14'	1°26'	1°34'	1°37'	1°43'	1°50'	1°54'	2°9'	2°27'	2°34'	2°52'	3°13'	3°26'	4°17'	5°42'	6°26'	8°32'	12°40'	
4½"			32'	35'	37'	40'	44'	49'	54'	1°1'	1°9'	1°21'	1°28'	1°31'	1°37'	1°41'	1°48'	2°2'	2°19'	2°26'	2°42'	3°2'	3°14'	4°3'	5°23'	6°4'	8°3'	11°59'	
4¾"				32'	35'	38'	42'	46'	51'	58'	1°6'	1°17'	1°24'	1°26'	1°32'	1°37'	1°42'	1°55'	2°12'	2°18'	2°33'	2°53'	3°4'	3°50'	5°6'	6°44'	7°33'	11°22'	
5						34'	36'	40'	44'	49'	55'	1°3'	1°13'	1°20'	1°22'	1°28'	1°34'	1°37'	1°49'	2°5'	2°11'	2°36'	2°44'	3°55'	3°39'	4°51'	5°27'	7°15'	10°49'
5⅓"							35'	38'	42'	46'	52'	1°1'	1°9'	1°16'	1°18'	1°23'	1°28'	1°33'	1°44'	1°59'	2°5'	2°19'	2°36'	2°41'	3°58'	4°37'	5°12'	6°54'	10°19'
5½"							36'	40'	44'	49'	50'	57'	1°6'	1°12'	1°15'	1°20'	1°25'	1°28'	1°39'	1°54'	1°59'	2°13'	2°29'	2°38'	3°19'	4°25'	4°55'	6°36'	9°51'
5¾"								38'	42'	48'	54'	1°3'	1°9'	1°11'	1°16'	1°22'	1°24'	1°35'	1°49'	1°54'	2°7'	2°23'	2°32'	3°10'	4°13'	4°45'	6°19'	9°26'	
6									40'	46'	52'	1°1'	1°6'	1°8'	1°13'	1°18'	1°21'	1°31'	1°44'	1°49'	2°1'	2°17'	2°26'	3°2'	4°2'	4°33'	6°3'	9°2'	

PITCH DIAMETERS.

PITCH DIAMETERS.

Tables of Prime Numbers and Factors. 1 to 10200.

In making use of these tables, the following explanation may be of assistance: the two columns at the left give the last two figures of the number to be factored; the first column gives all numbers to 50 and the second column from 50 to 100.

EXAMPLE 1.—Required, the factors of 138. Refer to the column of numbers from 100 to 150 and follow down the column until opposite 38 in the left-hand column; the factors are found to be $2 \times 3 \times 23$.

EXAMPLE 2.—Required, the factors for 1672. Refer to the column of numbers from 1650 to 1700 and follow down the column until opposite 72 in the second column at the left; the factors are found to be $2^3 \times 11 \times 19$ or, more conveniently stated for factoring, $2 \times 2 \times 2 \times 11 \times 19$.

Prime Numbers and Factors, 1-300.

From To	0 50	50 100	100 150	150 200	200 250	250 300
0	50	2·5 ²	2 ² ·5 ²	2·3·5 ²	2·5 ³
1	51	3·17	3·67
2	52	2 ² ·13	2·3·17	2 ³ ·19	2 ² ·3 ² ·7
3	53	3 ² ·17	7·29
4	54	2 ²	2·3 ³	2 ³ ·13	2·7·11	2 ² ·3·17
5	55	5·11	3·5·7	5·31	5·41
6	56	2·3	2 ³ ·7	2·53	2 ² ·3·13	2·103
7	57	3·19	3 ² ·23
8	58	2 ³	2·29	2 ² ·3 ³	2·79	2 ⁴ ·13
9	59	3 ²	3·53	11·19
10	60	2·5	2 ² ·3·5	2·5·11	2 ⁶ ·5	2·3·5·7
11	61	3·37	7·23
12	62	2 ² ·3	2·31	2 ⁴ ·7	2·3 ⁴	2 ² ·53
13	63	3 ² ·7	3·71
14	64	2·7	2 ⁸	2·3·19	2 ² ·41	2·107
15	65	3·5	5·13	5·23	3·5·11	5·43
16	66	2 ⁴	2·3·11	2 ² ·29	2·83	2 ³ ·3 ³
17	67	3 ² ·13	7·31
18	68	2·3 ²	2 ² ·17	2·59	2 ³ ·3·7	2·109
19	69	3·23	7·17	13 ²	3·73
20	70	2 ² ·5	2·5·7	2 ³ ·3·5	2·5·17	2 ² ·5·11
21	71	3·7	11 ²	3 ² ·19	13·17
22	72	2·11	2 ³ ·3 ²	2·61	2 ² ·43	2·3·37
23	73	3·41
24	74	2 ³ ·3	2·37	2 ² ·31	2·3·29	2 ³ ·7
25	75	5 ²	3·5 ²	5 ³	5 ² ·7	3 ² ·5 ²
26	76	2·13	2 ² ·19	2·3 ² ·7	2 ⁴ ·11	2·113
27	77	3 ³	7·11	3·59
28	78	2 ² ·7	2·3·13	2 ⁷	2·89	2 ² ·3·19
29	79	3·43
30	80	2·3·5	2 ⁴ ·5	2·5·13	2 ² ·3 ² ·5	2·5·23
31	81	3 ⁴	3·7·11
32	82	2 ⁵	2·41	2 ² ·3·11	2·7·13	2 ³ ·29
33	83	3·11	7·19	3·61
34	84	2·17	2 ² ·3·7	2·67	2 ³ ·23	2·3 ² ·13
35	85	5·7	5·17	3 ³ ·5	5·37	5·47
36	86	2 ² ·3 ²	2·43	2 ³ ·17	2·3·31	2 ² ·59
37	87	3·29	11·17	3·79
38	88	2·19	2 ³ ·11	2·3·23	2 ² ·47	2·7·17
39	89	3·13	3 ³ ·7
40	90	2 ³ ·5	2·3 ² ·5	2 ² ·5·7	2·5·19	2 ⁴ ·3·5
41	91	7·13	3·47
42	92	2·3·7	2 ² ·23	2·71	2 ⁶ ·3	2·11 ²
43	93	3·31	11·13	3 ³
44	94	2 ² ·11	2·47	2 ⁴ ·3 ²	2·97	2 ² ·61
45	95	3 ² ·5	5·19	5·29	3·5·13	5·7 ²
46	96	2·23	2 ⁵ ·3	2·73	2 ² ·7 ²	2·3·41
47	97	3·7 ²	13·19
48	98	2 ⁴ ·3	2·7 ²	2 ² ·37	2·3 ² ·11	2 ³ ·31
49	99	7 ²	3 ² ·11	3·83
50	100	2·5 ²	2 ² ·5 ²	2·3·5 ²	2 ³ ·5 ²	2·5 ³

Prime Numbers and Factors, 300-600.

From To		300 350	350 400	400 450	450 500	500 550	550 600
0	50	2 ² ·3·5 ²	2·5 ² ·7	2 ⁴ ·5 ²	2·3 ² ·5 ²	2 ² ·5 ³	2·5 ² ·11
1	51	7·43	3 ³ ·13	11·41	3·167	19·29
2	52	2·151	2 ⁵ ·11	2·3·67	2 ² ·113	2·251	2 ⁴ ·3·23
3	53	3·101	13·31	3·151	7·79
4	54	2 ⁴ ·19	2·3·59	2 ² ·101	2·227	2 ³ ·3 ² ·7	2·277
5	55	5·61	5·71	3 ⁴ ·5	5·7·13	5·101	3·5·37
6	56	2·3 ² ·17	2 ² ·89	2·7·29	2 ⁴ ·3·19	2·11·23	2 ² ·139
7	57	3·7·17	11·37	3·13 ²
8	58	2 ² ·7·11	2·179	2 ³ ·3·17	2·229	2 ² ·127	2·3 ² ·31
9	59	3·103	3 ³ ·17	13·43
10	60	2·5·31	2 ³ ·3 ² ·5	2·5·41	2 ² ·5·23	2·3·5·17	2 ⁴ ·5·7
11	61	19 ²	3·137	7·73	3·11·17
12	62	2 ³ ·3·13	2·181	2 ² ·103	2·3·7·11	2 ⁹	2·281
13	63	3·11 ²	7·59	3 ³ ·19
14	64	2·157	2 ² ·7·13	2·3 ² ·23	2 ⁴ ·29	2·257	2 ² ·3·47
15	65	3 ² ·5·7	5·73	5·83	3·5·31	5·103	5·113
16	66	2 ² ·79	2·3·61	2 ⁵ ·13	2·233	2 ² ·3·43	2·283
17	67	3·139	11·47	3 ⁴ ·7
18	68	2·3·53	2 ⁴ ·23	2·11·19	2 ² ·3 ² ·13	2·7·37	2 ³ ·71
19	69	11·29	3 ² ·41	7·67	3·173
20	70	2 ⁶ ·5	2·5·37	2 ² ·3·5·7	2·5·47	2 ³ ·5·13	2·3·5·19
21	71	3·107	7·53	3·157
22	72	2·7·23	2 ² ·3·31	2·211	2 ³ ·59	2·3 ² ·29	2 ² ·11·13
23	73	17·19	3 ² ·47	11·43	3·191
24	74	2 ² ·3 ⁴	2·11·17	2 ³ ·53	2·3·79	2 ² ·131	2·7·41
25	75	5 ² ·13	3·5 ³	5 ² ·17	5 ² ·19	3·5 ² ·7	5 ² ·23
26	76	2·163	2 ³ ·47	2·3·71	2 ² ·7·17	2·263	2 ⁶ ·3 ²
27	77	3·109	13·29	7·61	3 ² ·53	17·31
28	78	2 ³ ·41	2·3 ³ ·7	2 ² ·107	2·239	2 ⁴ ·3·11	2·17 ²
29	79	7·47	3·11·13	23 ²	3·193
30	80	2·3·5·11	2 ² ·5·19	2·5·43	2 ⁵ ·3·5	2·5·53	2 ² ·5·29
31	81	3·127	13·37	3 ² ·59	7·83
32	82	2 ² ·83	2·191	2 ⁴ ·3 ³	2·241	2 ² ·7·19	2·3·97
33	83	3 ² ·37	3·7·23	13·41	11·53
34	84	2·167	2 ⁷ ·3	2·7·31	2 ² ·11 ²	2·3·89	2 ³ ·73
35	85	5·67	5·7·11	3·5·29	5·97	5·107	3 ² ·5·13
36	86	2 ⁴ ·3·7	2·193	2 ² ·109	2·3 ⁵	2 ³ ·67	2·293
37	87	3 ² ·43	19·23	3·179
38	88	2·13 ²	2 ² ·97	2·3·73	2 ³ ·61	2·269	2 ² ·3·7 ²
39	89	3·113	3·163	7 ² ·11	19·31
40	90	2 ² ·5·17	2·3·5·13	2 ³ ·5·11	2·5·7 ²	2 ² ·3 ³ ·5	2·5·59
41	91	11·31	17·23	3 ² ·7 ²	3·197
42	92	2·3 ² ·19	2 ³ ·7 ²	2·13·17	2 ² ·3·41	2·271	2 ⁴ ·37
43	93	7 ³	3·131	17·29	3·181
44	94	2 ³ ·43	2·197	2 ² ·3·37	2·13·19	2 ⁵ ·17	2·3 ³ ·11
45	95	3·5 ² ·23	5·79	5·89	3 ² ·5·11	5·109	5·7·17
46	96	2·173	2 ² ·3 ² ·11	2·223	2 ⁴ ·31	2·3·7·13	2 ² ·149
47	97	3·149	7·71	3·199
48	98	2 ² ·3·29	2·199	2 ⁶ ·7	2·3·83	2 ² ·137	2·13·23
49	99	3·7·19	3 ² ·61
50	100	2·5 ² ·7	2 ⁴ ·5 ²	2·3 ² ·5 ²	2 ² ·5 ³	2·5 ² ·11	2 ³ ·3·5 ²

Prime Numbers and Factors, 600-900.

From To	600 650	650 700	700 750	750 800	800 850	850 900
0	50	$2^3 \cdot 3 \cdot 5^2$	$2 \cdot 5^2 \cdot 13$	$2^2 \cdot 5^2 \cdot 7$	$2 \cdot 3 \cdot 5^3$	$2 \cdot 5^2 \cdot 17$
1	51	$3 \cdot 7 \cdot 31$	$3^2 \cdot 89$	$23 \cdot 37$
2	52	$2 \cdot 7 \cdot 43$	$2^2 \cdot 163$	$2 \cdot 3^3 \cdot 13$	$2^4 \cdot 47$	$2^2 \cdot 3 \cdot 71$
3	53	$3^2 \cdot 67$	$19 \cdot 37$	$3 \cdot 251$
4	54	$2^2 \cdot 3 \cdot 151$	$2 \cdot 3 \cdot 109$	$2^6 \cdot 11$	$2 \cdot 13 \cdot 29$	$2^2 \cdot 3 \cdot 67$
5	55	$5 \cdot 11^2$	$5 \cdot 131$	$3 \cdot 5 \cdot 47$	$5 \cdot 151$	$5 \cdot 7 \cdot 23$
6	56	$2 \cdot 3 \cdot 101$	$2^4 \cdot 41$	$2 \cdot 353$	$2^2 \cdot 3^3 \cdot 7$	$2 \cdot 13 \cdot 31$
7	57	$3^2 \cdot 73$	$7 \cdot 101$	$3 \cdot 269$
8	58	$2^5 \cdot 19$	$2 \cdot 7 \cdot 47$	$2^2 \cdot 3 \cdot 59$	$2 \cdot 379$	$2^3 \cdot 101$
9	59	$3 \cdot 7 \cdot 29$	$3 \cdot 11 \cdot 23$
10	60	$2 \cdot 5 \cdot 61$	$2^2 \cdot 3 \cdot 5 \cdot 11$	$2 \cdot 5 \cdot 71$	$2^3 \cdot 5 \cdot 19$	$2 \cdot 3^4 \cdot 5$
11	61	$13 \cdot 47$	$3^2 \cdot 79$	$3 \cdot 7 \cdot 41$
12	62	$2^2 \cdot 3^2 \cdot 17$	$2 \cdot 331$	$2^3 \cdot 89$	$2 \cdot 3 \cdot 127$	$2 \cdot 431$
13	63	$3 \cdot 13 \cdot 17$	$23 \cdot 31$	$7 \cdot 109$
14	64	$2 \cdot 3 \cdot 7$	$2^3 \cdot 83$	$2 \cdot 3 \cdot 7 \cdot 17$	$2^2 \cdot 191$	$2 \cdot 11 \cdot 37$
15	65	$3 \cdot 5 \cdot 41$	$5 \cdot 7 \cdot 19$	$5 \cdot 11 \cdot 13$	$3^2 \cdot 5 \cdot 17$	$5 \cdot 163$
16	66	$2^3 \cdot 7 \cdot 11$	$2 \cdot 3^2 \cdot 37$	$2^2 \cdot 179$	$2 \cdot 383$	$2^4 \cdot 3 \cdot 17$
17	67	$23 \cdot 29$	$3 \cdot 239$	$13 \cdot 59$	$19 \cdot 43$
18	68	$2 \cdot 3 \cdot 103$	$2^2 \cdot 167$	$2 \cdot 359$	$2^3 \cdot 3$	$2 \cdot 409$
19	69	$3 \cdot 223$	$3^2 \cdot 7 \cdot 13$
20	70	$2^2 \cdot 5 \cdot 31$	$2 \cdot 5 \cdot 67$	$2^4 \cdot 3^2 \cdot 5$	$2 \cdot 5 \cdot 7 \cdot 11$	$2^2 \cdot 5 \cdot 41$
21	71	$3^3 \cdot 23$	$11 \cdot 61$	$7 \cdot 103$	$3 \cdot 257$
22	72	$2 \cdot 3 \cdot 11$	$2^5 \cdot 3 \cdot 7$	$2 \cdot 19^2$	$2^2 \cdot 193$	$2 \cdot 3 \cdot 137$
23	73	$7 \cdot 89$	$3 \cdot 241$
24	74	$2^4 \cdot 3 \cdot 13$	$2 \cdot 337$	$2^2 \cdot 181$	$2 \cdot 3^2 \cdot 43$	$2^3 \cdot 103$
25	75	5^4	$3^3 \cdot 5^2$	$5^2 \cdot 29$	$5^2 \cdot 31$	$3 \cdot 5^2 \cdot 11$
26	76	$2 \cdot 3 \cdot 13$	$2^2 \cdot 13^2$	$2 \cdot 3 \cdot 11^2$	$2^3 \cdot 97$	$2 \cdot 7 \cdot 59$
27	77	$3 \cdot 11 \cdot 19$	$3 \cdot 7 \cdot 37$
28	78	$2^2 \cdot 157$	$2 \cdot 3 \cdot 113$	$2^3 \cdot 7 \cdot 13$	$2 \cdot 389$	$2^2 \cdot 3^2 \cdot 23$
29	79	$17 \cdot 37$	$7 \cdot 97$	3^6	$19 \cdot 41$
30	80	$2 \cdot 3^2 \cdot 5 \cdot 7$	$2^3 \cdot 5 \cdot 17$	$2 \cdot 5 \cdot 73$	$2^2 \cdot 3 \cdot 5 \cdot 13$	$2 \cdot 5 \cdot 83$
31	81	$3 \cdot 227$	$17 \cdot 43$	$11 \cdot 71$	$3 \cdot 277$
32	82	$2^3 \cdot 79$	$2 \cdot 11 \cdot 31$	$2^2 \cdot 3 \cdot 61$	$2 \cdot 17 \cdot 23$	$2^6 \cdot 13$
33	83	$3 \cdot 211$	$3^3 \cdot 29$	$7^2 \cdot 17$
34	84	$2 \cdot 3 \cdot 17$	$2^2 \cdot 3^2 \cdot 19$	$2 \cdot 367$	$2^4 \cdot 7^2$	$2 \cdot 3 \cdot 139$
35	85	$5 \cdot 127$	$5 \cdot 137$	$3 \cdot 5 \cdot 7^2$	$5 \cdot 157$	$5 \cdot 167$
36	86	$2^2 \cdot 3 \cdot 53$	$2 \cdot 7^3$	$2^5 \cdot 23$	$2 \cdot 3 \cdot 131$	$2^2 \cdot 11 \cdot 19$
37	87	$7^2 \cdot 13$	$3 \cdot 229$	$11 \cdot 67$	$3^3 \cdot 31$
38	88	$2 \cdot 11 \cdot 29$	$2^4 \cdot 43$	$2 \cdot 3^2 \cdot 41$	$2^2 \cdot 197$	$2 \cdot 419$
39	89	$3^2 \cdot 71$	$13 \cdot 53$	$3 \cdot 263$
40	90	$2^7 \cdot 5$	$2 \cdot 3 \cdot 5 \cdot 23$	$2^2 \cdot 5 \cdot 37$	$2 \cdot 5 \cdot 79$	$2^3 \cdot 3 \cdot 5 \cdot 7$
41	91	$3 \cdot 13 \cdot 19$	$7 \cdot 113$	29^2
42	92	$2 \cdot 3 \cdot 107$	$2^2 \cdot 173$	$2 \cdot 7 \cdot 53$	$2^3 \cdot 3^2 \cdot 11$	$2 \cdot 421$
43	93	$3^2 \cdot 7 \cdot 11$	$13 \cdot 61$	$3 \cdot 281$
44	94	$2^2 \cdot 7 \cdot 23$	$2 \cdot 347$	$2^3 \cdot 3 \cdot 31$	$2 \cdot 397$	$2^2 \cdot 211$
45	95	$3 \cdot 5 \cdot 43$	$5 \cdot 139$	$5 \cdot 149$	$3 \cdot 5 \cdot 53$	$5 \cdot 13^2$
46	96	$2 \cdot 17 \cdot 19$	$2^3 \cdot 3 \cdot 29$	$2 \cdot 373$	$2^2 \cdot 199$	$2 \cdot 3^2 \cdot 47$
47	97	$17 \cdot 41$	$3^2 \cdot 83$	$7 \cdot 11^2$
48	98	$2^3 \cdot 3^4$	$2 \cdot 349$	$2^2 \cdot 11 \cdot 17$	$2 \cdot 3 \cdot 7 \cdot 19$	$2^4 \cdot 53$
49	99	$11 \cdot 59$	$3 \cdot 233$	$7 \cdot 107$	$17 \cdot 47$	$3 \cdot 283$
50	100	$2 \cdot 5^2 \cdot 13$	$2^2 \cdot 5^2 \cdot 7$	$2 \cdot 3 \cdot 5^3$	$2 \cdot 5 \cdot 5^2$	$2 \cdot 5^2 \cdot 17$

Prime Numbers and Factors, 900-1200.

From To	900 950	950 1000	1000 1050	1050 1100	1100 1150	1150 1200
0	50	2 ² ·3 ² ·5 ²	2 ⁵ ·2 ¹⁹	2 ³ ·5 ³	2 ² ·5 ² ·11	2 ⁵ ·2 ³
1	51	17·53	3·317	7·11·13	3·367
2	52	2 ³ ·11·41	2 ³ ·7·17	2 ³ ·167	2 ² ·263	2 ⁷ ·3 ²
3	53	3 ⁷ ·43	17·59	3 ⁴ ·13
4	54	2 ³ ·113	2 ³ ·2 ⁵³	2 ² ·251	2 ² ·17·31	2 ⁴ ·3·23
5	55	5·181	5·191	3·5·67	5·211	5·13·17
6	56	2 ³ ·151	2 ² ·239	2·503	2 ³ ·3·11	2 ⁷ ·79
7	57	3·11·29	19·53	7·151	3 ³ ·41
8	58	2 ² ·227	2·479	2 ⁴ ·3 ² ·7	2 ² ·23 ²	2 ² ·277
9	59	3 ² ·101	7·137	3·353
10	60	2 ⁵ ·7·13	2 ⁶ ·3·5	2 ⁵ ·101	2 ² ·5 ² ·53	2 ³ ·5·37
11	61	31 ²	3·337	11·101
12	62	2 ⁴ ·3·19	2 ² ·13·37	2 ² ·11·23	2 ³ ·59	2 ³ ·139
13	63	11·83	3 ² ·107	3·7·53
14	64	2·457	2 ² ·241	2 ³ ·13 ²	2 ³ ·7·19	2 ² ·557
15	65	3 ⁵ ·61	5·193	5·7·29	3·5·71	5·223
16	66	2 ² ·229	2 ³ ·7·23	2 ³ ·127	2 ² ·13·41	2 ² ·3 ² ·31
17	67	7·131	3 ² ·113	11·97
18	68	2 ³ ·3·17	2 ³ ·11 ²	2·509	2 ² ·3·89	2 ² ·13·43
19	69	3·17·19	3·373
20	70	2 ³ ·5·23	2 ⁵ ·97	2 ² ·3·5·17	2 ⁵ ·107	2 ³ ·5·7
21	71	3·307	3 ² ·7·17	19·59
22	72	2 ⁴ ·3·19	2 ² ·3 ⁵	2 ⁷ ·73	2 ⁴ ·67	2 ³ ·11·17
23	73	13·71	7·139	3 ² ·11·31	29·37
24	74	2 ² ·3 ⁷ ·11	2·487	2 ¹⁰	2 ³ ·179	2 ² ·281
25	75	5 ² ·37	3 ⁵ ·2·13	5 ² ·41	5 ² ·43	3 ² ·5 ³
26	76	2·463	2 ⁴ ·61	2 ³ ·19	2 ² ·269	2 ⁵ ·63
27	77	3 ² ·103	13·79	3·359	7 ² ·23
28	78	2 ⁵ ·29	2 ³ ·163	2 ² ·257	2 ⁷ ·2·11	2 ³ ·3·47
29	79	11·89	3·7 ³	13·83
30	80	2 ³ ·5·31	2 ² ·5·7 ²	2 ⁵ ·103	2 ³ ·3 ³ ·5	2 ⁵ ·113
31	81	7 ² ·19	3 ² ·109	23·47	3·13·29
32	82	2 ² ·233	2·491	2 ³ ·3·43	2 ² ·541	2 ² ·283
33	83	3·311	3·19 ²	11·103
34	84	2·467	2 ³ ·3·41	2 ² ·11·47	2 ² ·271	2 ³ ·4·7
35	85	5·11·17	5·197	3 ² ·5·23	5·7·31	5·227
36	86	2 ³ ·3 ² ·13	2 ² ·17·29	2 ² ·7·37	2 ³ ·181	2 ⁴ ·71
37	87	3 ⁷ ·47	17·61	3·379
38	88	2 ⁷ ·67	2 ² ·13·19	2 ³ ·173	2 ⁶ ·17	2 ⁵ ·69
39	89	3·313	23·43	3 ² ·11 ²	17·67
40	90	2 ² ·5·47	2 ³ ·2 ⁵ ·11	2 ⁴ ·5·13	2 ⁵ ·109	2 ² ·3·5·19
41	91	3·347	7·163
42	92	2 ³ ·157	2 ⁵ ·31	2 ⁵ ·21	2 ² ·3·7·13	2 ⁵ ·71
43	93	23·41	3·331	7·149	3 ² ·127
44	94	2 ⁴ ·59	2 ⁷ ·71	2 ² ·3 ² ·29	2·547	2 ³ ·11·13
45	95	3 ³ ·5·7	5·199	5·11·19	3·5·73	5·229
46	96	2 ² ·11·43	2 ² ·3·83	2 ⁵ ·23	2 ³ ·137	2 ³ ·191
47	97	3·349	31·37
48	98	2 ² ·3·79	2·499	2 ³ ·131	2 ³ ·2 ⁶ ·61	2 ² ·7·41
49	99	13·73	3 ³ ·37	7·157	3·383
50	100	2 ⁵ ·2·19	2 ³ ·5 ³	2 ³ ·5 ² ·7	2 ² ·5 ² ·11	2 ⁵ ·2 ³ ·23

Prime Numbers and Factors, 1200-1500.

From To		1200 1250	1250 1300	1300 1350	1350 1400	1400 1450	1450 1500
0	50	$2^1 \cdot 3 \cdot 5^2$	$2 \cdot 5^4$	$2^2 \cdot 5^2 \cdot 13$	$2 \cdot 3^3 \cdot 5^2$	$2^3 \cdot 5^2 \cdot 7$	$2 \cdot 5^2 \cdot 29$
1	51	$3^2 \cdot 139$	$7 \cdot 193$	$3 \cdot 467$
2	52	$2 \cdot 601$	$2^2 \cdot 313$	$2 \cdot 3 \cdot 7 \cdot 31$	$2^3 \cdot 13^2$	$2 \cdot 701$	$2^2 \cdot 3 \cdot 11^2$
3	53	$3 \cdot 401$	$7 \cdot 179$	$3 \cdot 11 \cdot 41$	$23 \cdot 61$
4	54	$2^2 \cdot 7 \cdot 43$	$2 \cdot 3 \cdot 11 \cdot 19$	$2^3 \cdot 163$	$2 \cdot 677$	$2^2 \cdot 3^3 \cdot 13$	$2 \cdot 727$
5	55	$5 \cdot 241$	$5 \cdot 251$	$3^2 \cdot 5 \cdot 29$	$5 \cdot 271$	$5 \cdot 281$	$3 \cdot 5 \cdot 97$
6	56	$2 \cdot 3^2 \cdot 67$	$2^3 \cdot 157$	$2 \cdot 653$	$2^2 \cdot 3 \cdot 113$	$2 \cdot 19 \cdot 37$	$2^1 \cdot 7 \cdot 13$
7	57	$17 \cdot 71$	$3 \cdot 419$	$23 \cdot 59$	$3 \cdot 7 \cdot 67$	$31 \cdot 47$
8	58	$2^3 \cdot 151$	$2 \cdot 17 \cdot 37$	$2^2 \cdot 3 \cdot 109$	$2 \cdot 7 \cdot 97$	$2^7 \cdot 11$	$2 \cdot 3^6$
9	59	$3 \cdot 13 \cdot 31$	$7 \cdot 11 \cdot 17$	$3^2 \cdot 151$
10	60	$2 \cdot 5 \cdot 11^2$	$2^2 \cdot 3^2 \cdot 5 \cdot 7$	$2 \cdot 5 \cdot 131$	$2^1 \cdot 5 \cdot 17$	$2 \cdot 3 \cdot 5 \cdot 47$	$2^2 \cdot 5 \cdot 73$
11	61	$7 \cdot 173$	$13 \cdot 97$	$3 \cdot 19 \cdot 23$	$17 \cdot 83$	$3 \cdot 487$
12	62	$2^2 \cdot 3 \cdot 101$	$2 \cdot 631$	$2^5 \cdot 41$	$2 \cdot 3 \cdot 227$	$2^2 \cdot 353$	$2 \cdot 17 \cdot 43$
13	63	$3 \cdot 421$	$13 \cdot 101$	$29 \cdot 47$	$3^2 \cdot 157$	$7 \cdot 11 \cdot 19$
14	64	$2 \cdot 607$	$2^1 \cdot 79$	$2 \cdot 3^2 \cdot 73$	$2^2 \cdot 11 \cdot 31$	$2 \cdot 7 \cdot 101$	$2^3 \cdot 3 \cdot 61$
15	65	$3^5 \cdot 5$	$5 \cdot 11 \cdot 23$	$5 \cdot 263$	$3 \cdot 5 \cdot 7 \cdot 13$	$5 \cdot 283$	$5 \cdot 293$
16	66	$2^6 \cdot 19$	$2 \cdot 3 \cdot 211$	$2^2 \cdot 7 \cdot 47$	$2 \cdot 683$	$2^3 \cdot 3 \cdot 59$	$2 \cdot 733$
17	67	$7 \cdot 181$	$3 \cdot 439$	$13 \cdot 109$	$3^2 \cdot 163$
18	68	$2 \cdot 3 \cdot 7 \cdot 29$	$2^2 \cdot 317$	$2 \cdot 659$	$2^3 \cdot 3^2 \cdot 19$	$2 \cdot 709$	$2^2 \cdot 367$
19	69	$2^3 \cdot 53$	$3^3 \cdot 47$	37^2	$3 \cdot 11 \cdot 43$	$13 \cdot 113$
20	70	$2^2 \cdot 5 \cdot 61$	$2^5 \cdot 127$	$2^3 \cdot 3 \cdot 5 \cdot 11$	$2 \cdot 5 \cdot 137$	$2^2 \cdot 5 \cdot 71$	$2 \cdot 3 \cdot 5 \cdot 7^2$
21	71	$3 \cdot 11 \cdot 37$	$31 \cdot 41$	$3 \cdot 457$	$7^2 \cdot 29$
22	72	$2 \cdot 13 \cdot 47$	$2^3 \cdot 3 \cdot 53$	$2 \cdot 661$	$2^2 \cdot 7^3$	$2 \cdot 3^2 \cdot 79$	$2^6 \cdot 23$
23	73	$19 \cdot 67$	$3^3 \cdot 7^2$	$3 \cdot 491$
24	74	$2^3 \cdot 3^2 \cdot 17$	$2 \cdot 7^2 \cdot 13$	$2^2 \cdot 331$	$2 \cdot 3 \cdot 229$	$2^4 \cdot 89$	$2 \cdot 11 \cdot 67$
25	75	$5^2 \cdot 7^2$	$3 \cdot 5^2 \cdot 17$	$5^2 \cdot 53$	$5^3 \cdot 11$	$3 \cdot 5^2 \cdot 19$	$5^2 \cdot 59$
26	76	$2 \cdot 613$	$2^2 \cdot 11 \cdot 29$	$2 \cdot 3 \cdot 13 \cdot 17$	$2^5 \cdot 43$	$2 \cdot 23 \cdot 31$	$2^2 \cdot 3^2 \cdot 41$
27	77	$3 \cdot 409$	$3^4 \cdot 17$	$7 \cdot 211$
28	78	$2^2 \cdot 307$	$2 \cdot 3^2 \cdot 71$	$2^4 \cdot 83$	$2^2 \cdot 13 \cdot 53$	$2^2 \cdot 3 \cdot 7 \cdot 17$	$2 \cdot 739$
29	79	$3 \cdot 443$	$7 \cdot 197$	$3 \cdot 17 \cdot 29$
30	80	$2 \cdot 3 \cdot 5 \cdot 41$	$2^8 \cdot 5$	$2 \cdot 5 \cdot 7 \cdot 19$	$2^2 \cdot 3 \cdot 5 \cdot 23$	$2 \cdot 5 \cdot 11 \cdot 13$	$2^3 \cdot 5 \cdot 37$
31	81	$3 \cdot 7 \cdot 61$	11^3	$3^3 \cdot 53$
32	82	$2^1 \cdot 7 \cdot 11$	$2 \cdot 641$	$2^2 \cdot 3^2 \cdot 37$	$2 \cdot 691$	$2^3 \cdot 179$	$2 \cdot 3 \cdot 13 \cdot 19$
33	83	$3^2 \cdot 137$	$31 \cdot 43$	$3 \cdot 461$
34	84	$2 \cdot 617$	$2^2 \cdot 3 \cdot 107$	$2 \cdot 23 \cdot 29$	$2^3 \cdot 173$	$2 \cdot 3 \cdot 239$	$2^4 \cdot 7 \cdot 53$
35	85	$5 \cdot 13 \cdot 19$	$5 \cdot 257$	$3 \cdot 5 \cdot 89$	$5 \cdot 277$	$5 \cdot 7 \cdot 41$	$3^3 \cdot 5 \cdot 11$
36	86	$2^2 \cdot 3 \cdot 103$	$2 \cdot 643$	$2^3 \cdot 167$	$2 \cdot 3^2 \cdot 7 \cdot 11$	$2^2 \cdot 359$	$2 \cdot 743$
37	87	$3^2 \cdot 11 \cdot 13$	$7 \cdot 191$	$19 \cdot 73$	$3 \cdot 479$
38	88	$2 \cdot 619$	$2^3 \cdot 7 \cdot 23$	$2 \cdot 3 \cdot 223$	$2^2 \cdot 347$	$2 \cdot 719$	$2^1 \cdot 3 \cdot 31$
39	89	$3 \cdot 7 \cdot 59$	$13 \cdot 103$	$3 \cdot 463$
40	90	$2^3 \cdot 5 \cdot 31$	$2 \cdot 3 \cdot 5 \cdot 43$	$2^2 \cdot 5 \cdot 67$	$2 \cdot 5 \cdot 139$	$2^5 \cdot 3^2 \cdot 5$	$2 \cdot 5 \cdot 149$
41	91	$17 \cdot 73$	$3^2 \cdot 149$	$13 \cdot 107$	$11 \cdot 131$	$3 \cdot 7 \cdot 71$
42	92	$2 \cdot 3^3 \cdot 23$	$2^2 \cdot 17 \cdot 19$	$2 \cdot 11 \cdot 61$	$2^1 \cdot 3 \cdot 29$	$2 \cdot 7 \cdot 103$	$2^2 \cdot 373$
43	93	$11 \cdot 113$	$3 \cdot 431$	$17 \cdot 79$	$7 \cdot 199$	$3 \cdot 13 \cdot 37$
44	94	$2^2 \cdot 311$	$2 \cdot 647$	$2^6 \cdot 3 \cdot 7$	$2 \cdot 17 \cdot 41$	$2^2 \cdot 19^2$	$2 \cdot 3^2 \cdot 83$
45	95	$3 \cdot 5 \cdot 83$	$5 \cdot 7 \cdot 37$	$5 \cdot 269$	$3^2 \cdot 5 \cdot 31$	$5 \cdot 17^2$	$5 \cdot 13 \cdot 23$
46	96	$2 \cdot 7 \cdot 89$	$2^1 \cdot 3^4$	$2 \cdot 673$	$2^2 \cdot 349$	$2 \cdot 3 \cdot 241$	$2^3 \cdot 11 \cdot 17$
47	97	$29 \cdot 43$	$3 \cdot 449$	$11 \cdot 127$	$3 \cdot 499$
48	98	$2^5 \cdot 3 \cdot 13$	$2 \cdot 11 \cdot 59$	$2^2 \cdot 337$	$2 \cdot 3 \cdot 233$	$2^3 \cdot 181$	$2 \cdot 7 \cdot 107$
49	99	$3 \cdot 433$	$19 \cdot 71$	$3^2 \cdot 7 \cdot 23$
50	100	$2 \cdot 5^4$	$2^2 \cdot 5^2 \cdot 13$	$2 \cdot 3^3 \cdot 5^2$	$2^3 \cdot 5^2 \cdot 7$	$2 \cdot 5^2 \cdot 29$	$2^2 \cdot 3 \cdot 5^3$

Prime Numbers and Factors, 1500-1800.

From To		1500 1550	1550 1600	1600 1650	1650 1700	1700 1750	1750 1800
0	50	2 ² ·3·5 ³	2·5 ² ·31	2 ⁶ ·5 ²	2·3·5 ² ·11	2 ² ·5 ² ·17	2·5 ³ ·7
1	51	19·79	3·11·47	13·127	3 ⁵ ·7	17·103
2	52	2·751	2 ⁴ ·97	2·3 ² ·89	2 ² ·7·59	2·23·37	2 ⁴ ·3·73
3	53	3 ² ·167	7·229	3·19·29	13·131
4	54	2 ³ ·47	2·3·7·37	2 ² ·401	2·827	2 ³ ·3·71	2·877
5	55	5·7·43	5·311	3·5·107	5·331	5·11·31	3 ³ ·5·13
6	56	2·3·251	2 ² ·389	2·11·73	2 ³ ·3 ² ·23	2·853	2 ² ·439
7	57	11·137	3 ² ·173	3·569	7·251
8	58	2 ² ·13·29	2·19·41	2 ³ ·3·67	2·829	2 ² ·7·61	2·3·293
9	59	3·593	3·7·79
10	60	2·5·151	2 ³ ·3·5·13	2·5·7·23	2 ² ·5·83	2·3 ² ·5·19	2 ³ ·5·11
11	61	7·223	3 ² ·179	11·151	29·59	3·587
12	62	2 ³ ·3 ³ ·7	2·11·71	2 ² ·13·31	2·3·277	2 ⁴ ·107	2·881
13	63	17·89	3·521	3·571	41·43
14	64	2·757	2 ² ·17·23	2·3·269	2 ⁷ ·13	2·857	2 ² ·3 ² ·7 ²
15	65	3·5·101	5·313	5·17·19	3 ² ·5·37	5·7 ³	5·353
16	66	2 ² ·379	2·3 ³ ·29	2 ⁴ ·101	2·7 ² ·17	2 ² ·3·11·13	2·883
17	67	37·41	3·7 ² ·11	17·101	3·19·31
18	68	2·3·11·23	2 ⁵ ·7 ²	2·809	2 ² ·3·139	2·859	2 ³ ·13·17
19	69	7 ² ·31	3·523	3 ² ·191	29·61
20	70	2 ⁴ ·5·19	2·5·157	2 ² ·3 ⁴ ·5	2·5·167	2 ³ ·5·43	2·3·5·59
21	71	3 ² ·13 ²	3·557	7·11·23
22	72	2·761	2 ² ·3·131	2·811	2 ³ ·11·19	2·3·7·41	2 ² ·443
23	73	11 ² ·13	3·541	7·239	3 ² ·197
24	74	2 ² ·3·127	2·787	2 ³ ·7·29	2·3 ³ ·31	2 ² ·431	2·887
25	75	5 ² ·61	3 ² ·5 ² ·7	5 ³ ·13	5 ² ·67	3·5 ² ·23	5 ² ·71
26	76	2·7·109	2 ³ ·197	2·3·271	2 ² ·419	2·863	2 ⁴ ·3·37
27	77	3·509	19·83	3·13·43	11·157
28	78	2 ³ ·191	2·3·263	2 ² ·11·37	2·839	2 ⁶ ·3 ³	2·7·127
29	79	11·139	3 ² ·181	23·73	7·13·19	3·593
30	80	2·3 ² ·5·17	2 ² ·5·79	2·5·163	2 ⁴ ·3·5·7	2·5·173	2 ² ·5·89
31	81	3·17·31	7·233	41 ²	3·577	13·137
32	82	2 ² ·383	2·7·113	2 ⁵ ·3·17	2·29 ²	2 ² ·433	2·3 ⁴ ·11
33	83	3·7·73	23·71	3 ² ·11·17
34	84	2·13·59	2 ⁴ ·3 ² ·11	2·19·43	2 ² ·421	2·3·17 ²	2 ³ ·223
35	85	5·307	5·317	3·5·109	5·337	5·347	3·5·7·17
36	86	2 ³ ·3	2·13·61	2 ² ·409	2·3·281	2 ² ·7·31	2·19·47
37	87	29·53	3·23 ²	7·241	3 ² ·193
38	88	2·769	2 ² ·397	2·3 ² ·7·13	2 ³ ·211	2·11·79	2 ² ·3·149
39	89	3 ⁴ ·19	7·227	11·149	3·563	37·47
40	90	2 ² ·5·7·11	2·3·5·53	2 ³ ·5·41	2·5·13 ²	2 ² ·3·5·29	2·5·179
41	91	23·67	37·43	3·547	19·89	3 ² ·199
42	92	2·3·257	2 ³ ·199	2·821	2 ² ·3 ² ·47	2·13·67	2 ⁸ ·7
43	93	3 ³ ·59	31·53	3·7·83	11·163
44	94	2 ³ ·193	2·797	2 ² ·3·137	2·7·11 ²	2 ⁴ ·109	2·3·13·23
45	95	3·5·103	5·11·29	5·7·47	3·5·113	5·349	5·359
46	96	2·773	2 ² ·3·7·19	2·823	2 ³ ·53	2·3 ² ·97	2 ² ·449
47	97	7·13·17	3 ³ ·61	3·599
48	98	2 ² ·3 ² ·43	2·17·47	2 ⁴ ·103	2·3·283	2 ² ·19·23	2·29·31
49	99	3·13·41	17·97	3·11·53	7·257
50	100	2·5 ² ·31	2 ⁶ ·5 ²	2·3·5 ² ·11	2 ² ·5 ² ·17	2·5 ³ ·7	2 ³ ·3 ² ·5 ²

Prime Numbers and Factors, 1800-2100.

From To		1800 1850	1850 1900	1900 1950	1950 2000	2000 2050	2050 2100
0	50	$2^3 \cdot 3^2 \cdot 5^2$	$2 \cdot 5^2 \cdot 37$	$2^2 \cdot 5^2 \cdot 19$	$2 \cdot 3 \cdot 5^2 \cdot 13$	$2^4 \cdot 5^3$	$2 \cdot 5^2 \cdot 41$
1	51	$3 \cdot 617$	$3 \cdot 23 \cdot 29$	$7 \cdot 293$
2	52	$2 \cdot 17 \cdot 53$	$2^2 \cdot 463$	$2 \cdot 3 \cdot 317$	$2^5 \cdot 61$	$2 \cdot 7 \cdot 11 \cdot 13$	$2^2 \cdot 3^3 \cdot 19$
3	53	$3 \cdot 601$	$17 \cdot 109$	$11 \cdot 173$	$3^2 \cdot 7 \cdot 31$
4	54	$2^2 \cdot 11 \cdot 41$	$2 \cdot 3^2 \cdot 103$	$2^4 \cdot 7 \cdot 17$	$2 \cdot 977$	$2^2 \cdot 3 \cdot 167$	$2 \cdot 13 \cdot 79$
5	55	$5 \cdot 19^2$	$5 \cdot 7 \cdot 53$	$3 \cdot 5 \cdot 127$	$5 \cdot 17 \cdot 23$	$5 \cdot 401$	$3 \cdot 5 \cdot 137$
6	56	$2 \cdot 3 \cdot 7 \cdot 43$	$2^6 \cdot 29$	$2 \cdot 953$	$2^2 \cdot 3 \cdot 163$	$2 \cdot 17 \cdot 59$	$2^8 \cdot 257$
7	57	$13 \cdot 139$	$3 \cdot 619$	$19 \cdot 103$	$3^2 \cdot 223$	$11^2 \cdot 17$
8	58	$2^4 \cdot 113$	$2 \cdot 929$	$2^2 \cdot 3^2 \cdot 53$	$2 \cdot 11 \cdot 89$	$2^3 \cdot 251$	$2 \cdot 3 \cdot 7^3$
9	59	$3^3 \cdot 67$	$11 \cdot 13^2$	$23 \cdot 83$	$3 \cdot 653$	$7^2 \cdot 41$	$29 \cdot 71$
10	60	$2 \cdot 5 \cdot 181$	$2^2 \cdot 3 \cdot 5 \cdot 31$	$2 \cdot 5 \cdot 191$	$2^3 \cdot 5 \cdot 7^2$	$2 \cdot 3 \cdot 5 \cdot 67$	$2^2 \cdot 5 \cdot 103$
11	61	$3 \cdot 7^2 \cdot 13$	$37 \cdot 53$	$3^2 \cdot 229$
12	62	$2^2 \cdot 3 \cdot 151$	$2 \cdot 7^2 \cdot 19$	$2^3 \cdot 239$	$2 \cdot 3^2 \cdot 109$	$2^2 \cdot 503$	$2 \cdot 1031$
13	63	$7^2 \cdot 37$	$3^4 \cdot 23$	$13 \cdot 151$	$3 \cdot 11 \cdot 61$
14	64	$2 \cdot 907$	$2^3 \cdot 233$	$2 \cdot 3 \cdot 11 \cdot 29$	$2^2 \cdot 491$	$2 \cdot 19 \cdot 53$	$2^4 \cdot 3 \cdot 43$
15	65	$3 \cdot 5 \cdot 11^2$	$5 \cdot 373$	$5 \cdot 383$	$3 \cdot 5 \cdot 131$	$5 \cdot 13 \cdot 31$	$5 \cdot 7 \cdot 59$
16	66	$2^3 \cdot 227$	$2 \cdot 3 \cdot 311$	$2^2 \cdot 479$	$2 \cdot 983$	$2^5 \cdot 3^2 \cdot 7$	$2 \cdot 1033$
17	67	$23 \cdot 79$	$3^3 \cdot 71$	$7 \cdot 281$	$3 \cdot 13 \cdot 53$
18	68	$2 \cdot 3^2 \cdot 101$	$2^2 \cdot 467$	$2 \cdot 7 \cdot 137$	$2^4 \cdot 3 \cdot 41$	$2 \cdot 1009$	$2^2 \cdot 11 \cdot 47$
19	69	$17 \cdot 107$	$3 \cdot 7 \cdot 89$	$19 \cdot 101$	$11 \cdot 179$	$3 \cdot 673$
20	70	$2^2 \cdot 5 \cdot 7 \cdot 13$	$2 \cdot 5 \cdot 11 \cdot 17$	$2^7 \cdot 3 \cdot 5$	$2 \cdot 5 \cdot 197$	$2^2 \cdot 5 \cdot 101$	$2 \cdot 3^2 \cdot 5 \cdot 23$
21	71	$3 \cdot 607$	$17 \cdot 113$	$3^3 \cdot 73$	$43 \cdot 47$	$19 \cdot 109$
22	72	$2 \cdot 911$	$2^4 \cdot 3^2 \cdot 13$	$2 \cdot 31^2$	$2^2 \cdot 17 \cdot 29$	$2 \cdot 3 \cdot 337$	$2^3 \cdot 7 \cdot 37$
23	73	$3 \cdot 641$	$7 \cdot 17^2$	$3 \cdot 691$
24	74	$2^3 \cdot 3 \cdot 19$	$2 \cdot 937$	$2^2 \cdot 13 \cdot 37$	$2 \cdot 3 \cdot 7 \cdot 47$	$2^3 \cdot 11 \cdot 23$	$2 \cdot 17 \cdot 61$
25	75	$5^2 \cdot 73$	$3 \cdot 5^4$	$5^2 \cdot 7 \cdot 11$	$5^2 \cdot 79$	$3^4 \cdot 5^2$	$5^2 \cdot 83$
26	76	$2 \cdot 11 \cdot 83$	$2^2 \cdot 7 \cdot 67$	$2 \cdot 3^2 \cdot 107$	$2^3 \cdot 13 \cdot 19$	$2 \cdot 1013$	$2^2 \cdot 3 \cdot 173$
27	77	$3^2 \cdot 7 \cdot 29$	$41 \cdot 47$	$3 \cdot 659$	$31 \cdot 67$
28	78	$2^2 \cdot 457$	$2 \cdot 3 \cdot 313$	$2^3 \cdot 241$	$2 \cdot 23 \cdot 43$	$2^2 \cdot 3 \cdot 13^2$	$2 \cdot 1039$
29	79	$31 \cdot 59$	$3 \cdot 643$	$3^3 \cdot 7 \cdot 11$
30	80	$2 \cdot 3 \cdot 5 \cdot 61$	$2^3 \cdot 5 \cdot 47$	$2 \cdot 5 \cdot 193$	$2^2 \cdot 3^2 \cdot 5 \cdot 11$	$2 \cdot 5 \cdot 7 \cdot 29$	$2^5 \cdot 5 \cdot 13$
31	81	$3^2 \cdot 11 \cdot 19$	$7 \cdot 283$	$3 \cdot 677$
32	82	$2^3 \cdot 229$	$2 \cdot 941$	$2^2 \cdot 3 \cdot 7 \cdot 23$	$2 \cdot 991$	$2^4 \cdot 127$	$2 \cdot 3 \cdot 347$
33	83	$3 \cdot 13 \cdot 47$	$7 \cdot 269$	$3 \cdot 661$	$19 \cdot 107$
34	84	$2 \cdot 7 \cdot 131$	$2^2 \cdot 3 \cdot 157$	$2 \cdot 967$	$2^6 \cdot 31$	$2 \cdot 3^2 \cdot 113$	$2^2 \cdot 521$
35	85	$5 \cdot 367$	$5 \cdot 13 \cdot 29$	$3^2 \cdot 5 \cdot 43$	$5 \cdot 397$	$5 \cdot 11 \cdot 37$	$3 \cdot 5 \cdot 139$
36	86	$2^2 \cdot 3^3 \cdot 17$	$2 \cdot 23 \cdot 41$	$2^4 \cdot 11^2$	$2 \cdot 3 \cdot 331$	$2^2 \cdot 5 \cdot 99$	$2 \cdot 7 \cdot 149$
37	87	$11 \cdot 167$	$3 \cdot 17 \cdot 37$	$13 \cdot 149$	$3 \cdot 7 \cdot 97$
38	88	$2 \cdot 919$	$2^5 \cdot 59$	$2 \cdot 3 \cdot 17 \cdot 19$	$2^2 \cdot 7 \cdot 71$	$2 \cdot 1019$	$2^3 \cdot 3^2 \cdot 29$
39	89	$3 \cdot 613$	$7 \cdot 277$	$3^2 \cdot 13 \cdot 17$
40	90	$2^4 \cdot 5 \cdot 23$	$2 \cdot 3^3 \cdot 5 \cdot 7$	$2^2 \cdot 5 \cdot 97$	$2 \cdot 5 \cdot 199$	$2^3 \cdot 3 \cdot 5 \cdot 17$	$2 \cdot 5 \cdot 11 \cdot 19$
41	91	$7 \cdot 263$	$31 \cdot 61$	$3 \cdot 647$	$11 \cdot 181$	$13 \cdot 157$	$3 \cdot 17 \cdot 41$
42	92	$2 \cdot 3 \cdot 307$	$2^2 \cdot 11 \cdot 43$	$2 \cdot 971$	$2^3 \cdot 3 \cdot 83$	$2 \cdot 1021$	$2^2 \cdot 523$
43	93	$19 \cdot 97$	$3 \cdot 631$	$29 \cdot 67$	$3^2 \cdot 227$	$7 \cdot 13 \cdot 23$
44	94	$2^2 \cdot 461$	$2 \cdot 947$	$2^3 \cdot 3^3$	$2 \cdot 997$	$2^2 \cdot 7 \cdot 73$	$2 \cdot 3 \cdot 349$
45	95	$3^2 \cdot 5 \cdot 41$	$5 \cdot 379$	$5 \cdot 389$	$3 \cdot 5 \cdot 7 \cdot 19$	$5 \cdot 409$	$5 \cdot 419$
46	96	$2 \cdot 13 \cdot 71$	$2^3 \cdot 3 \cdot 79$	$2 \cdot 7 \cdot 139$	$2^2 \cdot 499$	$2 \cdot 3 \cdot 11 \cdot 31$	$2^4 \cdot 131$
47	97	$7 \cdot 271$	$3 \cdot 11 \cdot 59$	$23 \cdot 89$	$3^2 \cdot 233$
48	98	$2^3 \cdot 3 \cdot 7 \cdot 11$	$2^2 \cdot 13 \cdot 73$	$2^2 \cdot 487$	$2 \cdot 3^3 \cdot 37$	2^{11}	$2 \cdot 1049$
49	99	43^2	$3^2 \cdot 211$	$3 \cdot 683$
50	100	$2 \cdot 5^2 \cdot 37$	$2^2 \cdot 5^2 \cdot 19$	$2 \cdot 3 \cdot 5^2 \cdot 13$	$2^4 \cdot 5^3$	$2 \cdot 5^2 \cdot 41$	$2^2 \cdot 3 \cdot 5^2 \cdot 7$

Prime Numbers and Factors, 2100-2400.

From To	2100 2150	2150 2200	2200 2250	2250 2300	2300 2350	2350 2400
0 50	$2^2 \cdot 3 \cdot 5^2 \cdot 7$	$2 \cdot 5^2 \cdot 43$	$2^3 \cdot 5^2 \cdot 11$	$2 \cdot 3^2 \cdot 5^3$	$2^2 \cdot 5^2 \cdot 23$	$2 \cdot 5^2 \cdot 47$
1 51	11·191	$3^2 \cdot 239$	$31 \cdot 71$	$3 \cdot 13 \cdot 59$
2 52	2·1051	$2^3 \cdot 269$	$2 \cdot 3 \cdot 367$	$2^2 \cdot 563$	$2 \cdot 1151$	$2^4 \cdot 3 \cdot 7^2$
3 53	$3 \cdot 701$	$3 \cdot 751$	$7^2 \cdot 57$	$13 \cdot 181$
4 54	$2^3 \cdot 263$	$2 \cdot 3 \cdot 359$	$2^2 \cdot 19 \cdot 29$	$2 \cdot 7^2 \cdot 23$	$2^8 \cdot 3^2$	$2 \cdot 11 \cdot 107$
5 55	$5 \cdot 421$	$5 \cdot 431$	$3^2 \cdot 5 \cdot 7^2$	$5 \cdot 11 \cdot 41$	$5 \cdot 461$	$3 \cdot 5 \cdot 157$
6 56	$2 \cdot 3^4 \cdot 13$	$2^2 \cdot 7^2 \cdot 11$	$2 \cdot 1103$	$2^4 \cdot 3 \cdot 47$	$2 \cdot 1153$	$2^2 \cdot 19 \cdot 31$
7 57	$7^2 \cdot 43$	$3 \cdot 719$	$37 \cdot 61$	$3 \cdot 769$
8 58	$2^2 \cdot 17 \cdot 31$	$2 \cdot 13 \cdot 83$	$2^5 \cdot 3 \cdot 23$	$2 \cdot 1129$	$2^2 \cdot 577$	$2 \cdot 3^2 \cdot 131$
9 59	$3 \cdot 19 \cdot 37$	$17 \cdot 127$	47^2	$3^2 \cdot 251$	$7 \cdot 337$
10 60	$2 \cdot 5 \cdot 211$	$2^4 \cdot 3^3 \cdot 5$	$2 \cdot 5 \cdot 13 \cdot 17$	$2^2 \cdot 5 \cdot 113$	$2 \cdot 3 \cdot 5 \cdot 7 \cdot 11$	$2^3 \cdot 5 \cdot 59$
11 61	$3 \cdot 11 \cdot 67$	$7 \cdot 17 \cdot 19$	$3 \cdot 787$
12 62	$2^6 \cdot 3 \cdot 11$	$2 \cdot 23 \cdot 47$	$2^2 \cdot 7 \cdot 79$	$2 \cdot 3 \cdot 13 \cdot 29$	$2^3 \cdot 17^2$	$2 \cdot 1181$
13 63	$3 \cdot 7 \cdot 103$	$31 \cdot 73$	$3^2 \cdot 257$	$17 \cdot 139$
14 64	$2 \cdot 7 \cdot 151$	$2^2 \cdot 541$	$2 \cdot 3^3 \cdot 41$	$2^3 \cdot 283$	$2 \cdot 13 \cdot 89$	$2^2 \cdot 3 \cdot 197$
15 65	$3^2 \cdot 5 \cdot 47$	$5 \cdot 433$	$5 \cdot 443$	$3 \cdot 5 \cdot 151$	$5 \cdot 463$	$5 \cdot 11 \cdot 43$
16 66	$2^2 \cdot 23^2$	$2 \cdot 3 \cdot 19^2$	$2^3 \cdot 277$	$2 \cdot 11 \cdot 103$	$2^2 \cdot 3 \cdot 193$	$2 \cdot 7 \cdot 13^2$
17 67	$29 \cdot 73$	$11 \cdot 197$	$3 \cdot 739$	$7 \cdot 331$	$3^2 \cdot 263$
18 68	$2 \cdot 3 \cdot 353$	$2^3 \cdot 271$	$2 \cdot 1109$	$2^2 \cdot 3^4 \cdot 7$	$2 \cdot 19 \cdot 61$	$2^6 \cdot 37$
19 69	$13 \cdot 163$	$3^2 \cdot 241$	$7 \cdot 317$	$3 \cdot 773$	$23 \cdot 103$
20 70	$2^3 \cdot 5 \cdot 53$	$2 \cdot 5 \cdot 7 \cdot 31$	$2^2 \cdot 3 \cdot 5 \cdot 37$	$2 \cdot 5 \cdot 227$	$2^4 \cdot 5 \cdot 29$	$2 \cdot 3 \cdot 5 \cdot 79$
21 71	$3 \cdot 7 \cdot 101$	$13 \cdot 167$	$3 \cdot 757$	$11 \cdot 211$
22 72	$2 \cdot 1061$	$2^2 \cdot 3 \cdot 181$	$2 \cdot 11 \cdot 101$	$2^5 \cdot 71$	$2 \cdot 3^3 \cdot 43$	$2^2 \cdot 593$
23 73	$11 \cdot 193$	$41 \cdot 53$	$3^2 \cdot 13 \cdot 19$	$23 \cdot 101$	$3 \cdot 7 \cdot 113$
24 74	$2^2 \cdot 3^2 \cdot 59$	$2 \cdot 1087$	$2^4 \cdot 139$	$2 \cdot 3 \cdot 379$	$2^2 \cdot 7 \cdot 83$	$2 \cdot 1187$
25 75	$5^3 \cdot 17$	$3 \cdot 5^2 \cdot 29$	$5^2 \cdot 89$	$5^2 \cdot 7 \cdot 13$	$3 \cdot 5^2 \cdot 31$	$5^3 \cdot 19$
26 76	$2 \cdot 1063$	$2^7 \cdot 17$	$2 \cdot 3 \cdot 7 \cdot 53$	$2^2 \cdot 569$	$2 \cdot 1163$	$2^3 \cdot 3^3 \cdot 11$
27 77	$3 \cdot 709$	$7 \cdot 311$	$17 \cdot 131$	$3^2 \cdot 11 \cdot 23$	$13 \cdot 179$
28 78	$2^4 \cdot 7 \cdot 19$	$2 \cdot 3^2 \cdot 11^2$	$2^2 \cdot 557$	$2 \cdot 17 \cdot 67$	$2^3 \cdot 3 \cdot 97$	$2 \cdot 29 \cdot 41$
29 79	$3 \cdot 743$	$43 \cdot 53$	$17 \cdot 137$	$3 \cdot 13 \cdot 61$
30 80	$2 \cdot 3 \cdot 5 \cdot 71$	$2^2 \cdot 5 \cdot 109$	$2 \cdot 5 \cdot 223$	$2^3 \cdot 3 \cdot 5 \cdot 19$	$2 \cdot 5 \cdot 233$	$2^2 \cdot 5 \cdot 7 \cdot 17$
31 81	$3 \cdot 727$	$23 \cdot 97$	$3^2 \cdot 7 \cdot 37$
32 82	$2^2 \cdot 13 \cdot 41$	$2 \cdot 1091$	$2^3 \cdot 3^2 \cdot 31$	$2 \cdot 7 \cdot 163$	$2^2 \cdot 11 \cdot 53$	$2 \cdot 3 \cdot 397$
33 83	$3^3 \cdot 79$	$37 \cdot 59$	$7 \cdot 11 \cdot 29$	$3 \cdot 761$
34 84	$2 \cdot 11 \cdot 97$	$2^3 \cdot 3 \cdot 7 \cdot 13$	$2 \cdot 1117$	$2^2 \cdot 571$	$2 \cdot 3 \cdot 389$	$2^4 \cdot 149$
35 85	$5 \cdot 7 \cdot 61$	$5 \cdot 19 \cdot 23$	$3 \cdot 5 \cdot 149$	$5 \cdot 457$	$5 \cdot 467$	$3^2 \cdot 5 \cdot 53$
36 86	$2^3 \cdot 3 \cdot 89$	$2 \cdot 1093$	$2^2 \cdot 13 \cdot 43$	$2 \cdot 3^2 \cdot 127$	$2^5 \cdot 73$	$2 \cdot 1193$
37 87	3^7	$3 \cdot 19 \cdot 41$	$7 \cdot 11 \cdot 31$
38 88	$2 \cdot 1069$	$2^2 \cdot 547$	$2 \cdot 3 \cdot 373$	$2^4 \cdot 11 \cdot 13$	$2 \cdot 7 \cdot 167$	$2^2 \cdot 3 \cdot 199$
39 89	$3 \cdot 23 \cdot 31$	$11 \cdot 199$	$3 \cdot 7 \cdot 109$
40 90	$2^2 \cdot 5 \cdot 107$	$2 \cdot 3 \cdot 5 \cdot 73$	$2^6 \cdot 5 \cdot 7$	$2 \cdot 5 \cdot 229$	$2^2 \cdot 3^2 \cdot 5 \cdot 13$	$2 \cdot 5 \cdot 239$
41 91	$7 \cdot 313$	$3^3 \cdot 83$	$29 \cdot 79$	$3 \cdot 797$
42 92	$2 \cdot 3^2 \cdot 7 \cdot 17$	$2^4 \cdot 137$	$2 \cdot 19 \cdot 59$	$2^2 \cdot 3 \cdot 191$	$2 \cdot 1171$	$2^2 \cdot 13 \cdot 23$
43 93	$3 \cdot 17 \cdot 43$	$3 \cdot 11 \cdot 71$
44 94	$2^5 \cdot 67$	$2 \cdot 1097$	$2^2 \cdot 3 \cdot 11 \cdot 17$	$2 \cdot 31 \cdot 37$	$2^3 \cdot 293$	$2 \cdot 3^2 \cdot 7 \cdot 19$
45 95	$3 \cdot 5 \cdot 11 \cdot 13$	$5 \cdot 439$	$5 \cdot 449$	$3^3 \cdot 5 \cdot 17$	$5 \cdot 7 \cdot 67$	$5 \cdot 479$
46 96	$2 \cdot 29 \cdot 37$	$2^2 \cdot 3^2 \cdot 61$	$2 \cdot 1123$	$2^3 \cdot 7 \cdot 41$	$2 \cdot 3 \cdot 17 \cdot 23$	$2^2 \cdot 599$
47 97	$19 \cdot 113$	13^3	$3 \cdot 7 \cdot 107$	$3 \cdot 17 \cdot 47$
48 98	$2^2 \cdot 3 \cdot 179$	$2 \cdot 7 \cdot 151$	$2^3 \cdot 281$	$2 \cdot 3 \cdot 383$	$2^2 \cdot 587$	$2 \cdot 11 \cdot 109$
49 99	$7 \cdot 307$	$3 \cdot 733$	$13 \cdot 173$	$11^2 \cdot 19$	$3^4 \cdot 29$
50 100	$2 \cdot 5^2 \cdot 43$	$2^3 \cdot 5^2 \cdot 11$	$2 \cdot 3^2 \cdot 5^3$	$2^2 \cdot 5^2 \cdot 23$	$2 \cdot 5^2 \cdot 47$	$2^5 \cdot 3 \cdot 5^2$

Prime Numbers and Factors, 2400-2700.

From To		2400 2450	2450 2500	2500 2550	2550 2600	2600 2650	2650 2700
0	50	2 ⁵ ·3·5 ²	2·5 ² ·7 ²	2 ² ·5 ⁴	2·3·5 ² ·17	2 ³ ·5 ² ·13	2·5 ² ·53
1	51	7 ⁴	3·19·43	41·61	3 ² ·17 ²	11·241
2	52	2·1201	2 ² ·613	2·3 ² ·139	2 ³ ·11·29	2·1301	2 ² ·3·13·17
3	53	3 ³ ·89	11·223	3·23·37	19·137	7·379
4	54	2 ² ·601	2·3·409	2 ³ ·313	2·1277	2 ² ·3·7·31	2·1327
5	55	5·13·37	5·491	3·5·167	5·7·73	5·521	3 ² ·5·59
6	56	2·3·401	2 ³ ·307	2·7·179	2 ² ·3 ² ·71	2·1303	2 ⁵ ·83
7	57	29·83	3 ³ ·7·13	23·109	3·11·79
8	58	2 ³ ·7·43	2·1229	2 ² ·3·11·19	2·1279	2 ⁴ ·163	2·3·443
9	59	3·11·73	13·193	3·853
10	60	2·5·241	2 ² ·3·5·41	2·5·251	2 ⁹ ·5	2·3 ² ·5·29	2 ² ·5·7·19
11	61	23·107	3 ⁴ ·31	13·197	7·373	3·887
12	62	2 ² ·3 ² ·67	2·1231	2 ⁴ ·157	2·3·7·61	2 ² ·653	2·11 ³
13	63	19·127	3·821	7·359	11·233	3·13·67
14	64	2·17·71	2 ⁵ ·7·11	2·3·419	2 ² ·641	2·1307	2 ³ ·3 ² ·37
15	65	3·5·7·23	5·17·29	5·503	3 ³ ·5·19	5·523	5·13·41
16	66	2 ⁴ ·151	2·3 ² ·137	2 ² ·17·37	2·1283	2 ³ ·3·109	2·31·43
17	67	3·839	17·151	3·7·127
18	68	2·3·13·31	2 ² ·617	2·1259	2 ³ ·3·107	2·7·11·17	2 ² ·23·29
19	69	41·59	3·823	11·229	7·367	3 ³ ·97	17·157
20	70	2 ² ·5·11 ²	2·5·13·19	2 ³ ·3 ² ·5·7	2·5·257	2 ² ·5·131	2·3·5·89
21	71	3 ² ·269	7·353	3·857
22	72	2·7·173	2 ³ ·3·103	2·13·97	2 ² ·643	2·3·19·23	2 ⁴ ·167
23	73	3·29 ²	31·83	43·61	3 ⁵ ·11
24	74	2 ³ ·3·101	2·1237	2 ² ·631	2·3 ² ·11·13	2 ⁶ ·41	2·7·191
25	75	5 ² ·97	3 ² ·5 ² ·11	5 ² ·101	5 ² ·103	3·5 ³ ·7	5 ² ·107
26	76	2·1213	2 ² ·619	2·3·421	2 ⁴ ·7·23	2·13·101	2 ² ·3·223
27	77	3·809	7·19 ²	3·859	37·71
28	78	2 ² ·607	2·3·7·59	2 ⁵ ·79	2·1289	2 ² ·3 ² ·73	2·13·103
29	79	7·347	37·67	3 ² ·281	11·239	3·19·47
30	80	2·3 ³ ·5	2 ⁴ ·5·31	2·5·11·23	2 ² ·3·5·43	2·5·263	2 ³ ·5·67
31	81	11·13·17	3·827	29·89	3·877	7·383
32	82	2 ⁷ ·19	2·17·73	2 ² ·3·211	2·1291	2 ³ ·7·47	2·3 ² ·149
33	83	3·811	13·191	17·149	3 ² ·7·41
34	84	2·1217	2 ² ·3 ³ ·23	2·7·181	2 ³ ·17·19	2·3·439	2 ² ·11·61
35	85	5·487	5·7·71	3·5·13 ²	5·11·47	5·17·31	3·5·179
36	86	2 ² ·3·7·29	2·11·113	2 ³ ·317	2·3·431	2 ² ·659	2·17·79
37	87	3·829	43·59	13·199	3 ² ·293
38	88	2·23·53	2 ³ ·311	2 ² ·3 ³ ·47	2 ² ·647	2·1319	2 ⁷ ·3·7
39	89	3 ² ·271	19·131	3·863	7·13·29
40	90	2 ³ ·5·61	2·3·5·83	2 ² ·5·127	2·5·7·37	2 ⁴ ·3·5·11	2·5·269
41	91	47·53	3·7·11 ²	19·139	3 ² ·13·23
42	92	2·3·11·37	2 ² ·7·89	2·31·41	2 ⁵ ·3 ⁴	2·1321	2 ² ·673
43	93	7·349	3 ² ·277	3·881
44	94	2 ² ·13·47	2·29·43	2 ⁴ ·3·53	2·1297	2 ² ·661	2·3·449
45	95	3·5·163	5·499	5·509	3·5·173	5·23 ²	5·7 ² ·11
46	96	2·1223	2 ⁶ ·3·13	2·19·67	2 ² ·11·59	2·3 ³ ·7 ²	2 ³ ·337
47	97	11·227	3 ² ·283	7 ² ·53	3·29·31
48	98	2 ⁴ ·3 ² ·17	2·1249	2 ² ·7 ² ·13	2·3·433	2 ³ ·331	2·19·71
49	99	31·79	3·7 ² ·17	23·113	3·883
50	100	2·5 ² ·7 ²	2 ² ·5 ⁴	2·3·5 ² ·17	2 ³ ·5 ² ·13	2·5 ² ·53	2 ² ·3 ³ ·5 ²

Prime Numbers and Factors, 2700-3000.

From To		2700 2750	2750 2800	2800 2850	2850 2900	2900 2950	2950 3000
0	50	2 ² ·3 ³ ·5 ²	2·5 ³ ·11	2 ⁴ ·5 ² ·7	2·3·5 ² ·19	2 ² ·5 ² ·29	2·5 ² ·59
1	51	37·73	3·7·131	3·967	13·227
2	52	2 ² ·7·193	2 ⁶ ·43	2·3·467	2 ² ·23·31	2·1451	2 ⁴ ·3 ² ·41
3	53	3 ² ·17·53	3 ² ·317
4	54	2 ⁴ ·13 ²	2·3 ² ·17	2 ² ·701	2·1427	2 ³ ·3·11 ²	2·7·211
5	55	5·541	5·19·29	3·5·11·17	5·571	5·7·83	3·5·197
6	56	2·3·11·41	2 ² ·13·53	2·23·61	2 ³ ·3·7·17	2·1453	2 ² ·739
7	57	3·919	7·401	3 ² ·17·19
8	58	2 ² ·677	2·7·197	2 ³ ·3 ³ ·13	2·1429	2 ² ·727	2·3·17·29
9	59	3 ² ·7·43	31·89	53 ²	3·953	11·269
10	60	2·5·271	2 ³ ·3·5·23	2·5·281	2 ² ·5·11·13	2·3·5·97	2 ⁴ ·5·37
11	61	11·251	3·937	41·71	3 ² ·7·47
12	62	2 ³ ·3·113	2·1381	2 ² ·19·37	2·3 ³ ·53	2 ⁵ ·7·13	2·1481
13	63	3 ² ·307	29·97	7·409	3·971
14	64	2·23·59	2 ² ·691	2·3·7·67	2 ⁴ ·179	2·31·47	2 ² ·3·13·19
15	65	3·5·181	5·7·79	5·563	3·5·191	5·11·53	5·593
16	66	2 ² ·7·97	2·3·461	2 ⁸ ·11	2·1433	2 ² ·3 ⁶	2·1483
17	67	11·13·19	3 ² ·313	47·61	3·23·43
18	68	2·3 ² ·151	2 ⁴ ·173	2·1409	2 ² ·3·239	2·1459	2 ³ ·7·53
19	69	3·13·71	19·151	3·7·139
20	70	2 ⁵ ·5·17	2·5·277	2 ² ·3·5·47	2·5·7·41	2 ³ ·5·73	2·3 ³ ·5·11
21	71	3·907	17·163	7·13·31	3 ² ·11·29	23·127
22	72	2·1361	2 ² ·3 ² ·7·11	2·17·83	2 ³ ·359	2·3·487	2 ² ·743
23	73	7·389	47·59	3·941	13 ² ·17	37·79	3·991
24	74	2 ² ·3·227	2·19·73	2 ³ ·353	2·3·479	2 ² ·17·43	2·1487
25	75	5 ² ·109	3·5 ² ·37	5 ² ·113	5 ³ ·23	3 ² ·5 ² ·13	5 ² ·7·17
26	76	2·29·47	2 ³ ·347	2·3 ² ·157	2 ² ·719	2·7·11·19	2 ⁵ ·3·31
27	77	3 ³ ·101	11·257	3·7·137	13·229
28	78	2 ³ ·11·31	2·3·463	2 ² ·7·101	2·1439	2 ⁴ ·3·61	2·1489
29	79	7·397	3·23·41	29·101	3 ² ·331
30	80	2·3·5·7·13	2 ² ·5·139	2·5·283	2 ⁶ ·3 ² ·5	2·5·293	2 ² ·5·149
31	81	3 ³ ·103	19·149	43·67	3·977	11·271
32	82	2 ² ·683	2·13·107	2 ⁴ ·3·59	2·11·131	2 ² ·733	2·3·7·71
33	83	3·911	11 ² ·23	3·31 ²	7·419	19·157
34	84	2·1367	2 ⁵ ·3·29	2·13·109	2 ² ·7·103	2·3 ² ·163	2 ³ ·373
35	85	5·547	5·557	3 ⁴ ·5·7	5·577	5·587	3·5·199
36	86	2 ⁴ ·3 ² ·19	2·7·199	2 ² ·709	2·3·13·37	2 ³ ·367	2·1493
37	87	7·17·23	3·929	3·11·89	29·103
38	88	2·37 ²	2 ² ·17·41	2·3·11·43	2 ³ ·19 ²	2·13·113	2 ² ·3 ² ·83
39	89	3·11·83	17·167	3 ³ ·107	7 ² ·61
40	90	2 ² ·5·137	2·3 ² ·5·31	2 ³ ·5·71	2·5·17 ²	2 ² ·3·5·7 ²	2·5·13·23
41	91	3·947	7 ² ·59	17·173	3·997
42	92	2·3·457	2 ³ ·349	2·7 ² ·29	2 ² ·3·241	2·1471	2 ⁴ ·11·17
43	93	13·211	3·7 ² ·19	11·263	3 ³ ·109	41·73
44	94	2 ² ·7 ³	2·11·127	2 ² ·3 ² ·79	2·1447	2 ⁷ ·23	2·3·499
45	95	3 ² ·5·61	5·13·43	5·569	3·5·193	5·19·31	5·599
46	96	2·1373	2 ² ·3·233	2·1423	2 ⁴ ·181	2·3·491	2 ² ·7·107
47	97	41·67	3·13·73	7·421	3 ⁴ ·37
48	98	2 ² ·3·229	3·1399	2 ⁵ ·89	2·3 ² ·7·23	2 ² ·11·67	2·1499
49	99	3 ² ·311	7·11·37	13·223	3·983
50	100	2·5 ³ ·11	2 ⁴ ·5 ² ·7	2·3·5 ² ·19	2 ² ·5 ² ·29	2·5 ² ·59	2 ³ ·3·5 ³

Prime Numbers and Factors, 3000-3300.

From To	3000 3050	3050 3100	3100 3150	3150 3200	3200 3250	3250 3300
0	50	$2^3 \cdot 3 \cdot 5^3$	$2 \cdot 5^2 \cdot 61$	$2^2 \cdot 5^2 \cdot 31$	$2 \cdot 3^2 \cdot 5^2 \cdot 7$	$2 \cdot 5^2 \cdot 13$
1	51	$3^3 \cdot 113$	7443	23137
2	52	$2 \cdot 19 \cdot 79$	$2^2 \cdot 7 \cdot 109$	$2 \cdot 3 \cdot 11 \cdot 47$	$2^4 \cdot 197$	$2^2 \cdot 3 \cdot 271$
3	53	$3 \cdot 7 \cdot 11 \cdot 13$	4371	29107	31051
4	54	$2^2 \cdot 751$	$2 \cdot 3 \cdot 509$	$2^5 \cdot 97$	$2 \cdot 19 \cdot 83$	$2^2 \cdot 3^2 \cdot 89$
5	55	$5 \cdot 601$	$5 \cdot 13 \cdot 47$	$3^3 \cdot 5 \cdot 23$	5631	5641
6	56	$2 \cdot 3^2 \cdot 167$	$2^4 \cdot 191$	21553	$2^2 \cdot 3 \cdot 263$	$2 \cdot 7 \cdot 229$
7	57	$31 \cdot 97$	31019	13239	71141	31069
8	58	$2^6 \cdot 47$	$2 \cdot 11 \cdot 139$	$2^2 \cdot 3 \cdot 7 \cdot 37$	21579	$2^3 \cdot 401$
9	59	$3 \cdot 17 \cdot 59$	$7 \cdot 19 \cdot 23$	$3^5 \cdot 13$
10	60	$2 \cdot 5 \cdot 7 \cdot 43$	$2^2 \cdot 3^2 \cdot 5 \cdot 17$	$2 \cdot 5 \cdot 311$	$2^3 \cdot 5 \cdot 79$	$2 \cdot 3 \cdot 5 \cdot 107$
11	61	$3 \cdot 17 \cdot 61$	29109	$13^2 \cdot 19$
12	62	$2^2 \cdot 3 \cdot 251$	$2 \cdot 1531$	$2^3 \cdot 389$	$2 \cdot 3 \cdot 17 \cdot 31$	$2^2 \cdot 11 \cdot 73$
13	63	$23 \cdot 131$	31021	11283	$3^3 \cdot 7 \cdot 17$
14	64	$2 \cdot 11 \cdot 137$	$2^3 \cdot 383$	$2 \cdot 3^2 \cdot 173$	$2^2 \cdot 7 \cdot 113$	$2 \cdot 1607$
15	65	$3^2 \cdot 5 \cdot 67$	5613	$5 \cdot 7 \cdot 89$	$3 \cdot 5 \cdot 211$	5643
16	66	$2^3 \cdot 13 \cdot 29$	$2 \cdot 3 \cdot 7 \cdot 73$	$2^2 \cdot 19 \cdot 41$	$2 \cdot 1583$	$2^4 \cdot 3 \cdot 67$
17	67	$7 \cdot 431$	31039
18	68	$2 \cdot 3 \cdot 503$	$2^2 \cdot 13 \cdot 59$	21559	$2^3 \cdot 3^2 \cdot 11$	21609
19	69	$3^2 \cdot 11 \cdot 31$	$3 \cdot 29 \cdot 37$
20	70	$2^2 \cdot 5 \cdot 151$	$2 \cdot 5 \cdot 307$	$2^4 \cdot 3 \cdot 5 \cdot 13$	$2 \cdot 5 \cdot 317$	$2^2 \cdot 5 \cdot 7 \cdot 23$
21	71	$3 \cdot 19 \cdot 53$	3783	$3 \cdot 7 \cdot 151$
22	72	$2 \cdot 1511$	$2^{10} \cdot 3$	$2 \cdot 7 \cdot 223$	$2^2 \cdot 13 \cdot 61$	$2 \cdot 3^2 \cdot 179$
23	73	7439	$3^2 \cdot 347$	19167	11293
24	74	$2^4 \cdot 3^3 \cdot 7$	$2 \cdot 29 \cdot 53$	$2^2 \cdot 11 \cdot 71$	$2 \cdot 3 \cdot 23^2$	$2^3 \cdot 13 \cdot 31$
25	75	$5^2 \cdot 11^2$	$3 \cdot 5^2 \cdot 41$	5^5	$5^2 \cdot 127$	$3 \cdot 5^2 \cdot 43$
26	76	$2 \cdot 17 \cdot 89$	$2^2 \cdot 769$	$2 \cdot 3 \cdot 521$	$2^3 \cdot 397$	$2 \cdot 1613$
27	77	$3 \cdot 1009$	17181	5359	$3^2 \cdot 353$	7461
28	78	$2^2 \cdot 757$	$2 \cdot 3^4 \cdot 19$	$2^3 \cdot 17 \cdot 23$	$2 \cdot 7 \cdot 227$	$2^2 \cdot 3 \cdot 269$
29	79	$13 \cdot 233$	$3 \cdot 7 \cdot 149$	$11 \cdot 17^2$
30	80	$2 \cdot 3 \cdot 5 \cdot 101$	$2^3 \cdot 5 \cdot 7 \cdot 11$	$2 \cdot 5 \cdot 313$	$2^2 \cdot 3 \cdot 5 \cdot 53$	$2 \cdot 5 \cdot 17 \cdot 19$
31	81	7433	$3 \cdot 13 \cdot 79$	31101	$3^2 \cdot 359$
32	82	$2^3 \cdot 379$	$2 \cdot 23 \cdot 67$	$2^2 \cdot 3^3 \cdot 29$	$2 \cdot 37 \cdot 43$	$2^5 \cdot 101$
33	83	$3^2 \cdot 337$	$13 \cdot 241$	31061	5361
34	84	$2 \cdot 37 \cdot 41$	$2^2 \cdot 3 \cdot 257$	$2 \cdot 1567$	$2^4 \cdot 199$	$2 \cdot 3 \cdot 7^2 \cdot 11$
35	85	$5 \cdot 607$	5617	$3 \cdot 5 \cdot 11 \cdot 19$	$5 \cdot 7^2 \cdot 13$	5647
36	86	$2^2 \cdot 3 \cdot 11 \cdot 23$	$2 \cdot 1543$	$2^6 \cdot 7^2$	$2 \cdot 3^3 \cdot 59$	$2^2 \cdot 809$
37	87	$3^2 \cdot 7^3$	$3 \cdot 13 \cdot 83$
38	88	$2 \cdot 7^2 \cdot 31$	$2^4 \cdot 193$	$2 \cdot 3 \cdot 523$	$2^2 \cdot 797$	$2 \cdot 1619$
39	89	$3 \cdot 1013$	4373	31063	4179
40	90	$2^5 \cdot 5 \cdot 19$	$2 \cdot 3 \cdot 5 \cdot 103$	$2^2 \cdot 5 \cdot 157$	$2 \cdot 5 \cdot 11 \cdot 29$	$2^3 \cdot 3^4 \cdot 5$
41	91	$11 \cdot 281$	$3^2 \cdot 349$	7463
42	92	$2 \cdot 3^2 \cdot 13^2$	$2^2 \cdot 773$	$2 \cdot 1571$	$2^3 \cdot 3 \cdot 7 \cdot 19$	$2 \cdot 1621$
43	93	$17 \cdot 179$	$3 \cdot 1031$	7449	$31 \cdot 103$	$3 \cdot 23 \cdot 47$
44	94	$2^2 \cdot 761$	$2 \cdot 7 \cdot 13 \cdot 17$	$2^3 \cdot 3 \cdot 131$	$2 \cdot 1597$	$2^2 \cdot 811$
45	95	$3 \cdot 5 \cdot 7 \cdot 29$	5619	$5 \cdot 17 \cdot 37$	$3^2 \cdot 5 \cdot 71$	$5 \cdot 11 \cdot 59$
46	96	$2 \cdot 1523$	$2^3 \cdot 3^2 \cdot 43$	$2 \cdot 11^2 \cdot 13$	$2^2 \cdot 17 \cdot 47$	$2 \cdot 3 \cdot 541$
47	97	$11 \cdot 277$	$19 \cdot 163$	$3 \cdot 1049$	23139	$17 \cdot 191$
48	98	$2^3 \cdot 3 \cdot 127$	$2 \cdot 1549$	$2^2 \cdot 787$	$2 \cdot 3 \cdot 13 \cdot 41$	$2^4 \cdot 7 \cdot 29$
49	99	$3 \cdot 1033$	4767	7457	$3^2 \cdot 19^2$
50	100	$2 \cdot 5^2 \cdot 61$	$2^2 \cdot 5^2 \cdot 31$	$2 \cdot 3^2 \cdot 5^2 \cdot 7$	$2 \cdot 7 \cdot 5^2$	$2 \cdot 5^3 \cdot 13$
						$2^2 \cdot 3 \cdot 5^2 \cdot 11$

Prime Numbers and Factors, 3300-3600.

From To		3300 3350	3350 3400	3400 3450	3450 3500	3500 3550	3550 3600
0	50	2 ² ·3·5 ² ·11	2·5 ² ·67	2 ³ ·5 ² ·17	2·3·5 ² ·23	2 ² ·5 ³ ·7	2·5 ² ·71
1	51	3·1117	19·179	7·17·29	3 ² ·389	53·67
2	52	2·13·127	2 ³ ·419	2·3 ⁵ ·7	2 ² ·863	2·17·103	2 ³ ·3·37
3	53	3 ² ·367	7·479	41·83	3·1151	31·113	11·17·19
4	54	2 ³ ·7·59	2·3·13·43	2 ² ·23·37	2·11·157	2 ⁴ ·3·73	2·1777
5	55	5·661	5·11·61	3·5·227	5·691	5·701	3 ² ·5·79
6	56	2·3·19·29	2 ² ·839	2·13·131	2 ⁷ ·3 ³	2·1753	2 ² ·7·127
7	57	3 ² ·373	3·7·167
8	58	2 ² ·827	2·23·73	2 ⁴ ·3·71	2·7·13·19	2 ² ·877	2·3·593
9	59	3·1103	7·487	3·1153	11 ² ·29
10	60	2·5·331	2 ⁵ ·3·5·7	2·5·11·31	2 ² ·5·173	2·3 ³ ·5·13	2 ³ ·5·89
11	61	7·11·43	3 ² ·379	3·1187
12	62	2 ⁴ ·3 ² ·23	2·41 ²	2 ² ·853	2·3·577	2 ³ ·439	2·13·137
13	63	3·19·59	3·1171	7·509
14	64	2·1657	2 ² ·29 ²	2·3·569	2 ³ ·433	2·7·251	2 ² ·3 ⁴ ·11
15	65	3·5·13·17	5·673	5·683	3 ² ·5·7·11	5·19·37	5·23·31
16	66	2 ² ·829	2·3 ² ·11·17	2 ³ ·7·61	2·1733	2 ² ·3·293	2·1783
17	67	31·107	7·13·37	3·17·67	3·29·41
18	68	2·3·7·79	2 ³ ·421	2·1709	2 ² ·3·17 ²	2·1759	2 ⁴ ·223
19	69	3·1123	13·263	3 ² ·17·23	43·83
20	70	2 ³ ·5·83	2·5·337	2 ² ·3 ² ·5·19	2·5·347	2 ⁶ ·5·11	2·3·5·7·17
21	71	3 ⁴ ·41	11·311	3·13·89	7·503
22	72	2·11·151	2 ² ·3·281	2·29·59	2 ⁴ ·7·31	2·3·587	2 ² ·19·47
23	73	3·7·163	23·151	13·271	3 ² ·397
24	74	2 ² ·3·277	2·7·241	2 ⁵ ·107	2·3 ² ·193	2 ² ·881	2·1787
25	75	5 ² ·7·19	3 ³ ·5 ³	5 ² ·137	5 ² ·139	3·5 ² ·47	5 ² ·11·13
26	76	2·1663	2 ⁴ ·211	2·3·571	2 ² ·11·79	2·41·43	2 ³ ·3·149
27	77	3·1109	11·307	23·149	3·19·61	7 ² ·73
28	78	2 ⁸ ·13	2·3·563	2 ² ·857	2·37·47	2 ³ ·3 ² ·7 ²	2·1789
29	79	31·109	3 ³ ·127	7 ² ·71	3·1193
30	80	2·3 ² ·5·37	2 ² ·5·13 ²	2·5·7 ³	2 ³ ·3·5·29	2·5·353	2 ² ·5·179
31	81	3·7 ² ·23	47·73	59 ²	3·11·107
32	82	2 ² ·7 ² ·17	2·19·89	2 ³ ·3·11·13	2·1741	2 ² ·883	2·3 ² ·199
33	83	3·11·101	17·199	3 ⁴ ·43
34	84	2·1667	2 ³ ·3 ² ·47	2·17·101	2 ² ·13·67	2·3·19·31	2 ⁹ ·7
35	85	5·23·29	5·677	3·5·229	5·17·41	5·7·101	3·5·239
36	86	2 ³ ·3·139	2·1693	2 ² ·859	2·3·7·83	2 ⁴ ·13·17	2·11·163
37	87	47·71	3·1129	7·491	11·317	3 ³ ·131	17·211
38	88	2·1669	2 ² ·7·11 ²	2·3 ² ·191	2 ⁵ ·109	2·29·61	2 ² ·3·13·23
39	89	3 ² ·7·53	19·181	3·1163	37·97
40	90	2 ² ·5·167	2·3·5·113	2 ⁴ ·5·43	2·5·349	2 ² ·3·5·59	2·5·359
41	91	13·257	3·31·37	3 ³ ·7·19
42	92	2·3·557	2 ⁶ ·53	2·1721	2 ² ·3 ² ·97	2·7·11·23	2 ³ ·449
43	93	3 ² ·13·29	11·313	7·499	3·1181
44	94	2 ⁴ ·11·19	2·1697	2 ² ·3·7·41	2·1747	2 ³ ·443	2·3·599
45	95	3·5·223	5·7·97	5·13·53	3·5·233	5·709	5·719
46	96	2·7·239	2 ² ·3·283	2·1723	2 ³ ·19·23	2·3 ² ·197	2 ² ·29·31
47	97	43·79	3 ² ·383	13·269	3·11·109
48	98	2 ² ·3 ³ ·31	2·1699	2 ³ ·431	2·3·11·53	2 ² ·887	2·7·257
49	99	17·197	3·11·103	3·7·13 ²	59·61
50	100	2·5 ² ·67	2 ³ ·5 ² ·17	2·3·5 ² ·23	2 ² ·5 ³ ·7	2·5 ² ·71	2 ⁴ ·3 ² ·5 ²

Prime Numbers and Factors, 3600-3900.

From To	3600 3650	3650 3700	3700 3750	3750 3800	3800 3850	3850 3900
0	50	2 ⁴ ·3 ² ·5 ²	2 ⁵ ·2 ⁷³	2 ² ·5 ² ·37	2 ³ ·5 ² ·19	2 ⁵ ·2 ⁷ ·11
1	51	13·277	3 ² ·1217	11 ² ·31
2	52	2·1801	2 ² ·11·83	2 ³ ·617	2 ³ ·7·67	2 ² ·3 ² ·107
3	53	3·1201	13·281	7·23 ²	3 ³ ·139
4	54	2 ² ·17·53	2 ³ ·2 ⁷ ·29	2 ³ ·463	2 ² ·1877	2 ⁴ ·47
5	55	5·7·103	5·17·43	3 ⁵ ·13·19	5·751	3 ⁵ ·257
6	56	2 ³ ·601	2 ³ ·457	2·17·109	2 ² ·3·3·13	2 ² ·11·173
7	57	3 ² ·3·53	11·337	13·17 ²	3 ⁴ ·47
8	58	2 ³ ·11·41	2 ³ ·1·59	2 ² ·3 ² ·103	2 ² ·1879	2 ⁵ ·7·17
9	59	3 ² ·401	3·7·179	13·293
10	60	2 ⁵ ·19 ²	2 ² ·3·5·61	2 ⁵ ·7·53	2 ⁴ ·5·47	2 ² ·3·5·127
11	61	23·157	7·523	3·1237	37·103
12	62	2 ² ·3 ⁷ ·43	2 ² ·1831	2 ⁷ ·29	2 ³ ·2 ¹¹ ·19	2 ² ·953
13	63	3 ² ·11·37	47·79	53·71	3 ³ ·1·41
14	64	2 ² ·13·139	2 ⁴ ·229	2 ³ ·619	2 ² ·941	2 ² ·1907
15	65	3 ⁵ ·241	5·733	5·743	3 ⁵ ·5 ² ·1	5·7·109
16	66	2 ⁵ ·113	2 ³ ·13·47	2 ² ·929	2 ² ·7·269	2 ³ ·3 ² ·53
17	67	19·193	3 ² ·7·59	11·347
18	68	2 ³ ·3·67	2 ² ·7·131	2 ² ·11·13 ²	2 ³ ·3·157	2 ² ·3·83
19	69	7·11·47	3·1223	3·19·67
20	70	2 ² ·5·181	2 ⁵ ·367	2 ³ ·3·5·31	2 ⁵ ·13·29	2 ² ·5·191
21	71	3·17·71	61 ²	3 ² ·419
22	72	2·1811	2 ³ ·3 ³ ·17	2 ² ·1861	2 ² ·23·41	2 ³ ·7 ² ·13
23	73	3·17·73	7 ³ ·11
24	74	2 ³ ·3·151	2 ² ·11·167	2 ² ·7 ² ·19	2 ³ ·17·37	2 ⁴ ·239
25	75	5 ³ ·29	3 ⁵ ·2·7 ²	5 ² ·149	5 ² ·151	3 ² ·5 ² ·17
26	76	2 ⁷ ·2·37	2 ² ·919	2 ³ ·4 ² ·23	2 ⁶ ·59	2 ² ·1913
27	77	3 ² ·13·31	3·1259	43·89
28	78	2 ² ·907	2 ³ ·613	2 ⁴ ·233	2 ² ·1889	2 ² ·3·11·29
29	79	19·191	13·283	3·11·113	7·547
30	80	2 ³ ·5·11 ²	2 ⁵ ·5·23	2 ⁵ ·373	2 ² ·3 ³ ·5·7	2 ⁵ ·383
31	81	3 ² ·409	7·13·41	19·199	3·1277
32	82	2 ⁴ ·277	2 ² ·7·263	2 ² ·3·311	2 ³ ·1·61	2 ³ ·479
33	83	3 ⁷ ·173	29·127	3 ³ ·13·97
34	84	2 ² ·3·79	2 ² ·3·307	2 ² ·1867	3 ² ·11·43	2 ³ ·3 ⁷ ·1
35	85	5·727	5·11·67	3 ² ·5·83	5·757	5·13·59
36	86	2 ² ·3 ² ·101	2 ² ·19·97	2 ³ ·467	2 ³ ·631	2 ² ·7·137
37	87	3·1229	37·101	7·541	3·1279
38	88	2·17·107	2 ³ ·461	2 ³ ·7·89	2 ² ·947	2 ² ·19·101
39	89	3·1213	7·17·31	3 ² ·421	11·349
40	90	2 ³ ·5·7·13	2 ³ ·2 ⁵ ·41	2 ² ·5·11·17	2 ⁵ ·379	2 ³ ·3·5
41	91	11·331	3·29·43	17·223	23·167
42	92	2 ³ ·607	2 ² ·13·71	2·1871	2 ⁴ ·3·79	2 ² ·17·113
43	93	3·1231	19·197	3 ² ·7·61
44	94	2 ² ·911	2 ² ·1847	2 ⁵ ·3 ² ·13	2 ⁷ ·271	2 ² ·31 ²
45	95	3 ⁶ ·5	5·739	5·7·107	3 ⁵ ·11·23	5·769
46	96	2 ⁴ ·1823	2 ⁴ ·3 ⁷ ·11	2·1873	2 ² ·13·73	2 ³ ·641
47	97	7·521	3·1249
48	98	2 ⁶ ·3·19	2·43 ²	2 ² ·937	2 ³ ·2·11	2 ³ ·13·37
49	99	41·89	3 ³ ·137	23·163	29·131	3·1283
50	100	2 ⁵ ·2 ⁷³	2 ² ·5 ² ·37	2 ³ ·5 ⁴	2 ³ ·5 ² ·19	2 ² ·5 ² ·7·11

Prime Numbers and Factors, 3900-4200.

From To	3900 3950	3950 4000	4000 4050	4050 4100	4100 4150	4150 4200
0	50	$2^2 \cdot 3 \cdot 5^2 \cdot 13$	$2 \cdot 5^2 \cdot 79$	$2^5 \cdot 5^3$	$2 \cdot 3^4 \cdot 5^2$	$2^2 \cdot 5^2 \cdot 41$
1	51	$47 \cdot 83$	$3^2 \cdot 439$	$2 \cdot 5^2 \cdot 83$
2	52	$2 \cdot 1951$	$2^4 \cdot 13 \cdot 19$	$2 \cdot 3 \cdot 23 \cdot 29$	$2^2 \cdot 1013$	$3 \cdot 1367$
3	53	$3 \cdot 1301$	$59 \cdot 67$	$2 \cdot 7 \cdot 293$	$2^3 \cdot 3 \cdot 173$
4	54	$2^6 \cdot 61$	$2 \cdot 3 \cdot 659$	$2^2 \cdot 7 \cdot 11 \cdot 13$	$11 \cdot 373$
5	55	$5 \cdot 11 \cdot 71$	$5 \cdot 7 \cdot 113$	$3^2 \cdot 5 \cdot 89$	$2 \cdot 2027$	$2 \cdot 31 \cdot 67$
6	56	$2^3 \cdot 2 \cdot 7 \cdot 31$	$2^2 \cdot 23 \cdot 43$	$2 \cdot 2003$	$5 \cdot 811$	$3 \cdot 5 \cdot 277$
7	57	$3 \cdot 1319$	$2^3 \cdot 3 \cdot 13^2$	$2^2 \cdot 1039$
8	58	$2^2 \cdot 977$	$2 \cdot 1979$	$2^3 \cdot 3 \cdot 167$	$3 \cdot 37^2$
9	59	$3 \cdot 1303$	$37 \cdot 107$	$19 \cdot 211$	$2 \cdot 2029$	$2^2 \cdot 13 \cdot 79$
10	60	$2 \cdot 5 \cdot 17 \cdot 23$	$2^3 \cdot 3^2 \cdot 5 \cdot 11$	$2 \cdot 5 \cdot 401$	$3^2 \cdot 11 \cdot 41$	$2 \cdot 3 \cdot 7 \cdot 11$
11	61	$17 \cdot 233$	$3 \cdot 7 \cdot 191$	$2 \cdot 5 \cdot 7 \cdot 29$	$2 \cdot 3 \cdot 5 \cdot 137$
12	62	$2^3 \cdot 3 \cdot 163$	$2 \cdot 7 \cdot 283$	$2^2 \cdot 17 \cdot 59$	$3 \cdot 19 \cdot 73$
13	63	$7 \cdot 13 \cdot 43$	$3 \cdot 1321$	$2 \cdot 3 \cdot 677$	$2 \cdot 2081$
14	64	$2 \cdot 19 \cdot 103$	$2^2 \cdot 991$	$2 \cdot 3^2 \cdot 223$	$17 \cdot 239$	$2^3 \cdot 457$
15	65	$3^8 \cdot 5 \cdot 29$	$5 \cdot 13 \cdot 61$	$5 \cdot 11 \cdot 73$	$2^5 \cdot 127$	$2 \cdot 11^2 \cdot 17$
16	66	$2^2 \cdot 11 \cdot 89$	$2 \cdot 3 \cdot 661$	$2^4 \cdot 251$	$3 \cdot 5 \cdot 271$	$5 \cdot 823$
17	67	$3 \cdot 13 \cdot 103$	$2 \cdot 19 \cdot 107$	$2^2 \cdot 3 \cdot 7^3$
18	68	$2 \cdot 3 \cdot 653$	$2^7 \cdot 31$	$2 \cdot 7^2 \cdot 41$	$7^2 \cdot 83$	$23 \cdot 179$
19	69	$3^4 \cdot 7^2$	$2^2 \cdot 3^2 \cdot 113$	$2 \cdot 29 \cdot 71$
20	70	$2^4 \cdot 5 \cdot 7^2$	$2 \cdot 5 \cdot 397$	$2^2 \cdot 3 \cdot 5 \cdot 67$	$13 \cdot 313$	$3 \cdot 1373$
21	71	$3 \cdot 1307$	$11 \cdot 19^2$	$2 \cdot 5 \cdot 11 \cdot 37$	$2^3 \cdot 5 \cdot 103$
22	72	$2 \cdot 37 \cdot 53$	$2^2 \cdot 3 \cdot 331$	$2 \cdot 2011$	$3 \cdot 23 \cdot 59$	$13 \cdot 317$
23	73	$29 \cdot 137$	$3^3 \cdot 149$	$2^3 \cdot 509$	$2 \cdot 3^2 \cdot 229$
24	74	$2^2 \cdot 3^2 \cdot 109$	$2 \cdot 1987$	$2^3 \cdot 503$	$7 \cdot 19 \cdot 31$
25	75	$5^2 \cdot 157$	$3 \cdot 5^2 \cdot 53$	$5^2 \cdot 7 \cdot 23$	$2 \cdot 3 \cdot 7 \cdot 97$	$2^2 \cdot 1031$
26	76	$2 \cdot 13 \cdot 151$	$2^3 \cdot 7 \cdot 71$	$2 \cdot 3 \cdot 11 \cdot 61$	$5^2 \cdot 163$	$3 \cdot 5^3 \cdot 11$
27	77	$3 \cdot 7 \cdot 11 \cdot 17$	$41 \cdot 97$	$2 \cdot 1019$	$2 \cdot 2063$
28	78	$2^3 \cdot 491$	$2 \cdot 3^2 \cdot 13 \cdot 17$	$2^2 \cdot 19 \cdot 53$	$3^3 \cdot 151$
29	79	$23 \cdot 173$	$3 \cdot 17 \cdot 79$	$2 \cdot 2039$	$2^5 \cdot 3 \cdot 43$
30	80	$2 \cdot 3 \cdot 5 \cdot 131$	$2^2 \cdot 5 \cdot 199$	$2 \cdot 5 \cdot 13 \cdot 31$	$3 \cdot 7 \cdot 199$
31	81	$3 \cdot 1327$	$29 \cdot 139$	$2^4 \cdot 3 \cdot 5 \cdot 17$	$2 \cdot 5 \cdot 7 \cdot 59$
32	82	$2^2 \cdot 983$	$2 \cdot 11 \cdot 181$	$2^6 \cdot 3^2 \cdot 7$	$7 \cdot 11 \cdot 53$	$3^5 \cdot 17$
33	83	$3^2 \cdot 19 \cdot 23$	$7 \cdot 569$	$37 \cdot 109$	$2 \cdot 13 \cdot 157$	$2^2 \cdot 1033$
34	84	$2 \cdot 7 \cdot 281$	$2^4 \cdot 3 \cdot 83$	$2 \cdot 2017$	$3 \cdot 1361$
35	85	$5 \cdot 787$	$5 \cdot 797$	$3 \cdot 5 \cdot 269$	$2^2 \cdot 1021$	$2 \cdot 3 \cdot 13 \cdot 53$
36	86	$2^5 \cdot 3 \cdot 41$	$2 \cdot 1993$	$2^2 \cdot 1009$	$5 \cdot 19 \cdot 43$	$5 \cdot 827$
37	87	$31 \cdot 127$	$3^2 \cdot 443$	$11 \cdot 367$	$2 \cdot 3^3 \cdot 227$	$2^3 \cdot 11 \cdot 47$
38	88	$2 \cdot 11 \cdot 179$	$2^2 \cdot 997$	$2 \cdot 3 \cdot 673$	$61 \cdot 67$	$3 \cdot 7 \cdot 197$
39	89	$3 \cdot 13 \cdot 101$	$7 \cdot 577$	$2 \cdot 7 \cdot 73$	$2 \cdot 2069$
40	90	$2^2 \cdot 5 \cdot 197$	$2 \cdot 3 \cdot 5 \cdot 7 \cdot 19$	$2^3 \cdot 5 \cdot 101$	$3 \cdot 29 \cdot 47$
41	91	$7 \cdot 563$	$13 \cdot 307$	$3^2 \cdot 449$	$59 \cdot 71$
42	92	$2 \cdot 3^3 \cdot 73$	$2^3 \cdot 499$	$2 \cdot 43 \cdot 47$	$2 \cdot 5 \cdot 409$	$2^2 \cdot 3^2 \cdot 5 \cdot 23$
43	93	$3 \cdot 11^3$	$13 \cdot 311$	$41 \cdot 101$
44	94	$2^3 \cdot 17 \cdot 29$	$2 \cdot 1997$	$2^2 \cdot 3 \cdot 337$	$2^2 \cdot 3 \cdot 11 \cdot 31$	$2 \cdot 19 \cdot 109$
45	95	$3 \cdot 5 \cdot 263$	$5 \cdot 17 \cdot 47$	$5 \cdot 809$	$3 \cdot 1381$
46	96	$2 \cdot 1973$	$2^2 \cdot 3^3 \cdot 37$	$2 \cdot 7 \cdot 17^2$	$2 \cdot 23 \cdot 89$	$2^4 \cdot 7 \cdot 37$
47	97	$7 \cdot 571$	$3 \cdot 19 \cdot 71$	$3^2 \cdot 5 \cdot 7 \cdot 13$	$5 \cdot 829$
48	98	$2^2 \cdot 3 \cdot 7 \cdot 47$	$2 \cdot 1999$	$2^4 \cdot 11 \cdot 23$	2^{12}	$2 \cdot 3 \cdot 691$
49	99	$11 \cdot 359$	$3 \cdot 31 \cdot 43$	$17 \cdot 241$	$11 \cdot 13 \cdot 29$
50	100	$2 \cdot 5^2 \cdot 79$	$2^5 \cdot 5^3$	$2 \cdot 3^4 \cdot 5^2$	$2 \cdot 3 \cdot 683$	$2^2 \cdot 17 \cdot 61$
					$3^2 \cdot 461$
					$2 \cdot 5^2 \cdot 41$	$2 \cdot 5^2 \cdot 83$
						$2^3 \cdot 3 \cdot 5^2 \cdot 7$

Prime Numbers and Factors, 4200-4500.

From To		4200 4250	4250 4300	4300 4350	4350 4400	4400 4450	4450 4500
0	50	2 ³ ·3·5 ² ·7	2·5 ³ ·17	2 ² ·5 ² ·43	2·3·5 ² ·29	2 ⁴ ·5 ² ·11	2·5 ² ·89
1	51	3 ¹³ ·109	11·17·23	19·229	3 ³ ·163
2	52	2·11·191	2 ² ·1063	2·3 ² ·239	2 ⁸ ·17	2·31·71	2 ² ·3·7·53
3	53	3 ² ·467	13·331	3·1451	7·17·37	61·73
4	54	2 ² ·1051	2·3·709	2 ⁴ ·269	2·7·311	2 ² ·3·367	2·17·131
5	55	5·29 ²	5·23·37	3·5·7·41	5·13·67	5·881	3 ⁴ ·5·11
6	56	2·3·701	2 ⁵ ·7·19	2·2153	2 ² ·3 ² ·11 ²	2·2203	2 ³ ·557
7	57	7·601	3 ² ·11·43	59·73	3·13·113
8	58	2 ⁴ ·263	2·2129	2 ² ·3·359	2·2179	2 ³ ·19·29	2·3·743
9	59	3·23·61	31·139	3·1453	7 ³ ·13
10	60	2·5·421	2 ² ·3·5·71	2·5·431	2 ³ ·5·109	2·3 ² ·5·7 ²	2 ² ·5·223
11	61	3 ² ·479	7 ² ·89	11·401	3·1487
12	62	2 ² ·3 ⁴ ·13	2·2131	2 ³ ·7 ² ·11	2·3·7 ² ·7	2 ² ·1103	2·23·97
13	63	11·383	3·7 ² ·29	19·227	3·1471
14	64	2·7 ² ·43	2 ³ ·13·41	2·3·719	2 ² ·1091	2·2207	2 ⁴ ·3 ² ·31
15	65	3·5·281	5·853	5·863	3 ² ·5·97	5·883	5·19·47
16	66	2 ³ ·17·31	2·3 ³ ·79	2 ² ·13·83	2·37·59	2 ⁶ ·3·23	2·7·11·29
17	67	17·251	3·1439	11·397	7·631	3·1489
18	68	2·3·19·37	2 ² ·11·97	2·17·127	2 ⁴ ·3·7·13	2·47 ²	2 ² ·1117
19	69	3·1423	7·617	17·257	3 ² ·491	41·109
20	70	2 ² ·5·211	2·5·7·61	2 ⁵ ·3 ³ ·5	2·5·19·23	2 ² ·5·13·17	2·3·5·149
21	71	3 ² ·7·67	29·149	3·31·47	17·263
22	72	2·2111	2 ⁴ ·3·89	2·2161	2 ² ·1093	2·3·11·67	2 ³ ·13·43
23	73	41·103	3·11·131	3 ² ·7·71
24	74	2 ⁷ ·3·11	2·2137	2 ² ·23·47	2·3 ⁷	3 ² ·7·79	2·2237
25	75	5 ² ·13 ²	3 ² ·5 ² ·19	5 ² ·173	5 ⁴ ·7	3·5 ² ·59	5 ² ·179
26	76	2·2113	2 ² ·1069	2·3·7·103	2 ³ ·547	2·2213	2 ² ·3·373
27	77	3·1409	7·13·47	3·1459	19·233	11 ² ·37
28	78	2 ² ·7·151	2·3·23·31	2 ³ ·541	2·11·199	2 ² ·3 ³ ·41	2·2239
29	79	11·389	3 ² ·13·37	29·151	43·103	3·1493
30	80	2·3 ² ·5·47	2 ³ ·5·107	2·5·433	2 ² ·3·5·73	2·5·443	2 ⁷ ·5·7
31	81	3·1427	61·71	13·337	3·7·211
32	82	2 ³ ·23 ²	2·2141	2 ² ·3·19 ²	2·7·313	2 ⁴ ·277	2·3 ³ ·83
33	83	3·17·83	7·619	3 ² ·487	11·13·31
34	84	2·29·73	2 ² ·3 ² ·7·17	2·11·197	2 ⁵ ·137	2·3·739	2 ² ·19·59
35	85	5·7·11 ²	5·857	3·5·17 ²	5·877	5·887	3·5·13·23
36	86	2 ² ·3·353	2·2143	2 ⁴ ·271	2·3·17·43	2 ² ·1109	2·2243
37	87	19·223	3·1429	41·107	3 ² ·17·29	7·641
38	88	2·13·163	2 ⁶ ·67	2·3 ² ·241	2 ² ·1097	2·7·317	2 ³ ·3·11·17
39	89	3 ³ ·157	3·7·11·19	23·193	67 ²
40	90	2 ⁴ ·5·53	2·3·5·11·13	2 ² ·5·7·31	2·5·439	2 ³ ·3·5·37	2·5·449
41	91	7·613	3·1447	3 ² ·499
42	92	2·3·7·101	2 ² ·29·37	2·13·167	2 ³ ·3 ² ·61	2·2221	2 ² ·1123
43	93	3 ⁴ ·53	43·101	23·191	3·1481
44	94	2 ² ·1061	2·19·113	2 ³ ·3·181	2·13 ³	2 ² ·11·101	2·3·7·107
45	95	3·5·283	5·859	5·11·79	3·5·293	5·7·127	5·29·31
46	96	2·11·193	2 ³ ·3·179	2·41·53	2 ² ·7·151	2·3 ² ·13·19	2 ⁴ ·281
47	97	31·137	3 ³ ·7·23	3·1499
48	98	2 ³ ·3 ² ·59	2·7·307	2 ² ·1087	2·3·733	2 ⁵ ·139	2·13·173
49	99	7·607	3·1433	53·83	3·1483	11·409
50	100	2·5 ³ ·17	2 ² ·5 ² ·43	2·3·5 ² ·29	2 ⁴ ·5 ² ·11	2·5 ² ·89	2 ² ·3 ² ·5 ³

Prime Numbers and Factors, 4500-4800.

From To	4500 4550	4550 4600	4600 4650	4650 4700	4700 4750	4750 4800
0 50	2 ² ·3 ² ·5 ³	2 ⁵ ·7·13	2 ³ ·5 ² ·23	2 ³ ·5 ² ·31	2 ² ·5 ² ·47	2·5 ³ ·19
1 51	7·643	3 ³ ·7·41	43·107	3·1567
2 52	2·2251	2 ³ ·569	2 ³ ·13·59	2 ² ·1163	2·2351	2 ⁴ ·3 ³ ·11
3 53	3·19·79	29·157	3 ² ·11·47	7 ² ·97
4 54	2 ³ ·563	2 ³ ·2 ¹¹ ·23	2 ² ·1151	2 ² ·13·179	2 ⁵ ·3·7 ²	2·2377
5 55	5·17·53	5·911	3·5·307	5·7 ² ·19	5·941	3·5·317
6 56	2 ³ ·751	2 ² ·17·67	2·7 ² ·47	2 ⁴ ·3·97	2·13·181	2 ² ·29·41
7 57	3·7 ² ·31	17·271	3 ² ·523	67·71
8 58	2 ² ·7 ² ·23	2·43·53	2 ⁹ ·3 ²	2·17·137	2 ² ·11·107	2·3·13·61
9 59	3 ³ ·167	47·97	11·419	3·1553	17·277
10 60	2·5·11·41	2 ⁴ ·3·5·19	2·5·461	2 ² ·5·233	2·3·5·157	2 ³ ·5·7·17
11 61	13·347	3·29·53	59·79	7·673	3 ² ·23 ²
12 62	2 ⁵ ·3·47	2·2281	2 ² ·1153	2 ³ ·7·37	2 ³ ·19·31	2·2381
13 63	3 ³ ·13 ²	7·659	3·1571	11·433
14 64	2·37·61	2 ² ·7·163	2 ³ ·769	2 ³ ·11·53	2·2357	2 ² ·3·397
15 65	3·5·7·43	5·11·83	5·13·71	3·5·311	5·23·41	5·953
16 66	2 ² ·1129	2·3·761	2 ³ ·577	2·2333	2 ² ·3 ² ·131	2·2383
17 67	3 ⁵ ·19	13·359	53·89	3·7·227
18 68	2·3 ² ·251	2 ³ ·571	2·2309	2 ² ·3·389	2·7·337	2 ⁵ ·149
19 69	3·1523	31·149	7·23·29	3·11 ² ·13	19·251
20 70	2 ³ ·5·113	2·5·457	2 ² ·3·5·7·11	2·5·467	2 ⁴ ·5·59	2·3 ² ·5·53
21 71	3·11·137	7·653	3 ³ ·173	13·367
22 72	2·7·17·19	2 ² ·3 ² ·127	2·2311	2 ⁶ ·73	2·3·787	2 ² ·1193
23 73	17·269	3·23·67	3·37·43
24 74	2 ² ·3·13·29	2·2287	2 ⁴ ·17 ²	2·3·19·41	2 ² ·1181	2·7·11·31
25 75	5 ² ·181	3·5 ² ·61	5 ³ ·37	5 ² ·11·17	3 ³ ·5 ² ·7	5 ² ·191
26 76	2·31·73	2 ⁵ ·11·13	2·3 ² ·257	2 ² ·7·167	2 ² ·17·139	2 ³ ·3·199
27 77	3 ² ·503	23·199	7·661	3·1559	29·163	17·281
28 78	2 ⁴ ·283	2·3·7·109	2 ² ·13·89	2·2339	2 ³ ·3·197	2·2389
29 79	7·647	19·241	3·1543	3 ⁴ ·59
30 80	2·3·5·151	2 ² ·5·229	2·5·463	2 ³ ·3 ² ·5·13	2·5·11·43	2 ² ·5·239
31 81	23·197	3 ² ·509	11·421	31·151	3·19·83	7·683
32 82	2 ² ·11·103	2·29·79	2 ³ ·3·193	2·2341	2 ² ·7·13 ²	2·3·797
33 83	3·1511	41·113	3·7·223
34 84	2·2267	2 ³ ·3·191	2·7·331	2 ² ·1171	2·3 ² ·263	2 ⁴ ·13·23
35 85	5·907	5·7·131	3 ² ·5·103	5·937	5·947	3·5·11·29
36 86	2 ³ ·3 ⁴ ·7	2·2293	2 ² ·19·61	2·3·11·71	2 ⁷ ·37	2·2393
37 87	13·349	3·11·139	43·109	3·1579
38 88	2·2269	2 ² ·31·37	2·3·773	2 ⁴ ·293	2·23·103	2 ² ·3 ² ·7·19
39 89	3·17·89	13·353	3 ² ·521	7·677
40 90	2 ² ·5·227	2·3 ³ ·5·17	2 ⁵ ·5·29	2·5·7·67	2 ² ·3·5·79	2·5·479
41 91	19·239	3·7·13·17	11·431	3·1597
42 92	2·3·757	2 ⁴ ·7·41	2·11·211	2 ² ·3·17·23	2·2371	2 ³ ·599
43 93	7·11·59	3·1531	13·19 ²	3 ² ·17·31
44 94	2 ⁶ ·71	2·2297	2 ² ·3 ³ ·43	2·2347	2 ³ ·593	2·3·17·47
45 95	3 ² ·5·101	5·919	5·929	3·5·313	5·13·73	5·7·137
46 96	2·2273	2 ² ·3·383	2·23·101	2 ³ ·587	2·3·7·113	2 ² ·11·109
47 97	3·1549	7·11·61	47·101	3 ² ·13·41
48 98	2 ² ·3·379	2·11 ² ·19	2 ³ ·7·83	2 ³ ·4·29	2 ² ·1187	2·2399
49 99	3 ² ·7·73	37·127	3·1583
50 100	2·5 ² ·7·13	2 ³ ·5 ² ·23	2·3·5 ² ·31	2 ² ·5 ² ·47	2·5 ³ ·19	2 ⁶ ·3·5 ²

Prime Numbers and Factors, 4800-5100.

From To		4800 4850	4850 4900	4900 4950	4950 5000	5000 5050	5050 5100
0	50	2 ⁶ ·3·5 ²	2·5 ² ·97	2 ² ·5 ² ·7 ²	2·3 ² ·5 ² ·11	2 ³ ·5 ⁴	2·5 ² ·101
1	51	3 ² ·7 ² ·11	13 ² ·29	3·1667
2	52	2·7 ⁴	2 ² ·1213	2·3·19·43	2 ³ ·619	2·41·61	2 ² ·3·421
3	53	3·1601	23·211	3·13·127	31·163
4	54	2 ² ·1201	2·3·809	2 ³ ·613	2·2477	2 ² ·3 ² ·139	2·7·19 ²
5	55	5·31 ²	5·971	3 ² ·5·109	5·991	5·7·11·13	3·5·337
6	56	2 ³ ·3 ³ ·89	2 ³ ·607	2·11·223	2 ² ·3·7·59	2·2503	2 ⁶ ·79
7	57	11·19·23	3·1619	7·701	3·1669	13·389
8	58	2 ³ ·601	2·7·347	2 ² ·3·409	2·37·67	2 ⁴ ·313	2·3 ² ·281
9	59	3·7·229	43·113	3 ² ·19·29
10	60	2·5·13·37	2 ² ·3 ⁵ ·5	2·5·491	2 ⁵ ·5·31	2·3·5·167	2 ² ·5·11·23
11	61	17·283	3·1637	11 ² ·41	3·7·241
12	62	2 ² ·3·401	2·11·13·17	2 ⁴ ·307	2·3·827	2 ² ·7·179	2·2531
13	63	3·1621	17 ³	7·709	3 ² ·557	61·83
14	64	2·29·83	2 ³ ·19	2·3 ³ ·7·13	2 ² ·17·73	2·23·109	2 ³ ·3·211
15	65	3 ² ·5·107	5·7·139	5·983	3·5·331	5·17·59	5·1013
16	66	2 ⁴ ·7·43	2·3·811	2 ² ·1229	2·13·191	2 ³ ·3·11·19	2·17·149
17	67	31·157	3·11·149	29·173	3 ² ·563
18	68	2·3·11·73	2 ² ·1217	2·2459	2 ³ ·3 ³ ·23	2·13·193	2 ² ·7·181
19	69	61·79	3 ² ·541	3·7·239	37·137
20	70	2 ² ·5·241	2·5·487	2 ³ ·3·5·41	2·5·7·71	2 ² ·5·251	2·3·5·13 ²
21	71	3·1607	7·19·37	3·1657	11·461
22	72	2·2411	2 ³ ·3·7·29	2·23·107	2 ² ·11·113	2·3 ⁴ ·31	2 ⁴ ·317
23	73	7·13·53	11·443	3 ² ·547	3·19·89
24	74	2 ³ ·3 ² ·67	2·2437	2 ² ·1231	2·3·829	2 ⁵ ·157	2·43·59
25	75	5 ² ·193	3·5 ³ ·13	5 ² ·197	5 ² ·199	3·5 ² ·67	5 ² ·7·29
26	76	2·19·127	2 ² ·23·53	2·3·821	2 ⁴ ·311	2·7·359	2 ² ·3 ³ ·47
27	77	3·1609	13·379	3 ² ·7·79	11·457
28	78	2 ² ·17·71	2·3 ² ·271	2 ⁶ ·7·11	2·19·131	2 ² ·3·419	2·2539
29	79	11·439	7·17·41	3·31·53	13·383	47·107	3·1693
30	80	2·3·5·7·23	2 ⁴ ·5·61	2·5·17·29	2 ² ·3·5·83	2·5·503	2 ³ ·5·127
31	81	3·1627	17·293	3 ² ·13·43
32	82	2 ⁵ ·151	2·2441	2 ² ·3 ² ·137	2·47·53	2 ³ ·17·37	2·3·7·11 ²
33	83	3 ³ ·179	19·257	3·11·151	7·719	13·17·23
34	84	2·2417	2 ² ·3·11·37	2·2467	2 ³ ·7·89	2·3·839	2 ² ·31·41
35	85	5·967	5·977	3·5·7·47	5·997	5·19·53	3 ² ·5·113
36	86	2 ² ·3·13·31	2·7·349	2 ³ ·617	2·3 ² ·277	2 ² ·1259	2·2543
37	87	7·691	3 ³ ·181	3·23·73
38	88	2·41·59	2 ³ ·13·47	2·3·823	2 ² ·29·43	2·11·229	2 ⁵ ·3·53
39	89	3·1613	11·449	3·1663	7·727
40	90	2 ³ ·5·11 ²	2·3·5·163	2 ² ·5·13·19	2·5·499	2 ⁴ ·3 ² ·5·7	2·5·509
41	91	47·103	67·73	3 ⁴ ·61	7·23·31	71 ²	3·1697
42	92	2·3 ² ·269	2 ² ·1223	2·7·353	2 ⁷ ·3·13	2·2521	2 ² ·19·67
43	93	29·167	3·7·233	3·41 ²	11·463
44	94	2 ² ·7·173	2·2447	2 ⁴ ·3·103	2·11·227	2 ² ·13·97	2·3 ² ·283
45	95	3·5·17·19	5·11·89	5·23·43	3 ³ ·5·37	5·1009	5·1019
46	96	2·2423	2 ⁵ ·3 ² ·17	2·2473	2 ² ·1249	2·3·29 ²	2 ³ ·7 ² ·13
47	97	37·131	59·83	3·17·97	19·263	7 ² ·103	3·1699
48	98	2 ⁴ ·3·101	2·31·79	2 ² ·1237	2·3·7 ² ·17	2 ³ ·631	2·2549
49	99	13·373	3·23·71	7 ² ·101	3 ³ ·21·17
50	100	2·5 ² ·97	2 ² ·5 ² ·7 ²	2·3 ² ·5 ² ·11	2 ³ ·5 ⁴	2·5 ² ·101	2 ² ·3·5 ² ·17

Prime Numbers and Factors, 5100-5400.

From To	5100 5150	5150 5200	5200 5250	5250 5300	5300 5350	5350 5400
0	50	2 ² ·3·5 ² ·17	2·5 ² ·103	2 ⁴ ·5 ² ·13	2·3·5 ³ ·7	2 ² ·5 ² ·53
1	51	3·17·101	7·743	59·89	3 ² ·19·31
2	52	2·2551	2 ⁵ ·7·23	2·3 ² ·17 ²	2 ² ·13·101	2·11·241
3	53	3 ⁶ ·7	11 ² ·43	3·17·103
4	54	2 ⁴ ·11·29	2·3·859	2 ² ·1301	2·37·71	2 ³ ·3·13·17
5	55	5·1021	5·1031	3·5·347	5·1051	5·1061
6	56	2·3·23·37	2 ² ·1289	2·19·137	3 ² ·3 ² ·73	2·7·379
7	57	3 ³ ·191	41·127	7·751	3·29·61
8	58	2 ² ·1277	2·2579	2 ³ ·3·7·31	2·11·239	2 ² ·1327
9	59	3·13·131	7·11·67	3·1753
10	60	2·5·7·73	2 ³ ·3·5·43	2·5·521	2 ² ·5·263	2·3 ² ·5·59
11	61	19·269	13·397	3 ³ ·193	47·113
12	62	2 ³ ·3 ² ·71	2·29·89	2 ² ·1303	2·3·877	2 ⁶ ·83
13	63	3·1721	13·401	19·277	3·7·11·23
14	64	2 ² ·557	2 ² ·1291	2·3·11·79	2 ⁴ ·7·47	2·2657
15	65	3·5·11·31	5·1033	5·7·149	3 ⁴ ·5·13	5·1063
16	66	2 ² ·1279	2·3 ² ·7·41	2 ⁵ ·163	2·2633	2 ² ·3·443
17	67	7·17·43	3·37·47	23·229	13·409
18	68	2·3·853	2 ⁴ ·17·19	2·2609	2 ² ·3·439	2·2659
19	69	3·1723	17·307	11·479	3 ³ ·197
20	70	2 ¹⁰ ·5	2·5·11·47	2 ² ·3 ² ·5·29	2·5·17·31	2 ³ ·5·7·19
21	71	3 ² ·569	23·227	3·7·251	17·313
22	72	2·13·197	2 ² ·3·431	2·7·373	2 ³ ·659	2·3·887
23	73	47·109	7·739	3·1741
24	74	2 ² ·3·7·61	2·13·199	2 ³ ·653	2·3 ² ·293	2 ² ·11 ³
25	75	5 ³ ·41	3 ² ·5 ² ·23	5 ² ·11·19	5 ² ·211	3·5 ² ·71
26	76	2·11·233	2 ³ ·647	2·3·13·67	2 ² ·1319	2·2663
27	77	3·1709	31·167	3·1759	7·761
28	78	2 ³ ·641	2·3·863	2 ² ·1307	2·7·13·29	2 ⁴ ·3 ² ·37
29	79	23·223	3 ² ·7·83	73 ²
30	80	2·3 ³ ·5·19	2 ² ·5·7·37	2·5·523	2 ⁵ ·3·5·11	2·5·13·41
31	81	7·733	3·11·157	3·1777
32	82	2 ² ·1283	2·2591	2 ⁴ ·3·109	2·19·139	2 ² ·31·43
33	83	3·29·59	71·73	3 ² ·587
34	84	2·17·151	2 ⁶ ·3 ⁴	2·2617	2 ² ·1321	2·3·7·127
35	85	5·13·79	5·17·61	3·5·349	5·7·151	5·11·97
36	86	2 ⁴ ·3·107	2·2593	2 ² ·7·11·17	2·3·881	2 ³ ·23·29
37	87	11·467	3·7·13·19	17·311	3 ² ·593
38	88	2·7·367	2 ² ·1297	2·3 ³ ·97	2 ³ ·661	2·17·157
39	89	3 ² ·571	13 ² ·31	3·41·43	19·281
40	90	2 ² ·5·257	2·3·5·173	2 ³ ·5·131	2·5·23 ²	2 ² ·3·5·89
41	91	53·97	29·179	3·1747	11·13·37	7 ² ·109
42	92	2·3·857	2 ³ ·11·59	2·2621	2 ² ·3 ³ ·7 ²	2·2671
43	93	37·139	3 ² ·577	7 ² ·107	67·79	3·13·137
44	94	2 ³ ·643	2·7 ² ·53	2 ² ·3·19·23	2·2647	2 ⁵ ·167
45	95	3·5·7 ³	5·1029	5·1049	3·5·353	5·1069
46	96	2·31·83	2 ² ·3·433	2·43·61	2 ⁴ ·331	2·3 ⁵ ·11
47	97	3 ² ·11·53
48	98	2 ² ·3 ² ·11·13	2·23·113	2 ⁷ ·41	2·3·883	2 ² ·7·191
49	99	19·271	3·1733	29·181	7·757	3·1783
50	100	2·5 ² ·103	2 ⁴ ·5 ² ·13	2·3·5 ³ ·7	2 ² ·5 ² ·53	2·5 ² ·107

Prime Numbers and Factors, 5400-5700.

From To	5400 5450	5450 5500	5500 5550	5550 5600	5600 5650	5650 5700
0	50	$2^3 \cdot 3^3 \cdot 5^2$	$2 \cdot 5^2 \cdot 109$	$2^2 \cdot 5^3 \cdot 11$	$2 \cdot 3 \cdot 5^2 \cdot 37$	$2 \cdot 5^2 \cdot 113$
1	51	11·491	$3 \cdot 23 \cdot 79$	$7 \cdot 13 \cdot 61$
2	52	$2 \cdot 37 \cdot 73$	$2^2 \cdot 29 \cdot 47$	$2 \cdot 3 \cdot 7 \cdot 131$	$2^4 \cdot 347$	$2^2 \cdot 3^2 \cdot 157$
3	53	$3 \cdot 1801$	$7 \cdot 19 \cdot 41$	$3^2 \cdot 617$
4	54	$2^2 \cdot 7 \cdot 193$	$2 \cdot 3^3 \cdot 101$	$2^7 \cdot 43$	$2 \cdot 2777$	$2^2 \cdot 3 \cdot 467$
5	55	$5 \cdot 23 \cdot 47$	$5 \cdot 1091$	$3 \cdot 5 \cdot 367$	$5 \cdot 11 \cdot 101$	$5 \cdot 19 \cdot 59$
6	56	$2 \cdot 3 \cdot 17 \cdot 53$	$2^4 \cdot 11 \cdot 31$	$2 \cdot 27 \cdot 53$	$2^2 \cdot 3 \cdot 463$	$5 \cdot 5 \cdot 13 \cdot 29$
7	57	$3 \cdot 17 \cdot 107$	$2^3 \cdot 7 \cdot 101$
8	58	$2^5 \cdot 13^2$	$2 \cdot 2729$	$2^2 \cdot 3^4 \cdot 17$	$2 \cdot 7 \cdot 397$
9	59	$3^2 \cdot 601$	$53 \cdot 103$	$7 \cdot 787$	$3 \cdot 17 \cdot 109$	$2 \cdot 3 \cdot 23 \cdot 41$
10	60	$2 \cdot 5 \cdot 541$	$2^2 \cdot 3 \cdot 5 \cdot 7 \cdot 13$	$2 \cdot 5 \cdot 19 \cdot 29$	$2^3 \cdot 5 \cdot 139$
11	61	7·773	$43 \cdot 127$	$3 \cdot 11 \cdot 167$	67·83	$2 \cdot 5 \cdot 283$
12	62	$2^2 \cdot 3 \cdot 11 \cdot 41$	$2 \cdot 2731$	$2^3 \cdot 13 \cdot 53$	$2 \cdot 3^3 \cdot 103$	$31 \cdot 181$
13	63	$3^2 \cdot 607$	$37 \cdot 149$	$2^2 \cdot 23 \cdot 61$
14	64	$2 \cdot 2707$	$2^3 \cdot 683$	$2 \cdot 3 \cdot 919$	$2^2 \cdot 13 \cdot 107$	$3 \cdot 1871$
15	65	$3 \cdot 5 \cdot 19^2$	$5 \cdot 1093$	$5 \cdot 1103$	$3 \cdot 5 \cdot 7 \cdot 53$	$2 \cdot 7 \cdot 401$
16	66	$2^3 \cdot 677$	$2 \cdot 3 \cdot 911$	$2^2 \cdot 7 \cdot 197$	$2 \cdot 11^2 \cdot 23$	$5 \cdot 11 \cdot 103$
17	67	$7 \cdot 11 \cdot 71$	$3^2 \cdot 613$	$19 \cdot 293$	$2^4 \cdot 3^3 \cdot 13$
18	68	$2 \cdot 3^2 \cdot 7 \cdot 43$	$2^2 \cdot 1367$	$2 \cdot 31 \cdot 89$	$2^6 \cdot 3 \cdot 29$	$41 \cdot 137$
19	69	$3 \cdot 1823$	$2 \cdot 53^2$
20	70	$2^2 \cdot 5 \cdot 271$	$2 \cdot 5 \cdot 547$	$2^4 \cdot 3 \cdot 5 \cdot 23$	$2 \cdot 5 \cdot 557$	$3 \cdot 1873$
21	71	$3 \cdot 13 \cdot 139$	$3^2 \cdot 619$
22	72	$2 \cdot 2711$	$2^5 \cdot 3^2 \cdot 19$	$2 \cdot 11 \cdot 251$	$2^2 \cdot 7 \cdot 199$	$2 \cdot 5 \cdot 281$
23	73	$11 \cdot 17 \cdot 29$	$13 \cdot 421$	$3 \cdot 7 \cdot 263$	$7 \cdot 11 \cdot 73$
24	74	$2^4 \cdot 3 \cdot 113$	$2 \cdot 7 \cdot 17 \cdot 23$	$2^2 \cdot 1381$	$2 \cdot 3 \cdot 929$	$2 \cdot 3 \cdot 937$
25	75	$5^2 \cdot 7 \cdot 31$	$3 \cdot 5^2 \cdot 73$	$5^2 \cdot 13 \cdot 17$	$5^2 \cdot 223$
26	76	$2^2 \cdot 2713$	$2^2 \cdot 37^2$	$2 \cdot 3^2 \cdot 307$	$2^3 \cdot 17 \cdot 41$	$2^3 \cdot 19 \cdot 37$
27	77	$3^4 \cdot 67$	$3 \cdot 11 \cdot 13^2$	$3^2 \cdot 5^4$
28	78	$2^2 \cdot 23 \cdot 59$	$2 \cdot 3 \cdot 11 \cdot 83$	$2^3 \cdot 691$	$2 \cdot 2789$	$2 \cdot 29 \cdot 97$
29	79	61·89	$3 \cdot 19 \cdot 97$	$7 \cdot 797$	$17 \cdot 331$
30	80	$2 \cdot 3 \cdot 5 \cdot 181$	$2^3 \cdot 5 \cdot 137$	$2 \cdot 5 \cdot 7 \cdot 79$	$2^2 \cdot 3^2 \cdot 5 \cdot 31$	$2^2 \cdot 3 \cdot 7 \cdot 67$
31	81	$3^3 \cdot 7 \cdot 29$	$13 \cdot 433$
32	82	$2^3 \cdot 7 \cdot 97$	$2 \cdot 2741$	$2^2 \cdot 3 \cdot 461$	$2 \cdot 2791$	$2 \cdot 5 \cdot 563$
33	83	$3 \cdot 1811$	$11 \cdot 503$	$3 \cdot 1861$	$3 \cdot 1877$
34	84	$2 \cdot 11 \cdot 13 \cdot 19$	$2^2 \cdot 3 \cdot 457$	$2 \cdot 2767$	$2^4 \cdot 349$	$2^9 \cdot 11$
35	85	$5 \cdot 1087$	$5 \cdot 1097$	$3^3 \cdot 5 \cdot 41$	$5 \cdot 1117$	$43 \cdot 131$
36	86	$2^2 \cdot 3^2 \cdot 151$	$2 \cdot 13 \cdot 211$	$2^5 \cdot 173$	$2 \cdot 3 \cdot 7^2 \cdot 19$	$2 \cdot 3^2 \cdot 313$
37	87	$3 \cdot 31 \cdot 59$	$7^2 \cdot 113$	$37 \cdot 151$	$5 \cdot 7^2 \cdot 23$
38	88	$2 \cdot 2719$	$2^4 \cdot 7^3$	$2 \cdot 3 \cdot 13 \cdot 71$	$2^2 \cdot 11 \cdot 127$	$2^2 \cdot 1409$
39	89	$3 \cdot 7^2 \cdot 37$	$11 \cdot 499$	$29 \cdot 191$	$3^5 \cdot 23$	$3 \cdot 1879$
40	90	$2^6 \cdot 5 \cdot 17$	$2 \cdot 3^2 \cdot 5 \cdot 61$	$2^2 \cdot 5 \cdot 277$	$2 \cdot 5 \cdot 13 \cdot 43$	$2 \cdot 2819$
41	91	$17^2 \cdot 19$	$3 \cdot 1847$
42	92	$2 \cdot 3 \cdot 907$	$2^2 \cdot 1373$	$2 \cdot 17 \cdot 163$	$2^3 \cdot 3 \cdot 233$	$3 \cdot 7 \cdot 271$
43	93	$3 \cdot 1831$	$23 \cdot 241$	$7 \cdot 17 \cdot 47$	$2^2 \cdot 1423$
44	94	$2^2 \cdot 1361$	$2 \cdot 41 \cdot 67$	$2^3 \cdot 3^2 \cdot 7 \cdot 11$	$2 \cdot 2797$	$3^3 \cdot 11 \cdot 19$
45	95	$3^2 \cdot 5 \cdot 11^2$	$5 \cdot 7 \cdot 157$	$5 \cdot 1109$	$3 \cdot 5 \cdot 373$	$2^2 \cdot 17 \cdot 83$
46	96	$2 \cdot 7 \cdot 389$	$2^3 \cdot 3 \cdot 229$	$2 \cdot 47 \cdot 59$	$2^2 \cdot 1399$	$2 \cdot 3 \cdot 13 \cdot 73$
47	97	$13 \cdot 419$	$23 \cdot 239$	$3 \cdot 43^2$	$29 \cdot 193$	$5 \cdot 11 \cdot 29$
48	98	$2^3 \cdot 3 \cdot 227$	$2 \cdot 2749$	$2^2 \cdot 19 \cdot 73$	$2 \cdot 3^2 \cdot 311$	$2 \cdot 3 \cdot 941$
49	99	$3^2 \cdot 13 \cdot 47$	$31 \cdot 179$	$11 \cdot 509$
50	100	$2 \cdot 5^2 \cdot 109$	$2^2 \cdot 5^3 \cdot 11$	$2 \cdot 3 \cdot 5^2 \cdot 37$	$2^3 \cdot 5^2 \cdot 7$	$3^3 \cdot 211$
						$2^4 \cdot 353$
						$3 \cdot 7 \cdot 269$
						$41 \cdot 139$
						$2^2 \cdot 3 \cdot 5 \cdot 19$

Prime Numbers and Factors, 5700-6000.

From To		5700 5750	5750 5800	5800 5850	5850 5900	5900 5950	5950 6000
0	50	2 ² ·3·5 ² ·19	2·5 ³ ·23	2 ³ ·5 ² ·29	2·3 ² ·5 ² ·13	2 ² ·5 ² ·59	2·5 ² ·7·17
1	51	3 ⁴ ·71	3·7·281	11·541
2	52	2·2851	2 ³ ·719	2·3·967	2 ² ·7·11·19	2·13·227	2 ⁶ ·3·31
3	53	3·1901	11·523	7·829	3·1951
4	54	2 ³ ·23·31	2·3·7·137	2 ² ·1451	2·2927	2 ⁴ ·3 ² ·41	2·13·229
5	55	5·7·163	5·1151	3 ³ ·5·43	5·1171	5·1181	3·5·397
6	56	2·3 ² ·317	2 ² ·1439	2·2903	2 ⁵ ·3·61	2·2953	2 ² ·1489
7	57	13·439	3·19·101	3·11·179	7·23·37
8	58	2 ² ·1427	2·2879	2 ⁴ ·3·11 ²	2·29·101	2 ² ·7·211	2·3 ² ·331
9	59	3·11·173	13·443	37·157	3 ³ ·7·31	19·311	59·101
10	60	2·5·571	2 ⁷ ·3 ² ·5	2·5·7·83	2 ² ·5·293	2·3·5·197	2 ³ ·5·149
11	61	7·823	3·13·149	23·257	3·1987
12	62	2 ⁴ ·3·7·17	2·43·67	2 ² ·1453	2·3·977	2 ³ ·739	2·11·271
13	63	29·197	3·17·113	11·13·41	3 ⁴ ·3	67·89
14	64	2·2857	2 ² ·11·131	2·3 ² ·17·19	2 ⁸ ·733	2·2957	2 ² ·3·7·71
15	65	3 ² ·5·127	5·1153	5·1163	3·5·17·23	5·7·13 ²	5·1193
16	66	2 ² ·1429	2·3·31 ²	2 ³ ·727	2·7·419	2 ² ·3·17·29	2·19·157
17	67	73·79	3·7·277	61·97	3 ³ ·13·17
18	68	2·3·953	2 ³ ·7·103	2·2909	2 ² ·3 ² ·163	2·11·269	2 ⁴ ·373
19	69	7·19·43	3 ² ·641	11·23 ²	3·1973	47·127
20	70	2 ³ ·5·11·13	2·5·577	2 ² ·3·5·97	2·5·587	2 ⁵ ·5·37	2·3·5·199
21	71	3·1907	29·199	3·19·103	31·191	7·853
22	72	2·2861	2 ² ·3·13·37	2·41·71	2 ⁴ ·367	2·3 ² ·7·47	2 ² ·1493
23	73	59·97	23·251	3 ² ·647	7·839	3·11·181
24	74	2 ² ·3 ³ ·53	2·2887	2 ⁶ ·7·13	2·3·11·89	2 ² ·1481	2·29·103
25	75	5 ² ·229	3·5 ² ·7·11	5 ² ·233	5 ³ ·47	3·5 ² ·79	5 ² ·239
26	76	2·7·409	2 ⁴ ·19 ²	2·3·971	2 ² ·13·113	2·2963	2 ³ ·3 ² ·83
27	77	3·23·83	53·109	3 ² ·653	43·139
28	78	2 ⁵ ·179	2·3 ³ ·107	2 ² ·31·47	2·2939	2 ³ ·3·13·19	2·7 ² ·61
29	79	17·337	3·29·67	7 ² ·11 ²	3·1993
30	80	2·3·5·191	2 ² ·5·17 ²	2·5·11·53	2 ³ ·3·5·7 ²	2·5·593	2 ² ·5·13·23
31	81	11·521	3·41·47	7 ³ ·17	3 ² ·659
32	82	2 ² ·1433	2·7 ² ·59	2 ³ ·3 ⁶	2·17·173	2 ² ·1483	2·3·997
33	83	3 ² ·7 ² ·13	19·307	3·37·53	17·349	31·193
34	84	2·47·61	2 ³ ·3·241	2·2917	2 ² ·1471	2·3·23·43	2 ⁵ ·11·17
35	85	5·31·37	5·13·89	3·5·389	5·11·107	5·1187	3 ² ·5·7·19
36	86	2 ³ ·3·239	2·11·263	2 ² ·1459	2·3 ³ ·109	2 ⁴ ·7·53	2·41·73
37	87	3 ² ·643	13·449	7·29 ²	3·1979
38	88	2·19·151	2 ² ·1447	2·3·7·139	2 ⁸ ·23	2·2969	2 ² ·3·499
39	89	3·1913	7·827	3·13·151	53·113
40	90	2 ² ·5·7·41	2·3·5·193	2 ⁴ ·5·73	2·5·19·31	2 ² ·3 ³ ·5·11	2·5·599
41	91	3 ² ·11·59	43·137	13·457	3·1997
42	92	2·3 ² ·11·29	2 ⁵ ·181	2·23·127	2 ² ·3·491	2·2971	2 ³ ·7·107
43	93	3·1931	71·83	3·7·283	13·461
44	94	2 ⁴ ·359	2·2897	2 ² ·3·487	2·7·421	2 ³ ·743	2·3 ⁴ ·37
45	95	3·5·383	5·19·61	5·7·167	3 ² ·5·131	5·29·41	5·11·109
46	96	2·13 ² ·17	2 ² ·3 ² ·7·23	2·37·79	2 ³ ·11·67	2·3·991	2 ² ·1499
47	97	7·821	11·17·31	3·1949	19·313	3·1999
48	98	2 ² ·3·479	2·13·223	2 ³ ·17·43	2·3·983	2 ² ·1487	2·2999
49	99	3·1933	17·347	3 ² ·661	7·857
50	100	2·5 ³ ·23	2 ³ ·5 ² ·29	2·3 ² ·5 ² ·13	2 ² ·5 ² ·59	2·5 ² ·7·17	2 ⁴ ·3·5 ³

Prime Numbers and Factors, 6000-6300.

From To		6000 6050	6050 6100	6100 6150	6150 6200	6200 6250	6250 6300
0	50	2 ⁴ ·3·5 ³	2·5 ² ·11 ²	2 ² ·5 ² ·61	2·3·5 ² ·41	2 ³ ·5 ² ·31	2·5 ⁵
1	51	17·353	3·2017	3 ² ·13·53	7·19·47
2	52	2·3001	2 ² ·17·89	2·3 ³ ·113	2 ³ ·769	2·7·443	2 ² ·3·521
3	53	3 ² ·23·29	17·359	3·7·293	13 ² ·37
4	54	2 ² ·19·79	2·3·1009	2 ³ ·7·109	2·17·181	2 ² ·3·11·47	2·53·59
5	55	5·1201	5·7·173	3·5·11·37	5·1231	5·17·73	3 ² ·5·139
6	56	2·3·7·11·13	2 ³ ·757	2·43·71	2 ² ·3 ⁴ ·19	2·29·107	2 ⁴ ·17·23
7	57	3 ² ·673	31·197	47·131	3·2069
8	58	2 ³ ·751	2·13·233	2 ² ·3·509	2·3079	2 ⁶ ·97	2·3·7·149
9	59	3·2003	73·83	41·149	3·2053	7·887	11·569
10	60	2·5·601	2 ² ·3·5·101	2·5·13·47	2 ⁴ ·5·7·11	2·3 ³ ·5·23	2 ² ·5·313
11	61	11·19·29	3 ² ·7·97	61·101	3·2087
12	62	2 ² ·3 ² ·167	2·7·433	2 ⁵ ·191	2·3·13·79	2 ² ·1553	2·31·101
13	63	7·859	3·43·47	3·19·109
14	64	2·31·97	2 ⁴ ·379	2·3·1019	2 ² ·23·67	2·13·239	2 ³ ·3 ³ ·29
15	65	3·5·401	5·1213	5·1223	3 ² ·5·137	5·11·113	5·7·179
16	66	2 ⁷ ·47	2·3 ² ·337	2 ² ·11·139	2·3083	2 ³ ·3·7·37	2·13·241
17	67	11·547	3·2039	7·881	3·2089
18	68	2·3·17·59	2 ² ·37·41	2·7·19·23	2 ³ ·3·257	2·3109	2 ² ·1567
19	69	13·463	3·7·17 ²	29·211	31·199	3 ² ·691
20	70	2 ² ·5·7·43	2·5·607	2 ³ ·3 ² ·5·17	2·5·617	2 ² ·5·311	2·3·5·11·19
21	71	3 ³ ·223	13·467	3·11 ² ·17
22	72	2·3011	2 ³ ·3·11·23	2·3061	2 ² ·1543	2·3·17·61	2 ⁷ ·7 ²
23	73	19·317	3·13·157	7 ² ·127	3 ² ·17·41
24	74	2 ³ ·3·251	2·3037	2 ² ·1531	2·3 ² ·7 ³	2 ⁴ ·389	2·3137
25	75	5 ² ·241	3 ⁵ ·5 ²	5 ³ ·7 ²	5 ² ·13·19	3·5 ² ·83	5 ² ·251
26	76	2·23·131	2 ² ·7 ² ·31	2·3·1021	2 ⁵ ·193	2·11·283	2 ² ·3·523
27	77	3·7 ² ·41	59·103	11·557	3·29·71	13·479
28	78	2 ² ·11·137	2·3·1013	2 ⁴ ·383	2·3089	2 ² ·3 ² ·173	2·43·73
29	79	3 ³ ·227	37·167	3·7·13·23
30	80	2·3 ² ·5·67	2 ⁶ ·5·19	2·5·613	2 ² ·3·5·103	2·5·7·89	2 ³ ·5·157
31	81	37·163	3·2027	7·883	3·31·67	11·571
32	82	2 ⁴ ·13·29	2·3041	2 ² ·3·7·73	2·11·281	2 ³ ·19·41	2·3 ² ·349
33	83	3·2011	7·11·79	3 ³ ·229	23·271	61·103
34	84	2·7·431	2 ² ·3 ² ·13 ²	2·3067	2 ³ ·773	2·3·1039	2 ² ·1571
35	85	5·17·71	5·1217	3·5·409	5·1237	5·29·43	3·5·419
36	86	2 ² ·3·503	2·17·179	2 ³ ·13·59	2·3·1031	2 ² ·1559	2·7·449
37	87	3·2029	17·19 ²	23·269	3 ⁴ ·7·11
38	88	2·3019	2 ³ ·761	2·3 ² ·11·31	2 ² ·7·13·17	2·3119	2 ⁴ ·3·131
39	89	3 ² ·11·61	7·877	3·2063	17·367	19·331
40	90	2 ³ ·5·151	2·3·5·7·29	2 ² ·5·307	2·5·619	2 ⁵ ·3·5·13	2·5·17·37
41	91	7·863	3·23·89	41·151	79 ²	3 ³ ·233
42	92	2·3·19·53	2 ² ·1523	2·37·83	2 ⁴ ·3 ² ·43	2·3121	2 ² ·11 ² ·13
43	93	3 ² ·677	11·563	3·2081	7·29·31
44	94	2 ² ·1511	2·11·277	2 ¹¹ ·3	2·19·163	2 ² ·7·223	2·3·1049
45	95	3·5·13·31	5·23·53	5·1229	3·5·7·59	5·1249	5·1259
46	96	2·3023	2 ⁴ ·3·127	2·7·439	2 ² ·1549	2·3 ² ·347	2 ³ ·787
47	97	7·13·67	3 ² ·683	3·2099
48	98	2 ⁵ ·3 ³ ·7	2·3049	2 ² ·29·53	2·3·1033	2 ³ ·11·71	2·47·67
49	99	23·263	3·19·107	11·13·43	3·2083
50	100	2·5 ² ·11 ²	2 ² ·5 ² ·61	2·3·5 ² ·41	2 ³ ·5 ² ·31	2·5 ⁵	2 ² ·3 ² ·5 ² ·7

Prime Numbers and Factors, 6300-6600.

From To	6300 6350	6350 6400	6400 6450	6450 6500	6500 6550	6550 6600
0	50	$2^2 \cdot 3^2 \cdot 5^2 \cdot 7$	$2 \cdot 5^2 \cdot 127$	$2^8 \cdot 5^2$	$2 \cdot 3 \cdot 5^2 \cdot 43$	$2^2 \cdot 5^3 \cdot 13$
1	51	$3 \cdot 29 \cdot 73$	$37 \cdot 173$	$3 \cdot 11 \cdot 197$
2	52	$2 \cdot 23 \cdot 137$	$2^4 \cdot 397$	$2 \cdot 3 \cdot 11 \cdot 97$	$2^2 \cdot 1613$	$2 \cdot 3251$
3	53	$3 \cdot 11 \cdot 191$	$19 \cdot 337$	$3^3 \cdot 239$	$7 \cdot 929$
4	54	$2^5 \cdot 197$	$2 \cdot 3^2 \cdot 353$	$2^2 \cdot 1601$	$2 \cdot 7 \cdot 461$	$2^3 \cdot 3 \cdot 271$
5	55	$5 \cdot 13 \cdot 97$	$5 \cdot 31 \cdot 41$	$3 \cdot 5 \cdot 7 \cdot 61$	$5 \cdot 1291$	$5 \cdot 1301$
6	56	$2 \cdot 3 \cdot 1051$	$2^2 \cdot 7 \cdot 227$	$2 \cdot 3203$	$2^3 \cdot 3 \cdot 269$	$2 \cdot 3253$
7	57	$7 \cdot 17 \cdot 53$	$3 \cdot 13 \cdot 163$	$43 \cdot 149$	$11 \cdot 587$	$3^3 \cdot 241$
8	58	$2^2 \cdot 19 \cdot 83$	$2 \cdot 11 \cdot 17^2$	$2^3 \cdot 3^2 \cdot 89$	$2 \cdot 3229$	$2^2 \cdot 1627$
9	59	$3^2 \cdot 701$	$13 \cdot 17 \cdot 29$	$3 \cdot 2153$	$23 \cdot 283$
10	60	$2 \cdot 5 \cdot 631$	$2^3 \cdot 3 \cdot 5 \cdot 53$	$2 \cdot 5 \cdot 641$	$2 \cdot 5 \cdot 17 \cdot 19$	$2 \cdot 3 \cdot 5 \cdot 7 \cdot 31$
11	61	$3 \cdot 2137$	$7 \cdot 13 \cdot 71$	$17 \cdot 383$
12	62	$2^3 \cdot 3 \cdot 263$	$2 \cdot 3181$	$2^2 \cdot 7 \cdot 229$	$2 \cdot 3^2 \cdot 359$	$2^4 \cdot 11 \cdot 37$
13	63	$59 \cdot 107$	$3^2 \cdot 7 \cdot 101$	$11^2 \cdot 53$	$23 \cdot 281$	$3 \cdot 13 \cdot 167$
14	64	$2 \cdot 7 \cdot 11 \cdot 41$	$2^2 \cdot 37 \cdot 43$	$2 \cdot 3 \cdot 1069$	$2^6 \cdot 101$	$2 \cdot 3257$
15	65	$3 \cdot 5 \cdot 421$	$5 \cdot 19 \cdot 67$	$5 \cdot 1283$	$3 \cdot 5 \cdot 431$	$5 \cdot 1303$
16	66	$2^2 \cdot 1579$	$2 \cdot 3 \cdot 1061$	$2^4 \cdot 401$	$2^2 \cdot 5 \cdot 61$	$2^2 \cdot 3^2 \cdot 181$
17	67	$3^2 \cdot 23 \cdot 31$	$29 \cdot 223$	$7^3 \cdot 19$
18	68	$2 \cdot 3^5 \cdot 13$	$2^5 \cdot 199$	$2 \cdot 3209$	$2^2 \cdot 3 \cdot 7^2 \cdot 11$	$2 \cdot 3259$
19	69	$71 \cdot 89$	$3 \cdot 11 \cdot 193$	$7^2 \cdot 131$	$3 \cdot 41 \cdot 53$
20	70	$2^4 \cdot 5 \cdot 79$	$2 \cdot 5 \cdot 7^2 \cdot 13$	$2^2 \cdot 3 \cdot 5 \cdot 107$	$2 \cdot 5 \cdot 647$	$2^3 \cdot 5 \cdot 163$
21	71	$3 \cdot 7^2 \cdot 43$	$23 \cdot 277$	$3^2 \cdot 719$
22	72	$2 \cdot 29 \cdot 109$	$2^2 \cdot 3^3 \cdot 59$	$2 \cdot 13^2 \cdot 19$	$2^3 \cdot 809$	$2 \cdot 3 \cdot 1087$
23	73	$3 \cdot 2141$	$11 \cdot 593$
24	74	$2^2 \cdot 3 \cdot 17 \cdot 31$	$2 \cdot 3187$	$2^3 \cdot 11 \cdot 73$	$2 \cdot 3 \cdot 13 \cdot 83$	$2^2 \cdot 7 \cdot 233$
25	75	$5^2 \cdot 11 \cdot 23$	$3 \cdot 5^3 \cdot 17$	$5^2 \cdot 257$	$5^2 \cdot 7 \cdot 37$	$3^2 \cdot 5^2 \cdot 29$
26	76	$2 \cdot 3163$	$2^3 \cdot 797$	$2 \cdot 3^3 \cdot 7 \cdot 17$	$2^2 \cdot 1619$	$2 \cdot 13 \cdot 251$
27	77	$3^2 \cdot 19 \cdot 37$	$7 \cdot 911$	$3 \cdot 17 \cdot 127$	$61 \cdot 107$
28	78	$2^3 \cdot 7 \cdot 113$	$2 \cdot 3 \cdot 1063$	$2^2 \cdot 1607$	$2 \cdot 41 \cdot 79$	$2^7 \cdot 3 \cdot 17$
29	79	$3 \cdot 2143$	$11 \cdot 19 \cdot 31$
30	80	$2 \cdot 3 \cdot 5 \cdot 211$	$2^2 \cdot 5 \cdot 11 \cdot 29$	$2 \cdot 5 \cdot 643$	$2^4 \cdot 3^4 \cdot 5$	$2 \cdot 5 \cdot 653$
31	81	$13 \cdot 487$	$3^2 \cdot 709$	$59 \cdot 109$	$3 \cdot 7 \cdot 311$
32	82	$2^2 \cdot 1583$	$2 \cdot 3191$	$2^5 \cdot 3 \cdot 67$	$2 \cdot 7 \cdot 463$	$2^2 \cdot 23 \cdot 71$
33	83	$3 \cdot 2111$	$13 \cdot 491$	$7 \cdot 919$	$3 \cdot 2161$	$47 \cdot 139$
34	84	$2 \cdot 3167$	$2^4 \cdot 3 \cdot 7 \cdot 19$	$2 \cdot 3217$	$2^2 \cdot 1621$	$2 \cdot 3^3 \cdot 11^2$
35	85	$5 \cdot 7 \cdot 181$	$5 \cdot 1277$	$3^2 \cdot 5 \cdot 11 \cdot 13$	$5 \cdot 1297$	$5 \cdot 1307$
36	86	$2^6 \cdot 3^2 \cdot 11$	$2 \cdot 31 \cdot 103$	$2^2 \cdot 1609$	$2 \cdot 3 \cdot 23 \cdot 47$	$2^3 \cdot 19 \cdot 43$
37	87	$3 \cdot 2129$	$41 \cdot 157$	$13 \cdot 499$	$3 \cdot 2179$
38	88	$2 \cdot 3169$	$2^2 \cdot 1597$	$2 \cdot 3 \cdot 29 \cdot 37$	$2^3 \cdot 811$	$2 \cdot 7 \cdot 467$
39	89	$3 \cdot 2113$	$47 \cdot 137$	$3^2 \cdot 7 \cdot 103$	$13 \cdot 503$
40	90	$2^2 \cdot 5 \cdot 317$	$2 \cdot 3^2 \cdot 5 \cdot 71$	$2^3 \cdot 5 \cdot 7 \cdot 23$	$2 \cdot 5 \cdot 11 \cdot 59$	$2^2 \cdot 3 \cdot 5 \cdot 109$
41	91	$17 \cdot 373$	$7 \cdot 11 \cdot 83$	$3 \cdot 19 \cdot 113$	$31 \cdot 211$
42	92	$2^3 \cdot 7 \cdot 151$	$2^3 \cdot 17 \cdot 47$	$2 \cdot 3221$	$2^2 \cdot 3 \cdot 541$	$2 \cdot 3271$
43	93	$3 \cdot 2131$	$17 \cdot 379$	$43 \cdot 151$	$3^2 \cdot 727$
44	94	$2^3 \cdot 13 \cdot 61$	$2 \cdot 23 \cdot 139$	$2^2 \cdot 3^2 \cdot 179$	$2 \cdot 17 \cdot 191$	$2^4 \cdot 409$
45	95	$3^3 \cdot 5 \cdot 47$	$5 \cdot 1279$	$5 \cdot 1289$	$3 \cdot 5 \cdot 433$	$5 \cdot 7 \cdot 11 \cdot 17$
46	96	$2 \cdot 19 \cdot 167$	$2^2 \cdot 3 \cdot 13 \cdot 41$	$2 \cdot 11 \cdot 293$	$2^3 \cdot 7 \cdot 29$	$2 \cdot 3 \cdot 1091$
47	97	$11 \cdot 577$	$3 \cdot 7 \cdot 307$	$73 \cdot 89$
48	98	$2^2 \cdot 3 \cdot 23^2$	$2 \cdot 7 \cdot 457$	$2^4 \cdot 13 \cdot 31$	$2 \cdot 3^2 \cdot 19^2$	$2^2 \cdot 1637$
49	99	$7 \cdot 907$	$3^4 \cdot 79$	$67 \cdot 97$	$3 \cdot 37 \cdot 59$
50	100	$2 \cdot 5^2 \cdot 127$	$2^8 \cdot 5^2$	$2 \cdot 3 \cdot 5^2 \cdot 43$	$2^2 \cdot 5^3 \cdot 13$	$2 \cdot 5^2 \cdot 131$

Prime Numbers and Factors, 6600-6900.

From To		6600 6650	6650 6700	6700 6750	6750 6800	6800 6850	6850 6900
0	50	2 ³ .3 ⁵ .2 ¹¹	2 ⁵ .2 ⁷ .19	2 ² .5 ² .67	2 ³ .3 ⁵ .5 ³	2 ⁴ .5 ² .17	2 ⁵ .2 ¹³ 7
1	51	7 ² .23.41	3 ² .739	43 ² .157	3 ² .2267	13 ² .17.31
2	52	2 ² .3301	2 ² .1663	2 ³ .1117	2 ⁵ .211	2 ¹⁹ .179	2 ² .3 ⁵ 71
3	53	3 ³ .31 ⁷	3 ² .251	7 ¹¹ .89
4	54	2 ² .13.127	2 ³ .1109	2 ⁴ .419	2 ¹¹ .307	2 ² .3 ⁵ .7	2 ²³ .149
5	55	5 ⁵ .131	5 ¹¹ 3	3 ² .5 ¹⁴ 9	5 ⁷ .193	5 ¹³ 61	3 ⁵ .457
6	56	2 ³ .3 ⁶ 7	2 ⁹ .13	2 ⁷ .479	2 ² .3 ⁵ 63	2 ⁴¹ .83	2 ³ .857
7	57	3 ⁷ .317	19.353	29.233	3 ² .269
8	58	2 ⁴ .7.59	2 ³ .329	2 ² .3 ¹³ .43	2 ³¹ .109	2 ³ .23.37	2 ³ .127
9	59	3 ² .203	3 ² .751	11.619	19 ³
10	60	2 ⁵ .661	2 ² .3 ² .5.37	2 ⁵ .11.61	2 ³ .5 ¹³ 2	2 ³ .5.227	2 ² .5 ⁷ 3
11	61	11.601	3 ² .2237	7 ² .139	3 ² .2287
12	62	2 ² .3 ¹⁹ .29	2 ³ .331	2 ³ .839	2 ³ .7 ² .23	2 ² .13 ¹³ 1	2 ⁴⁷ .73
13	63	17.389	3 ² .221	7 ² .137	3 ² .757
14	64	2 ³ .307	2 ³ .7 ² .17	2 ³ .2 ³ .373	2 ² .19.89	2 ³ .407	2 ⁴ .3 ¹¹ .13
15	65	3 ³ .5 ⁷ 2	5 ³ .1 ⁴³	5 ¹⁷ .79	3 ⁵ .11.41	5 ²⁹ .47	5 ¹³ 73
16	66	2 ³ .827	2 ³ .11.101	2 ² .23 ⁷ 3	2 ¹⁷ .199	2 ⁵ .3 ⁷ 1	2 ³ .433
17	67	13.509	59.113	3 ² .239	67.101	17.401	3 ² .7.109
18	68	2 ³ .1103	2 ² .1667	2 ³ .359	2 ⁴ .3 ² .47	2 ⁷ .487	2 ² .17.101
19	69	3 ³ .13.19	7 ⁹ 67	3 ² .273
20	70	2 ² .5 ³³ 1	2 ⁵ .23.29	2 ⁶ .3 ⁵ .7	2 ⁵ .677	2 ² .5 ¹¹ .31	2 ³ .5 ²² 9
21	71	3 ² .207	7.953	11.13.47	3 ³ .7 ⁶ 1	19.359
22	72	2 ⁷ .11.43	2 ⁴ .3 ¹³ 9	2 ³ .361	2 ² .1693	2 ³ .2 ³ .379	2 ³ .859
23	73	37.179	3 ⁴ .83	13.521	3 ²⁹ .79
24	74	2 ⁵ .3 ² .23	2 ⁴⁷ .71	2 ² .41 ²	2 ³ .1129	2 ³ .853	2 ⁷ .491
25	75	5 ⁵ .53	3 ⁵ .2 ⁸⁹	5 ² .269	5 ² .271	3 ⁵ .2 ⁷ .13	5 ⁴ .11
26	76	2 ³ .313	2 ² .1669	2 ³ .19.59	2 ³ .7 ¹¹ 2	2 ³ .413	2 ² .3 ² .191
27	77	3 ⁴ .7 ²	11.607	7 ³ .1 ²	3 ³ .251	13 ² .23 ²
28	78	2 ² .1657	2 ³ .2 ⁷ .53	2 ³ .29 ²	2 ³ .389	2 ² .3 ⁵ 69	2 ¹⁹ .181
29	79	7.947	3 ² .243	3 ² .293
30	80	2 ³ .5 ¹³ .17	2 ³ .5 ¹⁶ 7	2 ⁵ .673	2 ² .3 ⁵ .113	2 ⁵ .683	2 ⁵ .5 ⁴³
31	81	19.349	3 ¹⁷ .131	53.127	3 ³ .11.23	7 ⁹ 83
32	82	2 ³ .829	2 ¹³ .257	2 ² .3 ² .11.17	2 ³ .391	2 ⁴ .7.61	2 ³ .31.37
33	83	3 ² .11.67	41.163	3 ⁷ .17.19
34	84	2 ³ .1107	2 ² .3 ⁵ 57	2 ⁷ .13.37	2 ⁷ .53	2 ³ .17.67	2 ² .1721
35	85	5 ¹³ 27	5 ⁷ .191	3 ⁵ .449	5 ²³ .59	5 ¹³ 67	3 ⁴ .5.17
36	86	2 ² .3 ⁷ .79	2 ³ .343	2 ⁴ .421	2 ³ .2 ¹³ .29	2 ² .1709	2 ¹¹ .313
37	87	3 ² .743	11.617	3 ⁴ .3 ⁵ 3	71.97
38	88	2 ³ .319	2 ⁵ .11.19	2 ³ .1123	2 ² .1697	2 ¹³ .263	2 ³ .7 ⁴ 1
39	89	3 ² .213	23.293	3 ³ .173	7 ⁹ 77	83 ²
40	90	2 ⁴ .5.83	2 ³ .5 ²² 3	2 ² .5 ³³ 7	2 ⁵ .7 ⁹ 7	2 ³ .3 ² .5.19	2 ⁵ .13.53
41	91	29.229	3 ² .7.107	3 ² .297
42	92	2 ³ .4 ⁴ 1	2 ² .7.239	2 ³ .371	2 ³ .3.283	2 ¹¹ .311	2 ² .1723
43	93	7 ¹³ .73	3 ²³ .97	11.613	3 ² .281	61.113
44	94	2 ² .11.151	2 ³ .347	2 ³ .3 ² .81	2 ⁴³ .79	2 ² .29.59	2 ³ .2 ³ .83
45	95	3 ⁵ .443	5 ¹³ .103	5 ¹⁹ .71	3 ² .5 ¹⁵ 1	5 ³⁷ 2	5 ⁷ .197
46	96	2 ³ .323	2 ³ .3 ³ .31	2 ³ .373	2 ² .1699	2 ³ .7 ¹⁶ 3	2 ⁴ .431
47	97	17 ² .23	37.181	3 ¹³ .173	7 ⁹ 71	41.167	3 ¹¹ .2.19
48	98	2 ³ .3 ² 77	2 ¹⁷ .197	2 ² .7 ²⁴ 1	2 ³ .11.103	2 ⁶ .107	2 ³ .449
49	99	61.109	3 ⁷ .11.29	17.397	13 ⁵ .23	3 ² .761
50	100	2 ⁵ .2 ⁷ .19	2 ² .5 ² .67	2 ³ .5 ³	2 ⁴ .5 ² .17	2 ⁵ .2 ¹³ 7	2 ² .3 ⁵ .23

Prime Numbers and Factors, 6900-7200.

From To		6900 6950	6950 7000	7000 7050	7050 7100	7100 7150	7150 7200
0	50	2 ² ·3·5 ² ·23	2·5 ² ·139	2 ³ ·5 ³ ·7	2·3·5 ² ·47	2 ² ·5 ² ·71	2·5 ² ·11·13
1	51	67·103	3·7·331	11·641	3 ³ ·263
2	52	2·7·17·29	2 ³ ·11·79	2·3 ² ·389	2 ² ·41·43	2·53·67	2 ⁴ ·3·149
3	53	3 ² ·13·59	17·409	47·149	3·2351	23·311
4	54	2 ³ ·863	2·3·19·61	2 ² ·17·103	2·3527	2 ⁶ ·3·37	2·7 ² ·73
5	55	5·1381	5·13·107	3·5·467	5·17·83	5·7 ² ·29	3 ³ ·5·53
6	56	2·3·1151	2 ² ·37·47	2·31·113	2 ⁴ ·3 ² ·7 ²	2·11·17·19	2 ² ·1789
7	57	3 ² ·773	7 ² ·11·13	3·23·103	17·421
8	58	2 ² ·11·157	2·7 ² ·71	2 ⁵ ·3·73	2·3529	2 ² ·1777	2·3·1193
9	59	3·7 ² ·47	43·163	3·13·181
10	60	2·5·691	2 ⁴ ·3·5·29	2·5·701	2 ² ·5·353	2·3 ² ·5·79	2 ³ ·3·179
11	61	3·19·41	23·307	13·547	3·7·11·31
12	62	2 ³ ·3 ³	2·59 ²	2 ² ·1753	2·3·11·107	2 ³ ·7·127	2·3581
13	63	31·223	3·11·211	7·1009	3·2371	13·19·29
14	64	2·3457	2 ² ·1741	2·3·7·167	2 ³ ·883	2·3557	2 ² ·3 ² ·199
15	65	3·5·461	5·7·199	5·23·61	3 ² ·5·157	5·1423	5·1433
16	66	2 ² ·7·13·19	2·3 ⁴ ·43	2 ³ ·877	2·3533	2 ² ·3·593	2·3583
17	67	3·2339	37·191	11·647	3·2389
18	68	2·3·1153	2 ³ ·13·67	2·11 ² ·29	2 ² ·3·19·31	2·3559	2 ¹⁰ ·7
19	69	11·17·37	3·23·101	3 ² ·7·113	67·107
20	70	2 ³ ·5·173	2·5·17·41	2 ² ·3 ³ ·5·13	2·5·7·101	2 ⁴ ·5·89	2·3·5·239
21	71	3 ² ·769	7·17·59	3·2357	71·101
22	72	2·3461	2 ² ·3·7·83	2·3511	2 ⁵ ·13·17	2·3·1187	2 ² ·11·163
23	73	7·23·43	19·367	3·2341	11·643	17·419	3 ² ·797
24	74	2 ² ·3·577	2·11·317	2 ⁴ ·439	2·3 ³ ·131	2 ² ·13·137	2·17·211
25	75	5 ² ·277	3 ² ·5 ² ·31	5 ² ·281	5 ² ·283	3·5 ³ ·19	5 ² ·7·41
26	76	2·3463	2 ⁶ ·109	2·3·1171	2 ² ·29·61	2·7·509	2 ³ ·3·13·23
27	77	3·2309	3·7·337
28	78	2 ⁴ ·433	2·3·1163	2 ² ·7·251	2·3539	2 ³ ·3 ⁴ ·11	2·37·97
29	79	13 ² ·41	7·997	3 ² ·11·71	3·2393
30	80	2·3 ² ·5·7·11	2 ² ·5·349	2·5·19·37	2 ³ ·3·5·59	2·5·23·31	2 ² ·5·359
31	81	29·239	3·13·179	79·89	73·97	3·2377	43·167
32	82	2 ² ·1733	2·3491	2 ³ ·3·293	2·3541	2 ² ·1783	2·3 ³ ·7·19
33	83	3·2311	13·541	3 ² ·787	7·1019	11·653
34	84	2·3467	2 ³ ·3 ² ·97	2·3517	2 ² ·7·11·23	2·3·29·41	2 ⁴ ·449
35	85	5·19·73	5·11·127	3·5·7·67	5·13·109	5·1427	3·5·479
36	86	2 ³ ·3·17 ²	2·7·499	2 ² ·1759	2·3·1181	2 ⁵ ·223	2·3593
37	87	7·991	3·17·137	31·227	19·373	3 ² ·13·61
38	88	2·3469	2 ² ·1747	2·3 ² ·17·23	2 ⁴ ·443	2·43·83	2 ² ·3·599
39	89	3 ³ ·257	29·241	3·17·139	11 ² ·59	7·13·79
40	90	2 ² ·5·347	2·3·5·233	2 ⁷ ·5·11	2·5·709	2 ² ·3·5·7·17	2·5·719
41	91	11·631	3·2347	7·1013	37·193	3 ² ·17·47
42	92	2·3·13·89	2 ⁴ ·19·23	2·7·503	2 ² ·3 ² ·197	2·3571	2 ³ ·29·31
43	93	53·131	3 ³ ·7·37	41·173	3·2381
44	94	2 ⁵ ·7·31	2·13·269	2 ² ·3·587	2·3547	2 ³ ·19·47	2·3·11·109
45	95	3·5·463	5·1399	5·1409	3·5·11·43	5·1429	5·1439
46	96	2·23·151	2 ² ·3·11·53	2·13·271	2 ³ ·887	2·3 ² ·397	2 ² ·7·257
47	97	3 ⁵ ·29	47·151	7·1021	3·2399
48	98	2 ² ·3 ² ·193	3·3499	2 ³ ·881	2·3·7·13 ²	2 ² ·1787	2·59·61
49	99	3·2333	7·19·53	31·229	3·2383	23·313
50	100	2·5 ² ·139	2 ³ ·5 ³ ·7	2·3·5 ² ·47	2 ² ·5 ² ·71	2·5 ² ·11·13	2 ³ ·3 ² ·5 ²

Prime Numbers and Factors, 7200-7500.

From To	7200 7250	7250 7300	7300 7350	7350 7400	7400 7450	7450 7500
0	50	2 ⁵ ·3 ² ·5 ²	2 ⁵ ·5 ² ·29	2 ² ·5 ² ·7 ³	2 ³ ·5 ² ·7 ²	2 ³ ·5 ² ·37
1	51	19·379	3 ² ·417	7 ² ·149	3 ² ·2467
2	52	2 ² ·13 ² ·277	2 ² ·7 ² ·37	2 ³ ·1217	2 ³ ·919	2 ² ·3701
3	53	3 ⁷ ·4	67·109	3 ² ·19·43	11·673
4	54	2 ² ·1801	2 ³ ·2·13·31	2 ³ ·11·83	2 ² ·3677	2 ² ·3·617
5	55	5 ² ·11·131	5 ² ·1451	3 ⁵ ·487	5 ² ·1471	5 ² ·1481
6	56	2 ³ ·1201	2 ³ ·907	2 ² ·13·281	2 ² ·3·613	2 ⁷ ·23 ²
7	57	3 ⁴ ·159	7 ² ·1051	3 ² ·823
8	58	2 ³ ·17·53	2 ² ·19·191	2 ² ·3 ² ·7·29	2 ² ·13·283	2 ⁴ ·463
9	59	3 ⁴ ·89	7 ² ·17·61	3 ² ·11·223	31·239
10	60	2 ⁵ ·7·103	2 ² ·3 ⁵ ·11 ²	2 ⁵ ·17·43	2 ³ ·5 ² ·23	2 ³ ·3 ⁵ ·13·19
11	61	53·137	3 ² ·2437	17·433
12	62	2 ² ·3·601	2 ³ ·361	2 ⁴ ·457	2 ² ·3 ² ·409	2 ² ·17·109
13	63	3 ³ ·269	71·103	37·199	3 ⁷ ·353
14	64	2 ³ ·607	2 ³ ·277	2 ³ ·23·53	2 ² ·7·263	2 ² ·11·337
15	65	3 ⁵ ·13·37	5 ² ·1453	5 ² ·7·11·19	3 ⁵ ·491	5 ² ·1483
16	66	2 ⁴ ·11·41	2 ³ ·7·173	2 ² ·31·59	2 ² ·29·127	2 ³ ·3 ² ·103
17	67	7 ² ·1031	13 ² ·43	3 ³ ·271	53·139
18	68	2 ³ ·2·401	2 ² ·23·79	2 ³ ·659	2 ³ ·3·307	2 ² ·3709
19	69	3 ² ·2423	13 ² ·563	3 ² ·2473
20	70	2 ² ·5·19 ²	2 ⁵ ·7 ² 7	2 ³ ·3 ⁵ ·61	2 ⁵ ·11·67	2 ² ·5 ² ·7·53
21	71	3 ² ·29·83	11·661	3 ⁴ ·7·13	41·181
22	72	2 ² ·3 ² ·157	2 ³ ·3 ² ·101	2 ² ·7·523	2 ² ·19·97	2 ³ ·1237
23	73	31·233	7 ² ·1039	3 ² ·2441	73·101	13 ² ·571
24	74	2 ³ ·3 ² ·7·43	2 ² ·3637	2 ² ·1831	2 ³ ·1229	2 ⁸ ·29
25	75	5 ² ·17 ²	3 ⁵ ·2·97	5 ² ·293	5 ³ ·59	3 ³ ·5 ² ·11
26	76	2 ² ·3613	2 ² ·17·107	2 ² ·3 ² ·11·37	2 ⁴ ·461	2 ⁴ ·479
27	77	3 ² ·11·73	19·383	17·431	3 ² ·2459	7 ² ·1061
28	78	2 ² ·13·139	2 ³ ·1213	2 ⁵ ·229	2 ⁷ ·17·31	2 ² ·3·619
29	79	29·251	3 ² ·7·349	47·157	17·19·23
30	80	2 ³ ·5·241	2 ⁴ ·5·7·13	2 ⁵ ·733	2 ² ·3 ² ·5·41	2 ⁵ ·743
31	81	7 ² ·1033	3 ² ·809	11 ² ·61	3 ² ·2477
32	82	2 ⁶ ·113	2 ² ·11·331	2 ² ·3 ² ·13·47	2 ² ·3691	2 ³ ·929
33	83	3 ² ·2411	3 ² ·3 ² ·107
34	84	2 ³ ·617	2 ³ ·3·607	2 ² ·19·193	2 ³ ·13·71	2 ² ·3 ² ·7·59
35	85	5 ² ·1447	5 ² ·31·47	3 ² ·5·163	5 ² ·7·211	5 ² ·1487
36	86	2 ² ·3 ³ ·67	2 ² ·3643	2 ³ ·7·131	2 ³ ·1231	2 ² ·11·13 ²
37	87	3 ² ·7·347	11·23·29	83·89	3 ² ·7·67
38	88	2 ⁷ ·11·47	2 ³ ·911	2 ³ ·1223	2 ² ·1847	2 ² ·3719
39	89	3 ² ·19·127	37·197	41·179	3 ² ·821	43·173
40	90	2 ³ ·5·181	2 ³ ·6·5	2 ² ·5·367	2 ⁵ ·739	2 ⁴ ·3 ⁵ ·31
41	91	13·557	23·317	3 ² ·2447	19·389	7 ² ·1063
42	92	2 ³ ·17·71	2 ² ·1823	2 ² ·3671	2 ⁵ ·3 ² ·7·11	2 ² ·61 ²
43	93	3 ² ·11·13·17	7 ² ·1049	3 ² ·827
44	94	2 ² ·1811	2 ² ·7·521	2 ⁴ ·3 ³ ·17	2 ² ·3697	2 ² ·1861
45	95	3 ² ·5 ² ·7·23	5 ² ·1459	5 ² ·13·113	3 ⁵ ·17·29	5 ² ·1489
46	96	2 ² ·3623	2 ² ·3 ² ·19	2 ² ·43 ²	2 ² ·3 ² ·17·73	2 ³ ·937
47	97	3 ³ ·179	13 ² ·569	11·677
48	98	2 ⁴ ·3·151	2 ⁴ ·189	2 ² ·11·167	2 ³ ·3 ² ·137	3 ³ ·7 ² ·19
49	99	11·659	3 ² ·811	7 ² ·151	2 ³ ·13·191
50	100	2 ⁵ ·3 ² ·29	2 ⁵ ·5 ² ·73	2 ³ ·5 ² ·7 ²	2 ³ ·5 ² ·37	2 ⁵ ·2·149

Prime Numbers and Factors, 7500-7800.

From To	7500 7550	7550 7600	7600 7650	7650 7700	7700 7750	7750 7800
0	50	2 ² ·3·5 ⁴	2 ⁵ ·2 ¹⁵ 1	2 ⁴ ·5 ² ·19	2 ² ·5 ² ·7·11	2·5 ⁵ ·31
1	51	13·577	3 ² ·839	11·691	7·1093	3·17·151
2	52	2·11 ² ·31	2 ⁷ ·59	2·3·7·181	2 ² ·1913	2 ³ ·3·17·19
3	53	3·41·61	7·13·83	3·2551
4	54	2 ⁴ ·7·67	2·3·1259	2 ² ·1901	2·43·89	2 ³ ·3 ² ·107
5	55	5·19·79	5·1511	3 ² ·5·13 ²	5·1531	5·23·67
6	56	2·3 ³ ·139	2 ³ ·1889	2·3803	2 ³ ·3·11·29	2·3853
7	57	3·11·229	13·19·31	3·7·367
8	58	2 ² ·1877	2·3779	2 ³ ·3·317	2·7·547	2 ² ·41·47
9	59	3·2503	7·1087	3 ² ·23·37	13·593
10	60	2·5·751	2 ³ ·3 ³ ·5·7	2·5·761	2 ² ·5·383	2·3·5·257
11	61	7·29·37	3·43·59	47·163	11·701
12	62	2 ³ ·3·313	2·19·199	2 ² ·11·173	2·3·1277	2 ⁵ ·241
13	63	11·683	3·2521	23·331	79·97	3 ² ·857
14	64	2·13·17 ²	2 ² ·31·61	2·3 ⁴ ·47	2 ⁴ ·479	2·7·19·29
15	65	3 ² ·5·167	5·17·89	5·1523	3·5·7·73	5·1543
16	66	2 ² ·1879	2·3·13·97	2 ⁶ ·7·17	2·3833	2 ² ·3·643
17	67	7·23·47	3·2539	11·17·41
18	68	2·3·7·179	2 ⁴ ·11·43	2·13·293	2 ² ·3 ³ ·71	2·17·227
19	69	73·103	3 ² ·29 ²	19·401	3·31·83
20	70	2 ³ ·5·47	2·5·757	2 ² ·3·5·127	2·5·13·59	2 ³ ·5·193
21	71	3·23·109	67·113	3·2557	7·1103
22	72	2·3761	2 ² ·3·631	2·37·103	2 ³ ·7·137	2·3 ³ ·11·13
23	73	3 ² ·7·11 ²
24	74	2 ² ·3 ² ·11·19	2·7·541	2 ³ ·953	2·3·1279	2 ² ·1931
25	75	5 ² ·7·43	3·5 ² ·101	5 ³ ·61	5 ² ·307	3·5 ² ·103
26	76	2·53·71	2 ³ ·947	2·3·31·41	2 ² ·19·101	2·3863
27	77	3·13·193	29·263	3 ² ·853
28	78	2 ³ ·941	2·3 ² ·421	2 ² ·1907	2·11·349	2 ⁴ ·3·7·23
29	79	11·13·53	3·2543	7·1097	59·131
30	80	2·3·5·251	2 ² ·5·379	2·5·7·109	2 ⁹ ·3·5	2·5·773
31	81	17·443	3·7·19 ²	13·587	3 ² ·859
32	82	2 ² ·7·269	2·17·223	2 ⁴ ·3 ² ·53	2·23·167	2 ² ·1933
33	83	3 ⁵ ·31	17·449	3·13·197	11·19·37
34	84	2·3767	2 ³ ·3·79	2·11·347	2 ² ·17·113	2·3·1289
35	85	5·11·137	5·37·41	3·5·509	5·29·53	5·7·13·17
36	86	2 ⁴ ·3·157	2·3793	2 ² ·23·83	2·3 ² ·7·61	2 ³ ·967
37	87	3 ³ ·281	7·1091	3·2579
38	88	2·3769	2 ² ·7·271	2·3·19·67	2 ³ ·31 ²	2·53·73
39	89	3·7·359	3·11·233	71·109
40	90	2 ² ·5·13·29	2·3·5·11·23	2 ³ ·5·191	2·5·769	2 ² ·3 ² ·5·43
41	91	3 ³ ·283
42	92	2·3 ² ·419	2 ³ ·13·73	2·3821	2 ² ·3·641	2·7 ² ·53
43	93	19·397	3·2531	7 ² ·157	3·29·89
44	94	2 ³ ·23·41	2·3797	2 ² ·3·7 ² ·13	2·3847	2 ⁶ ·11 ²
45	95	3·5·503	5·7 ² ·31	5·11·139	3 ⁴ ·5·19	5·1549
46	96	2·7 ³ ·11	2 ⁴ ·3 ² ·211	2·3823	2 ⁴ ·13·37	2·3·1291
47	97	71·107	3·2549	43·179	61·127
48	98	2 ² ·3·17·37	2·29·131	2 ⁵ ·239	2·3·1283	2 ² ·13·149
49	99	3·17·149	3 ³ ·7·41
50	100	2·5 ² ·151	2 ⁴ ·5 ² ·19	2·3 ² ·5 ² ·17	2 ² ·5 ² ·7·11	2 ³ ·3·5 ² ·13

Prime Numbers and Factors, 7800-8100.

From To	7800 7850	7850 7900	7900 7950	7950 8000	8000 8050	8050 8100
0	50	2 ³ ·3·5 ² ·13	2·5 ² ·157	2 ² ·5 ² ·79	2·3·5 ² ·53	2 ⁶ ·5 ³
1	51	29·269	3·2617	3 ² ·7·127
2	52	2·47·83	2 ² ·13·151	2·3 ² ·439	2 ⁴ ·7·71	2·4001
3	53	3 ³ ·17 ²	7·1129	3·11·241	53·151
4	54	2 ² ·1951	2·3·7·11·17	2 ⁵ ·13·19	2·41·97	2 ² ·3·23·29
5	55	5·7·223	5·1571	3·5·17·31	5·37·43	5·1601
6	56	2·3·1301	2 ⁴ ·491	2·59·67	2 ² ·3 ² ·13·17	2·4003
7	57	37·211	3 ⁴ ·97	73·109	3·17·157
8	58	2 ⁷ ·61	2·3929	2 ² ·3·659	2·23·173	2 ³ ·7·11·13
9	59	3·19·137	29·271	11·719	3·7·379
10	60	2·5·11·71	2 ² ·3·5·131	2·5·7·113	2 ³ ·5·199	2·3 ² ·5·89
11	61	73·107	7·1123	3 ³ ·293	19·419
12	62	2 ² ·3 ² ·7·31	2·3931	2 ³ ·23·43	2·3·1327	2 ² ·2003
13	63	13·601	3·2621	41·193	3·2671
14	64	2·3907	2 ³ ·983	2·3·1319	2 ² ·11·181	2·4007
15	65	3·5·521	5·11 ² ·13	5·1583	3 ³ ·5·59	5·7·229
16	66	2 ³ ·977	2·3 ² ·19·23	2 ² ·1979	2·7·569	2 ⁴ ·3·167
17	67	3·7·13·29	31·257
18	68	2·3·1303	2 ² ·7·281	2·37·107	2 ⁵ ·3·83	2·19·211
19	69	7·1117	3·43·61	13·613	3 ⁶ ·11
20	70	2 ² ·5·17·23	2·5·787	2 ⁴ ·3 ² ·5·11	2·5·797	2 ² ·5·401
21	71	3 ² ·11·79	17·463	89 ²	3·2657	13·617
22	72	2·3911	2 ⁶ ·3·41	2·17·233	2 ² ·1993	2·3·7·191
23	73	3·19·139	7·17·67	71·113
24	74	2 ⁴ ·3·163	2·31·127	2 ² ·7·283	2·3 ² ·443	2 ³ ·17·59
25	75	5 ² ·313	3 ² ·5 ³ ·7	5 ² ·317	5 ² ·11·29	3·5 ² ·107
26	76	2·7·13·43	2 ² ·11·179	2·3·1321	2 ³ ·997	2·4013
27	77	3·2609	3·2659	2·3·349
28	78	2 ² ·19·103	2·3·13·101	2 ³ ·991	2·3989	2 ² ·3 ² ·223
29	79	3 ² ·881	79·101	7·31·37
30	80	2·3 ³ ·5·29	2 ³ ·5·197	2·5·13·61	2 ² ·3·5·7·19	2·5·11·73
31	81	41·191	3·37·71	7·11·103	23·347	3·2677
32	82	2 ³ ·11·89	2·7·563	2 ² ·3·661	2·13·307	2 ⁵ ·251
33	83	3·7·373	3 ² ·887	29·277
34	84	2·3917	2 ² ·3 ³ ·73	2·3967	2 ⁴ ·499	2·3·13·103
35	85	5·1567	5·19·83	3·5·23 ²	5·1597	5·1607
36	86	2 ² ·3·653	2·3943	2 ⁶ ·31	2·3·11 ³	2 ² ·7 ² ·41
37	87	17·461	3·11·239	7 ² ·163	3 ² ·19·47
38	88	2·3919	2 ⁴ ·17·29	2·3 ⁴ ·7 ²	2 ² ·1997	2·4019
39	89	3 ² ·13·67	7 ³ ·23	17·467	3·2663
40	90	2 ⁵ ·5·7 ²	2·3·5·263	2 ² ·5·397	2·5·17·47	2 ³ ·3·5·67
41	91	13·607	3·2647	61·131	11·17·43
42	92	2·3·1307	2 ² ·1973	2·11·19 ²	2 ³ ·3 ³ ·37	2·4021
43	93	11·23·31	3 ² ·877	13 ² ·47	3·7·383
44	94	2 ² ·37·53	2·3947	2 ³ ·3·331	2·7·571	2 ² ·2011
45	95	3·5·523	5·1579	5·7·227	3·5·13·41	5·1609
46	96	2·3923	2 ³ ·3·7·47	2·29·137	2 ² ·1999	2·3 ³ ·149
47	97	7·19·59	53·149	3 ² ·883	11·727	13·619
48	98	2 ³ ·3 ² ·109	2·11·359	2 ² ·1987	2·3·31·43	2 ⁴ ·503
49	99	47·167	3·2633	19·421	3·2683
50	100	2·5 ² ·157	2 ² ·5 ² ·79	2·3·5 ² ·53	2 ⁶ ·5 ³	2·5 ² ·7·23

Prime Numbers and Factors, 8100-8400.

From To	8100 8150	8150 8200	8200 8250	8250 8300	8300 8350	8350 8400
0 50	2 ² ·3 ⁴ ·5 ²	2 ⁵ ·2 ¹⁶³	2 ³ ·5 ² ·41	2 ³ ·5 ² ·11	2 ² ·5 ² ·83	2 ⁵ ·2 ¹⁶⁷
1 51	3 ¹¹ ·13 ¹⁹	59·139	37·223	3·2767	7 ¹¹⁹³
2 52	2·4051	2 ³ ·1019	2 ³ ·1367	2 ² ·2063	2 ⁷ ·593	2 ⁵ ·3 ² ·29
3 53	3 ³⁷ ·73	31·263	13·631	3 ² ·7·131	19 ² ·23
4 54	2 ³ ·1013	2 ³ ·3 ¹⁵¹	2 ² ·7·293	2·4127	2 ⁴ ·3·173	2·4177
5 55	5·1621	5 ⁷ ·233	3 ⁵ ·547	5·13·127	5·11·151	3 ⁵ ·557
6 56	2 ³ ·7·193	2 ² ·2039	2 ¹¹ ·373	2 ⁶ ·3·43	2 ⁴ ·153	2 ² ·2089
7 57	11 ² ·67	3 ² ·719	29·283	23·359	3 ² ·13 ⁷¹	61·137
8 58	2 ² ·2027	2 ⁴ ·79	2 ⁴ ·3 ³ ·19	2·4129	2 ² ·31·67	2 ³ ·7·199
9 59	3 ² ·17·53	41·199	3 ² ·753	7·1187	13 ⁶⁴³
10 60	2 ⁵ ·811	2 ⁵ ·3 ⁵ ·17	2 ⁵ ·821	2 ² ·5 ⁷ ·59	2 ³ ·5 ² ·277	2 ³ ·5 ¹¹ ·19
11 61	3 ⁷ ·17·23	11·751	3 ² ·929
12 62	2 ⁴ ·3·13 ²	2 ⁷ ·11·53	2 ² ·2053	2 ³ ·3 ¹⁷	2 ³ ·1039	2 ³ ·7·113
13 63	7·19·61	3 ² ·907	43·191	3 ¹⁷ ·163
14 64	2·4057	2 ² ·13·157	2 ³ ·37 ²	2 ³ ·1033	2 ⁴ ·157	2 ² ·3 ¹⁷ ·41
15 65	3 ⁵ ·541	5 ²³ ·71	5·31·53	3 ⁵ ·19·29	5·1663	5 ⁷ ·239
16 66	2 ² ·2029	2 ³ ·1361	2 ³ ·13·79	2 ⁴ ·133	2 ² ·3 ³ ·7·11	2 ⁴ ·7·89
17 67	3 ² ·11·83	7·1181	3 ² ·789
18 68	2 ³ ·2 ¹¹ ·41	2 ³ ·1021	2 ⁷ ·587	2 ² ·3·13·53	2 ⁴ ·159	2 ⁴ ·523
19 69	23·353	3 ⁷ ·389	3 ⁴ ·7·59
20 70	2 ³ ·5 ⁷ ·29	2 ⁵ ·19·43	2 ² ·3 ⁵ ·137	2 ⁵ ·827	2 ⁷ ·5·13	2 ³ ·3 ⁵ ·31
21 71	3 ² ·707	3 ² ·919	53·157	11·761
22 72	2 ³ ·1·131	2 ² ·3 ³ ·227	2·4111	2 ⁴ ·11·47	2 ³ ·19·73	2 ² ·7·13·23
23 73	11·743	3 ² ·741	7 ²⁹ ·41	3 ² ·791
24 74	2 ² ·3·677	2 ⁶ ·1·67	2 ⁵ ·257	2 ³ ·7·197	2 ² ·2081	2 ⁵³ ·79
25 75	5 ⁴ ·13	3 ⁵ ·2 ¹⁰⁹	5 ² ·7·47	5 ² ·331	3 ² ·5 ² ·37	5 ³ ·67
26 76	2 ¹⁷ ·239	2 ⁴ ·7·73	2 ³ ·2 ⁴⁵⁷	2 ² ·2069	2 ²³ ·181	2 ³ ·3 ³ ·49
27 77	3 ³ ·7·43	13·17·37	19·433	3 ³ ·189	11·757
28 78	2 ⁶ ·127	2 ³ ·29·47	2 ² ·11 ² ·17	2 ⁴ ·139	2 ³ ·3 ³ ·47	2 ⁵⁹ ·71
29 79	11·739	3 ¹³ ·211	17·487	3 ² ·7 ² ·19
30 80	2 ³ ·5 ² ·271	2 ² ·5·409	2 ⁵ ·823	2 ³ ·3 ² ·5·23	2 ⁵ ·7 ² ·17	2 ² ·5 ⁴ ·19
31 81	47·173	3 ⁴ ·101	7 ² ·13 ²	3 ² ·777	17 ² ·29
32 82	2 ² ·19·107	2 ⁴ ·91	2 ³ ·3 ⁷ ·3	2 ⁴ ·101	2 ² ·2083	2 ³ ·11·127
33 83	3 ² ·711	7 ² ·167	3 ¹¹ ·251	13 ⁶⁴¹	83·101
34 84	2 ⁷ ·2 ⁸³	2 ³ ·3 ¹¹ ·31	2 ²³ ·179	2 ² ·19·109	2 ³ ·2 ⁴⁶³	2 ⁶ ·131
35 85	5 ¹⁶²⁷	5 ¹⁶³⁷	3 ³ ·5·61	5 ² ·331	5 ¹⁶⁶⁷	3 ⁵ ·13·43
36 86	2 ³ ·3 ² ·113	2 ⁴ ·93	2 ² ·29·71	2 ³ ·1381	2 ⁴ ·521	2 ⁷ ·599
37 87	79·103	3 ² ·729	3 ⁷ ·397
38 88	2 ¹³ ·313	2 ² ·23·89	2 ³ ·1373	2 ⁵ ·7·37	2 ¹¹ ·379	2 ² ·3 ² ·233
39 89	3 ² ·713	19·431	7 ¹¹ ·107	3 ³ ·307	31·269
40 90	2 ² ·5 ¹¹ ·37	2 ³ ·2 ⁵ ·7·13	2 ⁴ ·5·103	2 ⁵ ·829	2 ² ·3 ⁵ ·139	2 ⁵ ·839
41 91	7·1163	3 ⁴ ·167	19·439	3 ² ·797
42 92	2 ³ ·23·59	2 ¹³	2 ¹³ ·317	2 ² ·3·691	2 ⁴³ ·97	2 ³ ·1049
43 93	17·479	3 ² ·731	3 ⁴ ·103	7 ¹¹ ·109
44 94	2 ⁴ ·509	2 ¹⁷ ·241	2 ² ·3 ² ·229	2 ¹¹ ·13·29	2 ³ ·7·149	2 ³ ·1399
45 95	3 ² ·5 ¹⁸¹	5 ¹¹ ·149	5 ¹⁷ ·97	3 ⁵ ·7·79	5 ¹⁶⁶⁹	5 ²³ ·73
46 96	2 ⁴ ·73	2 ² ·3 ⁶⁸³	2 ⁷ ·19·31	2 ³ ·17·61	2 ³ ·13·107	2 ² ·2099
47 97	7·1171	3 ² ·749	17·491	3 ³ ·311
48 98	2 ² ·3 ⁷ ·97	2 ⁴ ·99	2 ³ ·1031	2 ³ ·2 ⁴⁶¹	2 ² ·2087	2 ¹³ ·17·19
49 99	29·281	3 ² ·911	73·113	43·193	3 ¹¹ ·2 ²³	37 ²²⁷
50 100	2 ⁵ ·2 ¹⁶³	2 ³ ·5 ² ·41	2 ³ ·5 ³ ·11	2 ² ·5 ² ·83	2 ⁵ ·2 ¹⁶⁷	2 ⁴ ·3 ⁵ ·7

Prime Numbers and Factors, 8400-8700.

From To	8400 8450	8450 8500	8500 8550	8550 8600	8600 8650	8650 8700
0	50	$2^4 \cdot 3 \cdot 5^2 \cdot 7$	$2 \cdot 5^2 \cdot 13^2$	$2^2 \cdot 5^3 \cdot 17$	$2 \cdot 3^2 \cdot 5^2 \cdot 19$	$2^3 \cdot 5^2 \cdot 43$
1	51	$3^1 \cdot 271$	$3^3 \cdot 313$	17·503	$3 \cdot 47 \cdot 61$
2	52	$2 \cdot 4201$	$2^2 \cdot 2113$	$2 \cdot 3 \cdot 13 \cdot 109$	$2^3 \cdot 1069$	$2 \cdot 11 \cdot 17 \cdot 23$
3	53	$3 \cdot 2801$	79·107	11·773	3·2851	7·1229
4	54	$2^2 \cdot 11 \cdot 191$	$2 \cdot 3 \cdot 1409$	$2^3 \cdot 1063$	$2 \cdot 7 \cdot 13 \cdot 47$	$2^2 \cdot 3^2 \cdot 239$
5	55	$5 \cdot 41^2$	$5 \cdot 19 \cdot 89$	$3^5 \cdot 5 \cdot 7$	5·29·59	5·1721
6	56	$2 \cdot 3^2 \cdot 467$	$2^3 \cdot 7 \cdot 151$	2·4253	$2^2 \cdot 3 \cdot 23 \cdot 31$	$2 \cdot 13 \cdot 331$
7	57	$7 \cdot 1201$	3·2819	47·181	43·199	$3 \cdot 19 \cdot 151$
8	58	$2^3 \cdot 1051$	2·4229	$2^2 \cdot 3 \cdot 709$	$2 \cdot 11 \cdot 389$	$2^3 \cdot 269$
9	59	$3 \cdot 2803$	11·769	67·127	$3^3 \cdot 317$
10	60	$2 \cdot 5 \cdot 29^2$	$2^2 \cdot 3^2 \cdot 5 \cdot 47$	$2 \cdot 5 \cdot 23 \cdot 37$	$2^4 \cdot 5 \cdot 107$	$2 \cdot 3 \cdot 5 \cdot 7 \cdot 41$
11	61	$13 \cdot 647$	3·2837	7·1223	79·109
12	62	$2^2 \cdot 3 \cdot 701$	2·4231	$2^6 \cdot 7 \cdot 19$	$2 \cdot 3 \cdot 1427$	$2^2 \cdot 2153$
13	63	$47 \cdot 179$	$3 \cdot 7 \cdot 13 \cdot 31$	$3^3 \cdot 11 \cdot 29$
14	64	$2 \cdot 7 \cdot 601$	$2^4 \cdot 23^2$	$2 \cdot 3^2 \cdot 11 \cdot 43$	$2^2 \cdot 2141$	$2 \cdot 59 \cdot 73$
15	65	$3^2 \cdot 5 \cdot 11 \cdot 17$	5·1693	$5 \cdot 13 \cdot 131$	$3 \cdot 5 \cdot 571$	5·1723
16	66	$2^5 \cdot 263$	$2 \cdot 3 \cdot 17 \cdot 83$	$2^2 \cdot 2129$	2·4283	$2^3 \cdot 3 \cdot 359$
17	67	19·443	3·17·167	13·659	7·1231
18	68	$2 \cdot 3 \cdot 23 \cdot 61$	$2^2 \cdot 29 \cdot 73$	2·4259	$2^3 \cdot 3^2 \cdot 7 \cdot 17$	$2 \cdot 31 \cdot 139$
19	69	$3^2 \cdot 941$	7·1217	$11 \cdot 19 \cdot 41$	$3 \cdot 13^2 \cdot 17$
20	70	$2^2 \cdot 5 \cdot 421$	$2 \cdot 5 \cdot 7 \cdot 11^2$	$2^3 \cdot 3 \cdot 5 \cdot 71$	$2 \cdot 5 \cdot 857$	$2^2 \cdot 5 \cdot 431$
21	71	$3 \cdot 7 \cdot 401$	43·197	3·2857	37·233
22	72	$2 \cdot 4211$	$2^3 \cdot 3 \cdot 353$	2·4261	$2^2 \cdot 2143$	$2 \cdot 3^2 \cdot 479$
23	73	37·229	$3^2 \cdot 947$
24	74	$2^3 \cdot 3^4 \cdot 13$	$2 \cdot 19 \cdot 223$	$2^2 \cdot 2131$	$2 \cdot 3 \cdot 1429$	$2^4 \cdot 7^2 \cdot 11$
25	75	$5^2 \cdot 337$	$3 \cdot 5^2 \cdot 113$	$5^2 \cdot 11 \cdot 31$	$5^2 \cdot 7^3$	$3 \cdot 5^3 \cdot 23$
26	76	$2 \cdot 11 \cdot 383$	$2^2 \cdot 13 \cdot 163$	$2 \cdot 3 \cdot 7^2 \cdot 29$	21·67	$2 \cdot 19 \cdot 227$
27	77	$3 \cdot 53^2$	7 ² ·173	$3^2 \cdot 953$
28	78	$2^2 \cdot 7^2 \cdot 43$	$2 \cdot 3^3 \cdot 157$	$2^4 \cdot 13 \cdot 41$	2·4289	$2^2 \cdot 3 \cdot 719$
29	79	61·139	3·2843	23·373
30	80	$2 \cdot 3 \cdot 5 \cdot 281$	$2^5 \cdot 5 \cdot 53$	$2 \cdot 5 \cdot 853$	$2^2 \cdot 3 \cdot 5 \cdot 11 \cdot 13$	$2 \cdot 5 \cdot 863$
31	81	$3 \cdot 11 \cdot 257$	19·449	$3^2 \cdot 7 \cdot 137$
32	82	$2^4 \cdot 17 \cdot 31$	2·4241	$2^2 \cdot 3^3 \cdot 79$	$2 \cdot 7 \cdot 613$	$2^3 \cdot 13 \cdot 83$
33	83	$3^2 \cdot 937$	17·499	7·23·53	3·2861	89·97
34	84	$2 \cdot 4217$	$2^2 \cdot 3 \cdot 7 \cdot 101$	$2 \cdot 17 \cdot 251$	$2^3 \cdot 29 \cdot 37$	$2 \cdot 3 \cdot 1439$
35	85	$5 \cdot 7 \cdot 241$	5·1697	$3 \cdot 5 \cdot 569$	$5 \cdot 17 \cdot 101$	$5 \cdot 11 \cdot 157$
36	86	$2^2 \cdot 3 \cdot 19 \cdot 37$	2·4243	$2^3 \cdot 11 \cdot 97$	$2 \cdot 3^4 \cdot 53$	$2^2 \cdot 17 \cdot 127$
37	87	$11 \cdot 13 \cdot 59$	$3^2 \cdot 23 \cdot 41$	31·277	3·2879
38	88	$2 \cdot 4219$	$2^3 \cdot 1061$	$2 \cdot 3 \cdot 1423$	$2^2 \cdot 19 \cdot 113$	$2 \cdot 7 \cdot 617$
39	89	$3 \cdot 29 \cdot 97$	13·653	3·7·409	53·163
40	90	$2^3 \cdot 5 \cdot 211$	$2 \cdot 3 \cdot 5 \cdot 283$	$2^2 \cdot 5 \cdot 7 \cdot 61$	$2 \cdot 5 \cdot 859$	$2^6 \cdot 3^3 \cdot 5$
41	91	$23 \cdot 367$	7·1213	$3^2 \cdot 13 \cdot 73$	$11^2 \cdot 71$
42	92	$2 \cdot 3^2 \cdot 7 \cdot 67$	$2 \cdot 11 \cdot 193$	2·4271	$2^4 \cdot 3 \cdot 179$	$2 \cdot 29 \cdot 149$
43	93	$3 \cdot 19 \cdot 149$	13·661	3·43·67
44	94	$2^2 \cdot 2111$	$2 \cdot 31 \cdot 137$	$2^5 \cdot 3 \cdot 89$	2·4297	$2^2 \cdot 2161$
45	95	$3 \cdot 5 \cdot 563$	5·1699	5·1709	$3^2 \cdot 5 \cdot 191$	$5 \cdot 7 \cdot 13 \cdot 19$
46	96	$2 \cdot 41 \cdot 103$	$2^4 \cdot 3^2 \cdot 59$	2·4273	$2^2 \cdot 7 \cdot 307$	$2 \cdot 3 \cdot 11 \cdot 131$
47	97	29·293	$3 \cdot 7 \cdot 11 \cdot 37$
48	98	$2^3 \cdot 3 \cdot 11$	$2 \cdot 7 \cdot 607$	$2^2 \cdot 2137$	$2 \cdot 3 \cdot 1433$	$2^3 \cdot 23 \cdot 47$
49	99	$7 \cdot 17 \cdot 71$	3·2833	83·103	$3^2 \cdot 31^2$
50	100	$2 \cdot 5^2 \cdot 13^2$	$2^2 \cdot 5^3 \cdot 17$	$2 \cdot 3^2 \cdot 5^2 \cdot 19$	$2^3 \cdot 5^2 \cdot 43$	$2 \cdot 5^2 \cdot 173$

Prime Numbers and Factors, 8700-9000.

From To		8700 8750	8750 8800	8800 8850	8850 8900	8900 8950	8950 9000
0	50	2 ² ·3·5 ² ·29	2·5 ⁴ ·7	2 ⁵ ·5 ² ·11	2·3·5 ² ·59	2 ² ·5 ² ·89	2·5 ² ·179
1	51	7·11·113	3·2917	13·677	53·167	3 ³ ·23·43
2	52	2·19·229	2 ⁴ ·547	2·3 ³ ·163	2 ² ·2213	2·4451	2 ³ ·3·373
3	53	3 ² ·967	3·13·227	29·307	7·1279
4	54	2 ⁹ ·17	2·3·1459	2 ² ·31·71	2·19·233	2 ³ ·3·7·53	2·11 ² ·37
5	55	5·1·41	5·17·103	3·5·587	5·7·11·23	5·13·137	3 ² ·5·199
6	56	2·3·1451	2 ² ·11·199	2·7·17·37	2 ³ ·3 ³ ·41	2·61·73	2 ² ·2239
7	57	3 ² ·7·139	17·521	3·2969	13 ² ·53
8	58	2 ² ·7·311	2·29·151	2 ³ ·3·367	2·43·103	2 ² ·17·131	2·3·1493
9	59	3·2903	19·461	23·383	3·2953	59·151	17 ² ·31
10	60	2·5·13·67	2 ³ ·3·5·73	2·5·881	2 ² ·5·443	2·3 ⁴ ·5·11	2 ⁸ ·5·7
11	61	31·281	3 ² ·11·89	7·19·67	3·29·103
12	62	2 ³ ·3 ² ·11 ²	2·13·337	2 ² ·2203	2·3·7·211	2 ⁴ ·557	2·4481
13	63	3·23·127	7·1259	3·2971
14	64	2·4357	2 ² ·7·313	2·3·13·113	2 ⁵ ·277	2·4457	2 ² ·3 ³ ·83
15	65	3·5·7·83	5·1753	5·43·41	3 ² ·5·197	5·1783	5·11·163
16	66	2 ² ·2179	2·3 ² ·487	2 ⁴ ·19·29	2·11·13·31	2 ² ·3·743	2·4483
17	67	23·379	11·797	3·2939	37·241	3·7 ² ·61
18	68	2·3·1453	2 ⁶ ·137	2·4409	2 ² ·3·739	2·7 ³ ·13	2 ³ ·19·59
19	69	3·37·79	7 ² ·181	3 ² ·991
20	70	2 ⁴ ·5·109	2·5·877	2 ² ·3 ² ·5·7 ²	2·5·887	2 ³ ·5·223	2·3·5·13·23
21	71	3 ³ ·17·19	7 ² ·179	3·2957	11·811
22	72	2·7 ² ·89	2 ² ·3·17·43	2·11·401	2 ³ ·1109	2·3·1487	2 ² ·2243
23	73	11·13·61	31·283	3·17·173	19·467	3 ² ·997
24	74	2 ² ·3·727	2·41·107	2 ³ ·1103	2·3 ² ·17·29	2 ² ·23·97	2·7·641
25	75	5 ² ·349	3 ³ ·5 ² ·13	5 ² ·353	5 ³ ·71	3·5 ² ·7·17	5 ² ·359
26	76	2·4363	2 ³ ·1097	2·3·1471	2 ² ·7·317	2·4463	2 ⁴ ·3·11·17
27	77	3·2909	67·131	7·13·97	3·11·269	79·113	47·191
28	78	2 ³ ·1091	2·3·7·11·19	2 ² ·2207	2·23·193	2 ⁵ ·3 ² ·31	2·67 ²
29	79	7·29·43	3 ⁴ ·109	13·683	3·41·73
30	80	2·3 ² ·5·97	2 ² ·5·439	2·5·883	2 ⁴ ·3·5·37	2·5·19·47	2 ² ·5·449
31	81	3·2927	83·107	3·13·229	7·1283
32	82	2 ² ·37·59	2·4391	2 ⁷ ·3·23	2·4441	2 ² ·7·11·29	2·3 ² ·499
33	83	3·41·71	11 ² ·73	3 ³ ·7·47	13·691
34	84	2·11·397	2 ⁴ ·3 ² ·61	2·7·631	2 ² ·2221	2·3·1489	2 ³ ·1123
35	85	5·1747	5·7·251	3·5·19·31	5·1777	5·1787	3·5·599
36	86	2 ⁵ ·3·7·13	2·23·191	2 ² ·47 ²	2·3·1481	2 ³ ·1117	2·4493
37	87	3·29·101	3 ³ ·331	11·19·43
38	88	2·17·257	2 ² ·13 ³	2·3 ² ·491	2 ³ ·11·101	2·41·109	2 ² ·3·7·107
39	89	3 ² ·971	11·17·47	3·2963	7·1277	89·101
40	90	2 ² ·5·19·23	2·3·5·293	2 ³ ·5·13·17	2·5·7·127	2 ² ·3·5·149	2·5·29·31
41	91	59·149	3·7·421	17·523	3 ⁵ ·37
42	92	2·3·31·47	2 ³ ·7·151	2·4421	2 ² ·3 ² ·13·19	2·17·263	2 ⁵ ·281
43	93	7·1249	3 ² ·977	37·239	3·11·271	17·23 ²
44	94	2 ³ ·1093	2·4397	2 ³ ·3·11·67	2·4447	2 ⁴ ·13·43	2·3·1499
45	95	3·5·11·53	5·1759	5·29·61	3·5·593	5·1789	5·7·257
46	96	2·4373	2 ² ·3·733	2·4423	2 ⁶ ·139	2·3 ² ·7·71	2 ² ·13·173
47	97	19·463	3 ² ·983	7·31·41	23·389	3·2999
48	98	2 ² ·3 ⁷	2·53·83	2 ⁴ ·7·79	2·3·1483	2 ² ·2237	2·11·409
49	99	13·673	3·7·419	11·809	3·19·157
50	100	2·5 ⁴ ·7	2 ⁵ ·5 ² ·11	2·3·5 ² ·59	2 ² ·5 ² ·89	2·5 ² ·179	2 ³ ·3 ² ·5 ³

Prime Numbers and Factors, 9000-9300.

From To		9000 9050	9050 9100	9100 9150	9150 9200	9200 9250	9250 9300
0	50	2 ³ ·3 ² ·5 ³	2·5 ² ·181	2 ² ·5 ² ·7·13	2·3·5 ² ·61	2 ⁴ ·5 ² ·23	2·5 ³ ·37
1	51	3·7·431	19·479	3·3067	11·29 ²
2	52	2·7·643	2 ² ·31·73	2·3·37·41	2 ⁶ ·11·13	2·43·107	2 ² ·3 ² ·257
3	53	3·3001	11·823	3 ⁴ ·113	19·487
4	54	2 ² ·2251	2·3 ² ·503	2 ⁴ ·569	2·23·199	2 ² ·3·13·59	2·7·661
5	55	5·1801	5·1811	3·5·607	5·1831	5·7·263	3·5·617
6	56	2·3·19·79	2 ⁵ ·283	2·29·157	2 ² ·3·7·109	2·4603	2 ³ ·13·89
7	57	3·3019	7·1301	3 ³ ·11·31
8	58	2 ⁴ ·563	2·7·647	2 ² ·3 ² ·11·23	2·19·241	2 ³ ·1151	2·3·1543
9	59	3 ² ·7·11·13	3·43·71	47·197
10	60	2·5·17·53	2 ² ·3·5·151	2·5·911	2 ³ ·5·229	2·3·5·307	2 ² ·5·463
11	61	13·17·41	3·3037	61·151	3 ³ ·7 ³
12	62	2 ³ ·3·751	2·23·197	2 ³ ·17·67	2·3 ² ·509	2 ² ·7 ² ·47	2·11·421
13	63	3 ² ·19·53	13·701	7 ² ·11·17	3·37·83	59·157
14	64	2·4507	2 ³ ·11·103	2·3·7 ² ·31	2 ² ·29·79	2·17·271	2 ³ ·3·193
15	65	3·5·601	5·7 ² ·37	5·1823	3·5·13·47	5·19·97	5·17·109
16	66	2 ³ ·7 ² ·23	2·3·1511	2 ² ·43·53	2·4583	2 ¹⁰ ·3 ²	2·41·113
17	67	71·127	3 ² ·1013	89·103	13·709	3·3089
18	68	2·3 ³ ·167	2 ² ·2267	2·47·97	2 ⁴ ·3·191	2·11·419	2 ² ·7·331
19	69	29·311	3·3023	11·829	53·173	3·7·439	13·23·31
20	70	2 ² ·5·11·41	2·5·907	2 ⁵ ·3·5·19	2·5·7·131	2 ² ·5·461	2·3 ² ·5·103
21	71	3·31·97	47·193	7·1303	3 ² ·1019	73·127
22	72	2·13·347	2 ⁴ ·3 ⁴ ·7	2·4561	2 ² ·2293	2·3·29·53	2 ³ ·19·61
23	73	7·1289	43·211	3·3041	23·401	3·11·281
24	74	2 ⁶ ·3·47	2·13·349	2 ² ·2281	2·3·11·139	2 ³ ·11·53	2·4637
25	75	5 ² ·19 ²	3·5 ² ·11 ²	5 ³ ·73	5 ² ·367	3 ² ·5 ² ·41	5 ² ·7·53
26	76	2·4513	2 ² ·2269	2·3 ³ ·13 ²	2 ³ ·31·37	2·7·659	2 ² ·3·773
27	77	3 ² ·17·59	29·313	3·7·19·23
28	78	2 ² ·37·61	2·3·17·89	2 ³ ·7·163	2·13·353	2 ² ·3·769	2·4639
29	79	7·1297	3·17·179	67·137	11·839	3 ² ·1031
30	80	2·3·5·7·43	2 ³ ·5·227	2·5·11·83	2 ² ·3 ³ ·5·17	2·5·13·71	2 ⁶ ·5·29
31	81	11·821	3 ² ·1009	23·397	3·17·181
32	82	2 ³ ·11·29	2·19·239	2 ² ·3·761	2·4591	2 ⁴ ·577	2·3·7·13·17
33	83	3·3011	31·293	3·3061	7·1319
34	84	2·4517	2 ² ·3·757	2·4567	2 ⁵ ·7·41	2·3 ⁵ ·19	2 ² ·11·211
35	85	5·13·139	5·23·79	3 ² ·5·7·29	5·11·167	5·1847	3·5·619
36	86	2 ² ·3 ² ·251	2·7·11·59	2 ⁴ ·571	2·3·1531	2 ² ·2309	2·4643
37	87	7·1291	3·13·233	3·3079	37·251
38	88	2·4519	2 ⁷ ·71	2·3·1523	2 ² ·2297	2·31·149	2 ³ ·3 ³ ·43
39	89	3·23·131	61·149	13·19·37	3 ² ·1021	7·1327
40	90	2 ⁴ ·5·113	2·3 ² ·5·101	2 ² ·5·457	2·5·919	2 ³ ·3·5·7·11	2·5·929
41	91	3·11·277	7·13·101	3·19·163
42	92	2·3·11·137	2 ² ·2273	2·7·653	2 ³ ·3·383	2·4621	2 ² ·23·101
43	93	3·7·433	41·223	29·317	3 ² ·13·79
44	94	2 ² ·7·17·19	2·4547	2 ³ ·3 ² ·127	2·4597	2 ² ·2311	2·3·1549
45	95	3 ³ ·5·67	5·17·107	5·31·59	3·5·613	5·43 ²	5·11·13 ²
46	96	2·4523	2 ³ ·3·379	2·17·269	2 ² ·11 ² ·19	2·3·23·67	2 ⁴ ·7·83
47	97	83·109	11·827	3·3049	17·541	7·1321	3 ² ·1033
48	98	2 ³ ·3·13·29	2·4549	2 ² ·2287	2·3 ² ·7·73	2 ⁵ ·17 ²	2·4649
49	99	3 ⁸ ·337	7·1307	3·3083	17·547
50	100	2·5 ² ·181	2 ² ·5 ² ·7·13	2·3·5 ² ·61	2 ⁴ ·5 ² ·23	2·5 ³ ·37	2 ² ·3·5 ² ·31

Prime Numbers and Factors, 9300-9600.

From To	9300 9350	9350 9400	9400 9450	9450 9500	9500 9550	9550 9600
0	50	2 ² ·3·5 ² ·31	2 ² ·5 ² ·11·17	2 ³ ·5 ² ·47	2 ³ ·3 ³ ·5 ² ·7	2 ² ·5 ³ ·19
1	51	71·131	3 ² ·1039	7·17·79	13·727	3·3167
2	52	2·4651	2 ³ ·7·167	2·3·1567	2 ² ·17·139	2·4751
3	53	3·7·443	47·199	3·23·137	13·17·43
4	54	2 ³ ·1163	2·3·1559	2 ² ·2351	2·29·163	2 ⁵ ·3 ³ ·11
5	55	5·1861	5·1871	3 ² ·5·11·19	5·31·61	5·1901
6	56	2 ³ ·2·11·47	2 ² ·2339	2·4703	2 ⁴ ·3·197	2·7 ² ·97
7	57	41·227	3·3119	23·409	7 ² ·193	3·3169
8	58	2 ² ·13·179	2·4679	2 ⁶ ·3·7 ²	2·4729	2 ² ·2377
9	59	3·29·107	7 ² ·191	97 ²	3 ² ·1051	37·257
10	60	2·5·7 ² ·19	2 ⁴ ·3 ² ·5·13	2·5·941	2 ² ·5·11·43	2·3·5·317
11	61	11·23·37	3·3137
12	62	2 ⁵ ·3·97	2·31·151	2 ² ·13·181	2·3·19·83	2 ³ ·29·41
13	63	67·139	3·3121	3 ² ·7·151
14	64	2·4657	2 ² ·2341	2 ³ ·5·23	2 ³ ·7·13 ²	2·67·71
15	65	3 ⁴ ·5·23	5·1873	5·7·269	3·5·631	5·11·173
16	66	2 ² ·17·137	2·3·7·223	2 ³ ·11·107	2·4733	2 ² ·3·13·61
17	67	7·11 ³	17·19·29	3·43·73	31·307
18	68	2·3·1553	2 ³ ·1171	2·17·277	2 ² ·3 ² ·263	2·4759
19	69	3 ³ ·347	17·557	3·19·167
20	70	2 ³ ·5·233	2·5·937	2 ² ·3·5·157	2·5·947	2 ⁴ ·5·7·17
21	71	3·13·239	3·7·11·41
22	72	2·59·79	2 ² ·3·11·71 ²	2·7·673	2 ⁸ ·37	2 ³ ·2 ³ ·2 ³
23	73	7·13·103	3 ³ ·349	89·107
24	74	2 ² ·3 ² ·7·37	2·43·109	2 ⁴ ·19·31	2·3·1579	2 ² ·2381
25	75	5 ² ·373	3·5 ³	5 ² ·13·29	5 ² ·379	3·5 ² ·127
26	76	2·4663	2 ² ·293	2·3·1571	2 ² ·23·103	2·11·433
27	77	3·3109	11·857	3 ⁶ ·13	7·1361
28	78	2 ⁴ ·11·53	2 ³ ·5·521	2 ² ·2357	2·7·677	2 ³ ·3·397
29	79	19·491	83·113	3·7·449	13·733
30	80	2·3·5·311	2 ² ·5·7·67	2·5·23·41	2 ³ ·3·5·79	2·5·953
31	81	7·31·43	3·53·59	19·499	3 ³ ·353
32	82	2 ² ·2333	2·4691	2 ³ ·3 ² ·131	2·11·431	2 ² ·2383
33	83	3 ² ·17·61	11·853	3·29·109
34	84	2·13·359	2 ³ ·3·17·23	2·53·89	2 ² ·2371	2·3·7·227
35	85	5·1867	5·1877	3·5·17·37	5·7·271	5·1907
36	86	2 ³ ·3·389	2·13·19 ²	2 ² ·7·337	2·3 ² ·17·31	2 ⁶ ·149
37	87	3 ² ·7·149	53·179	3·11·17 ²
38	88	2·7·23·29	2 ² ·2347	2·3·11 ² ·13	2 ⁴ ·593	2·19·251
39	89	3·11·283	41·229	3·3163
40	90	2 ² ·5·467	2·3·5·313	2 ⁵ ·5·59	2·5·13·73	2 ² ·3 ² ·5·53
41	91	3 ² ·1049	7·29·47
42	92	2·3 ³ ·173	2 ⁴ ·587	2·4721	2 ² ·3·7·113	2·13·369
43	93	3·31·101	7·19·71	11·863	3·31·81
44	94	2 ⁷ ·73	2·7·11·61	2 ² ·3·787	2·47·101	2 ³ ·1193
45	95	3·5·7·89	5·1879	5·1889	3 ² ·5·211	5·23·83
46	96	2·4673	2 ² ·3 ⁴ ·29	2·4723	2 ³ ·1187	2·3·37·43
47	97	13·719	3·47·67
48	98	2 ² ·3·19·41	2·37·127	2 ³ ·1181	2·3·1583	2 ² ·7·11·31
49	99	3·13·241	11·859	7·23·59	3 ² ·1061
50	100	2·5 ² ·11·17	2 ³ ·5 ² ·47	2·3 ³ ·5 ² ·7	2 ² ·5 ³ ·19	2·5 ² ·191

Prime Numbers and Factors, 9600-9900.

From To	9600 9650	9650 9700	9700 9750	9750 9800	9800 9850	9850 9900
0 50	2 ⁷ ·3·5 ²	2·5 ² ·193	2 ² ·5 ² ·97	2·3·5 ³ ·13	2 ³ ·5 ² ·7 ²	2·5 ² ·197
1 51	3·3217	89·109	7 ² ·199	3 ⁴ ·11 ²
2 52	2·4801	2 ² ·19·127	2·3 ² ·7 ² ·11	2 ³ ·23·53	2·13 ² ·29	2 ² ·3·821
3 53	3 ² ·11·97	7 ² ·197	31·313	3·3251	59·167
4 54	2 ² ·7 ⁴	2·3·1609	2 ³ ·1213	2·4877	2 ² ·3·19·43	2·13·379
5 55	5·17·113	5·1931	3·5·647	5·1951	5·37·53	3 ³ ·5·73
6 56	2·3·1601	2 ³ ·17·71	2·23·211	2 ² ·3 ² ·271	2·4903	2 ⁷ ·7·11
7 57	13·739	3 ² ·29·37	17·571	11·887	3·7·467
8 58	2 ³ ·1201	2·11·439	2 ² ·3·809	2·7·17·41	2 ⁴ ·613	2·3·31·53
9 59	3·3203	13·743	7·19·73	3·3253	17·577
10 60	2·5·31 ²	2 ² ·3·5·7·23	2·5·971	2 ⁵ ·5·61	2·3 ³ ·5·109	2 ² ·5·17·29
11 61	7·1373	3 ² ·13·83	43·227	3·19·173
12 62	2 ² ·3 ³ ·89	2·4831	2 ⁴ ·607	2·3·1627	2 ² ·11·223	2·4931
13 63	3·3221	11·883	13·751	3·3271	7·1409
14 64	2·11·19·23	2 ⁶ ·151	2·3·1619	2 ² ·2441	2·7·701	2 ³ ·3 ² ·137
15 65	3·5·641	5·1933	5·29·67	3 ² ·5·7·31	5·13·151	5·1973
16 66	2 ⁴ ·601	2·3 ³ ·179	2 ² ·7·347	2·19·257	2 ³ ·3·409	2·4933
17 67	59·163	7·1381	3·41·79	3·11·13·23
18 68	2·3·7·229	2 ² ·2417	2·43·113	2 ³ ·3·11·37	2·4909	2 ² ·2467
19 69	3·11·293	3 ² ·1091	71·139
20 70	2 ² ·5·13·37	2·5·967	2 ³ ·3 ⁵ ·5	2·5·977	2 ² ·5·491	2·3·5·7·47
21 71	3 ² ·1069	19·509	3·3257	7·23·61
22 72	2·17·283	2 ³ ·3·13·31	2·4861	2 ² ·7·349	2·3·1637	2 ⁴ ·617
23 73	17·569	3·7·463	29·337	11·19·47	3 ² ·1097
24 74	2 ³ ·3·401	2·7·691	2 ² ·11·13·17	2·3 ³ ·181	2 ⁵ ·307	2·4937
25 75	5 ³ ·7·11	3 ² ·5 ² ·43	5 ² ·389	5 ² ·17·23	3·5 ² ·131	5 ³ ·79
26 76	2·4813	2 ² ·41·59	2·3·1621	2 ⁴ ·13·47	2·17 ³	2 ² ·3·823
27 77	3·3209	71·137	3·3259	31·317	7·17·83
28 78	2 ² ·29·83	2·3·1613	2 ⁹ ·19	2·4889	2 ² ·3 ³ ·7·13	2·11·449
29 79	3 ² ·23·47	7·11·127	3·37·89
30 80	2·3 ² ·5·107	2 ⁴ ·5·11 ²	2·5·7·139	2 ² ·3·5·163	2·5·983	2 ³ ·5·13·19
31 81	3·7·461	37·263	3·29·113	41·241
32 82	2 ⁵ ·7·43	2·47·103	2 ² ·3·811	2·67·73	2 ³ ·1229	2·3 ⁴ ·61
33 83	3·13 ² ·19	2 ³ ·421	3 ² ·1087
34 84	2·4817	2 ² ·3 ² ·269	2·31·157	2 ³ ·1223	2·3·11·149	2 ² ·7·353
35 85	5·41·47	5·13·149	3·5·11·59	5·19·103	5·7·281	3·5·659
36 86	2 ² ·3·11·73	2·29·167	2 ³ ·1217	2·3·7·233	2 ² ·2459	2·4943
37 87	23·419	3·3229	7·13·107	3 ² ·1093
38 88	2·61·79	2 ³ ·7·173	2·3 ² ·541	2 ² ·1247	2·4919	2 ⁵ ·3·103
39 89	3 ⁴ ·7·17	3·13·251	11·29·31
40 90	2 ³ ·5·241	2·3·5·17·19	2 ² ·5·487	2·5·11·89	2 ⁴ ·3·5·41	2·5·23·43
41 91	31·311	11·881	3·17·191	13·757	3 ² ·7·157
42 92	2·3·1607	2 ² ·2423	2·4871	2 ⁶ ·3 ² ·17	2·7·19·37	2 ² ·2473
43 93	3 ³ ·359	7·1399	3·17·193	13·761
44 94	2 ² ·2411	2·37·131	2 ⁴ ·3·7·29	2·59·83	2 ² ·23·107	2·3·17·97
45 95	3·5·643	5·7·277	5·1949	3·5·653	5·11·179	5·1979
46 96	2·7·13·53	2 ⁴ ·3·101	2·11·443	2 ² ·31·79	2·3 ² ·547	2 ³ ·1237
47 97	11·877	3 ³ ·19 ²	97·101	43·229	3·3299
48 98	2 ⁴ ·3 ² ·67	2·13·373	2 ² ·2437	2·3·23·71	2 ³ ·1231	2·7 ² ·101
49 99	3·53·61	41·239	3·7 ² ·67	19·521
50 100	2·5 ² ·193	2 ² ·5 ² ·97	2·3·5 ³ ·13	2 ³ ·5 ² ·7 ²	2·5 ² ·197	2 ² ·3 ² ·5 ² ·11

Prime Numbers and Factors, 9900-10200.

From To	9900 9950	9950 10000	10000 10050	10050 10100	10100 10150	10150 10200
0 50	2 ² ·3 ² ·5 ² ·11	2 ⁵ ·2 ¹⁹⁹	2 ⁴ ·5 ⁴	2 ³ ·5 ² ·67	2 ² ·5 ² ·101	2 ⁵ ·7 ² ·29
1 51	3 ³ ·107	73·137	19·23 ²	3 ⁷ ·13·37
2 52	2·4951	2 ⁵ ·311	2 ³ ·1667	2 ² ·7·359	2·5051	2 ³ ·3 ³ ·47
3 53	3·3301	37·269	7·1429	3 ² ·1117	11·13·71
4 54	2 ⁴ ·619	2 ³ ·7·79	2 ⁹ ·41·61	2·11·457	2 ³ ·3·421	2·5077
5 55	5·7·283	5·11·181	3 ⁵ ·23·29	5·2011	5·43·47	3 ⁵ ·677
6 56	2 ³ ·13·127	2 ² ·19·131	2·5003	2 ³ ·3·419	2 ³ ·163	2 ² ·2539
7 57	3 ³ ·19	89·113	3 ² ·1123	7·1451
8 58	2 ² ·2477	2·13·383	2 ³ ·3 ² ·139	2·47·107	2 ² ·7·19 ²	2 ³ ·1693
9 59	3 ³ ·367	23·433	3 ⁷ ·479	11·919
10 60	2 ⁵ ·991	2 ³ ·3·5·83	2 ⁵ ·7·11·13	2 ² ·5·503	2 ³ ·5·337	2 ⁴ ·5·127
11 61	11·17·53	7·1423	3·47·71	3 ² ·1129
12 62	2 ³ ·3·7·59	2·17·293	2 ² ·2503	2 ³ ·2·13·43	2 ⁷ ·79	2·5081
13 63	23·431	3 ⁵ ·41	17·19·31	29·347	3·3371
14 64	2·4957	2 ² ·47·53	2 ³ ·1669	2 ⁴ ·17·37	2·13·389	2 ² ·3·7·11 ²
15 65	3 ⁵ ·661	5·1993	5·2003	3 ⁵ ·11·61	5 ⁷ ·17 ²	5·19·107
16 66	2 ² ·37·67	2 ³ ·11·151	2 ⁵ ·313	2 ⁷ ·719	2 ² ·3 ² ·281	2 ³ ·13·17·23
17 67	47·211	3 ³ ·7·53	67·151	3·3389
18 68	2 ³ ·2·19·29	2 ⁴ ·7·89	2·5009	2 ² ·3·839	2·5059	2 ³ ·31·41
19 69	7·13·109	3 ³ ·323	43·233	3·3373
20 70	2 ⁶ ·5·31	2 ⁵ ·997	2 ² ·3·5·167	2 ⁵ ·19·53	2 ³ ·5·11·23	2 ³ ·2 ⁵ ·113
21 71	3·3307	13 ² ·59	11·911	3 ³ ·373	29·349	7·1453
22 72	2·11 ² ·41	2 ² ·3 ² ·277	2·5011	3 ³ ·1259	2 ³ ·7·241	2 ² ·2543
23 73	3 ³ ·13·257	7·1439	53·191	3·3391
24 74	2 ² ·3·827	2·4987	2 ³ ·7·179	2 ³ ·23·73	2 ² ·2531	2·5087
25 75	5 ² ·397	3 ⁵ ·2·7·19	5 ² ·401	5 ² ·13·31	3 ⁴ ·5 ³	5 ² ·11·37
26 76	2 ⁷ ·709	2 ³ ·29·43	2 ³ ·2 ⁵ ·57	2 ² ·11·229	2·61·83	2 ⁶ ·3·53
27 77	3 ² ·1103	11·907	37·271	3·3359	13·19·41
28 78	2 ³ ·17·73	2 ³ ·1663	2 ² ·23·109	2·5039	2 ⁴ ·3·211	2·7·727
29 79	17·587	3·3343	7·1447	3 ³ ·13·29
30 80	2 ³ ·5·331	2 ² ·5·499	2 ⁵ ·17·59	2 ⁵ ·3 ² ·5·7	2 ⁵ ·1013	2 ² ·5·509
31 81	3 ² ·1109	7·1433	17·593	3·11·307
32 82	2 ² ·13·191	2 ⁷ ·23·31	2 ⁴ ·3·11·19	2·71 ²	2 ² ·17·149	2 ³ ·1697
33 83	3·7·11·43	67·149	79·127	3·3361	17·599
34 84	2·4967	2 ³ ·3·13	2·29·173	2 ² ·2521	2 ³ ·5·563	2 ³ ·19·67
35 85	5·1987	5·1997	3 ² ·5·223	5·2017	5·2027	3 ⁵ ·7·97
36 86	2 ⁴ ·3 ³ ·23	2·4993	2 ² ·13·193	2 ³ ·41 ²	2 ³ ·7·181	2 ² ·11·463
37 87	19·523	3 ³ ·329	7·11·131	3·31·109	61·167
38 88	2·4969	2 ² ·11·227	2 ³ ·7·239	2 ³ ·13·97	2·37·137	2 ³ ·3 ² ·283
39 89	3·3313	7·1427	3 ² ·19·59	23·443
40 90	2 ² ·5·7·71	2 ³ ·3·5·37	2 ³ ·5·251	2 ⁵ ·1009	2 ² ·3·5·13 ²	2 ⁵ ·1019
41 91	97·103	3·3347	3·43·79
42 92	2 ³ ·1657	2 ³ ·1249	2·5021	2 ² ·3·29 ²	2 ² ·11·461	2 ⁴ ·7 ² ·13
43 93	61·163	3 ³ ·331	11 ² ·83	3 ² ·7 ² ·23
44 94	2 ³ ·11·113	2·19·263	2 ² ·3 ⁴ ·31	2·7 ² ·103	2 ⁵ ·317	2 ³ ·1699
45 95	3 ² ·5·13·17	5·1999	5·7 ² ·41	3 ⁵ ·673	5·2029	5·2039
46 96	2·4973	2 ² ·3·7 ² ·17	2·5023	2 ⁴ ·631	2 ³ ·19·89	2 ² ·2549
47 97	7 ³ ·29	13·769	3·17·197	23·439	73·139	3 ⁴ ·11·103
48 98	2 ² ·3·829	2·4999	2 ⁶ ·157	2 ³ ·11·17	2 ² ·43·59	2·5099
49 99	3 ² ·11·101	13·773	3·17·199	7·31·47
50 100	2 ⁵ ·2 ¹⁹⁹	2 ⁴ ·5 ⁴	2 ³ ·5 ² ·67	2 ² ·5 ² ·101	2 ⁵ ·7·29	2 ² ·3·5 ² ·17

Table of Leads.

Table of Leads.

This table contains all the leads that can be obtained with any possible combination of the change gears furnished with Universal Milling Machines made by Brown & Sharpe Mfg. Co., even though some of the leads are not available for use on account of the gears interfering or not reaching. Combinations of gears that are too small in diameter to reach for right-hand spirals can generally be used for left-hand spirals, as the reverse gear is then required and will enable the gears to reach.

The two driving gears or the two driven gears of any combination can be transposed, but a driver must not be substituted for a driven or vice versa. Four different arrangements of the gears of any combination are thus possible without changing the ratio, and when one arrangement interferes or will not reach, the others should be tried. Thus, the gears to give a lead of 3.60" are : drivers, 100 teeth and 32 teeth ; driven 24 teeth and 48 teeth. By transposing the gears, the following four arrangements may be obtained.

	<i>1st.</i>	<i>2d.</i>	<i>3d.</i>	<i>4th.</i>	
Gear on screw	100	32	100	32	} Drivers.
1st gear on stud	32	100	32	100	
2d gear on Stud	24	24	48	48	} Driven.
Gear on Worm	48	48	24	24	

The first arrangement, however, is the only one available, owing to the interference of the gears in the others preventing their meshing properly.

When very short leads are required, it is preferable to disengage the worm wheel and connect the gearing directly to the spiral head spindle (using the differential indexing centre) instead of to the worm shaft. This method gives leads one fortieth of the leads given in the table for the same combinations of gears. Thus, for a lead of 6.160" the table calls for gear on worm 56 teeth, 1st gear on stud 40 teeth, 2d gear on stud 44 teeth and

gear on screw 100 teeth. Putting the 56 tooth gear on the spindle instead of on the worm, gives a lead of $\frac{6.160}{40} = .154''$.

With this method very short leads may be obtained without excessively straining the mechanism but the regular means of indexing the work cannot be employed. A special face plate or dial can be used or another method is to have the number of teeth in the gear on the spindle some multiple of the number required to be indexed, swinging the gears out of mesh and advancing the gear on spindle the number of teeth required to index the work one division, at each indexing. Thus, if 9 divisions are required with a lead of $.261''$, we select a lead from the table equal to about $.261'' \times 40 = 10.440''$, where the gear on worm (which will now be the gear on spindle) is some multiple of 9, as 72. The nearest lead is $10.467''$, which gives $\frac{10.467}{40} = .2617''$ lead, giving an error of $.0007''$. To index the work, the gear on spindle is advanced $\frac{72}{9} = 8$ teeth at each indexing.

Table of Leads, .670" to 2.182".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
.670	24	86	24	100	1.527	24	44	28	100	1.886	24	56	44	100
.781	24	86	28	100	1.550	24	72	40	86	1.905	24	56	32	72
.800	24	72	24	100	1.556	28	72	40	100	1.919	24	64	44	86
.893	24	86	32	100	1.563	24	86	56	100	1.920	24	40	32	100
.900	24	64	24	100	1.563	28	86	48	100	1.925	28	64	44	100
.930	24	72	24	86	1.595	24	56	32	86	1.944	24	48	28	72
.933	24	72	28	100	1.600	24	48	32	100	1.944	28	64	32	72
1.029	24	56	24	100	1.600	28	56	32	100	1.954	24	40	28	86
1.042	28	86	32	100	1.600	24	72	48	100	1.956	32	72	44	100
1.047	24	64	24	86	1.607	24	56	24	64	1.990	28	72	44	86
1.050	24	64	28	100	1.628	24	48	28	86	1.993	24	56	40	86
1.067	24	72	32	100	1.628	28	64	32	86	2.000	24	40	24	72
1.085	24	72	28	86	1.637	32	86	44	100	2.000	24	48	40	100
1.116	24	86	40	100	1.650	24	64	44	100	2.000	28	56	40	100
1.196	24	56	24	86	1.667	24	56	28	72	2.000	32	64	40	100
1.200	24	48	24	100	1.667	24	48	24	72	2.009	24	86	72	100
1.200	24	56	28	100	1.667	24	64	32	72	2.030	24	44	32	86
1.200	24	64	32	100	1.674	24	40	24	86	2.035	28	64	40	86
1.221	24	64	28	86	1.680	24	40	28	100	2.036	28	44	32	100
1.228	24	86	44	100	1.706	24	72	44	86	2.045	24	44	24	64
1.240	24	72	32	86	1.711	28	72	44	100	2.047	40	86	44	100
1.244	28	72	32	100	1.714	24	56	40	100	2.057	24	28	24	100
1.250	24	64	24	72	1.744	24	64	40	86	2.057	24	56	48	100
1.302	28	86	40	100	1.745	24	44	32	100	2.067	32	72	40	86
1.309	24	44	24	100	1.750	28	64	40	100	2.083	24	64	40	72
1.333	24	72	40	100	1.776	24	44	28	86	2.084	28	86	64	100
1.340	24	86	48	100	1.778	32	72	40	100	2.084	32	86	56	100
1.371	24	56	32	100	1.786	24	86	64	100	2.093	24	64	48	86
1.395	24	48	24	86	1.786	32	86	48	100	2.093	24	32	24	86
1.395	24	56	28	86	1.800	24	64	48	100	2.100	24	64	56	100
1.395	24	64	32	86	1.800	24	32	24	100	2.100	28	64	48	100
1.400	24	48	28	100	1.809	28	72	40	86	2.100	24	32	28	100
1.400	28	64	32	100	1.818	24	44	24	72	2.121	24	44	28	72
1.429	24	56	24	72	1.823	28	86	56	100	2.133	24	72	64	100
1.433	28	86	44	100	1.860	28	56	32	86	2.133	32	72	48	100
1.440	24	40	24	100	1.861	24	72	48	86	2.143	24	56	32	64
1.447	28	72	32	86	1.861	24	48	32	86	2.143	24	48	24	56
1.458	24	64	28	72	1.867	28	48	32	100	2.171	24	72	56	86
1.467	24	72	44	100	1.867	24	72	56	100	2.171	28	48	32	86
1.488	32	86	40	100	1.867	28	72	48	100	2.171	28	72	48	86
1.500	24	64	40	100	1.875	24	48	24	64	2.175	28	72	56	100
1.522	24	44	24	86	1.875	24	56	28	64	2.182	24	44	40	100

Table of Leads, 2.188" to 3.080".

LEAD IN INCHES	DRIVEN GEAR ON WORM	DRIVER 1ST GEAR ON STUD	DRIVEN 2ND GEAR ON STUD	DRIVER GEAR ON SCREW	LEAD IN INCHES	DRIVEN GEAR ON WORM	DRIVER 1ST GEAR ON STUD	DRIVEN 2ND GEAR ON STUD	DRIVER GEAR ON SCREW	LEAD IN INCHES	DRIVEN GEAR ON WORM	DRIVER 1ST GEAR ON STUD	DRIVEN 2ND GEAR ON STUD	DRIVER GEAR ON SCREW
2.188	24	48	28	64	2.500	24	48	28	56	2.800	24	24	28	100
2.193	24	56	44	86	2.500	28	56	32	64	2.800	32	64	56	100
2.200	24	48	44	100	2.500	24	64	48	72	2.800	24	48	56	100
2.200	28	56	44	100	2.500	24	48	32	64	2.812	24	32	24	64
2.200	32	64	44	100	2.500	24	32	24	72	2.828	28	44	32	72
2.222	24	48	32	72	2.514	32	56	44	100	2.843	40	72	44	86
2.222	28	56	32	72	2.532	28	72	56	86	2.845	32	72	64	100
2.233	40	86	48	100	2.537	24	44	40	86	2.849	28	64	56	86
2.233	24	40	32	86	2.546	28	44	40	100	2.857	24	48	32	56
2.238	28	64	44	86	2.558	32	64	44	86	2.857	24	56	48	72
2.240	28	40	32	100	2.558	28	56	44	86	2.857	24	28	24	72
2.250	24	40	24	64	2.558	24	48	44	86	2.865	44	86	56	100
2.274	32	72	44	86	2.567	28	48	44	100	2.867	86	72	24	100
2.286	32	56	40	100	2.571	24	40	24	56	2.880	24	40	48	100
2.292	24	64	44	72	2.593	28	48	32	72	2.894	28	72	64	86
2.326	32	64	40	86	2.605	28	40	32	86	2.894	32	72	56	86
2.326	24	48	40	86	2.605	40	86	56	100	2.909	32	44	40	100
2.326	28	56	40	86	2.618	24	44	48	100	2.917	24	64	56	72
2.333	28	48	40	100	2.619	24	56	44	72	2.917	28	64	48	72
2.333	24	40	28	72	2.625	24	40	28	64	2.917	28	48	32	64
2.338	24	44	24	56	2.640	24	40	44	100	2.917	24	32	28	72
2.344	28	86	72	100	2.658	32	56	40	86	2.924	32	56	44	86
2.368	28	44	32	86	2.667	40	72	48	100	2.933	44	72	48	100
2.381	32	86	64	100	2.667	32	48	40	100	2.934	32	48	44	100
2.381	24	56	40	72	2.667	24	40	32	72	2.946	24	56	44	64
2.386	24	44	28	64	2.674	28	64	44	72	2.950	28	44	40	86
2.392	24	56	48	86	2.678	24	56	40	64	2.977	40	86	64	100
2.392	24	28	24	86	2.679	32	86	72	100	2.984	28	48	44	86
2.400	28	56	48	100	2.700	24	64	72	100	3.000	24	40	28	56
2.400	32	64	48	100	2.713	28	48	40	86	3.000	24	40	32	64
2.424	24	44	32	72	2.727	24	44	32	64	3.000	24	32	40	100
2.431	28	64	40	72	2.727	24	44	28	56	3.000	40	64	48	100
2.442	24	32	28	86	2.727	24	44	24	48	3.000	24	40	24	48
2.442	28	64	48	86	2.743	24	56	64	100	3.030	24	44	40	72
2.442	24	64	56	86	2.743	32	56	48	100	3.044	24	44	48	86
2.445	40	72	44	100	2.743	24	28	32	100	3.055	28	44	48	100
2.450	28	64	56	100	2.750	40	64	44	100	3.055	24	44	56	100
2.456	44	86	48	100	2.778	32	64	40	72	3.056	32	64	44	72
2.481	32	72	48	86	2.778	24	48	40	72	3.056	28	56	44	72
2.481	24	72	64	86	2.778	40	56	28	72	3.056	24	48	44	72
2.489	32	72	56	100	2.791	28	56	48	86	3.070	24	40	44	86
2.489	28	72	64	100	2.791	32	64	48	86	3.080	28	40	44	100

Table of Leads, 3.086" to 3.896".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW
3.086	24	56	72	100	3.349	48	40	24	86	3.637	48	44	24	72
3.101	40	72	48	86	3.360	56	40	24	100	3.646	40	48	28	64
3.101	32	48	40	86	3.360	48	40	28	100	3.655	40	56	44	86
3.111	28	40	32	72	3.383	32	44	40	86	3.657	64	56	32	100
3.111	40	72	56	100	3.403	28	64	56	72	3.663	72	64	28	86
3.117	24	44	32	56	3.409	24	44	40	64	3.667	40	48	44	100
3.125	28	56	40	64	3.411	32	48	44	86	3.667	44	40	24	72
3.125	24	48	40	64	3.411	44	72	48	86	3.673	24	28	24	56
3.126	48	86	56	100	3.422	44	72	56	100	3.684	44	86	72	100
3.140	24	86	72	64	3.428	24	40	32	56	3.686	86	56	24	100
3.143	40	56	44	100	3.429	40	28	24	100	3.704	32	48	40	72
3.150	28	100	72	64	3.429	40	56	48	100	3.721	24	24	32	86
3.175	32	56	40	72	3.438	24	48	44	64	3.721	64	48	24	86
3.182	28	44	32	64	3.438	28	56	44	64	3.721	64	56	28	86
3.182	24	44	28	48	3.488	40	64	48	86	3.733	48	72	56	100
3.189	32	56	48	86	3.488	40	32	24	86	3.733	56	48	32	100
3.189	24	28	32	86	3.491	64	44	24	100	3.733	64	48	28	100
3.190	24	86	64	56	3.491	48	44	32	100	3.733	28	24	32	100
3.198	40	64	44	86	3.492	32	56	44	72	3.750	24	32	24	48
3.200	28	100	64	56	3.500	40	64	56	100	3.750	24	32	28	56
3.200	24	100	64	48	3.500	28	32	40	100	3.750	28	56	48	64
3.200	24	24	32	100	3.500	28	40	32	64	3.763	86	64	28	100
3.214	24	56	48	64	3.500	24	40	28	48	3.771	44	56	48	100
3.214	24	32	24	56	3.520	32	40	44	100	3.772	24	28	44	100
3.214	24	28	24	64	3.535	28	44	40	72	3.799	56	48	28	86
3.225	24	100	86	64	3.552	56	44	24	86	3.809	24	28	32	72
3.241	28	48	40	72	3.552	48	44	28	86	3.810	64	56	24	72
3.256	24	24	28	86	3.556	40	72	64	100	3.810	32	56	48	72
3.256	24	86	56	48	3.564	56	44	28	100	3.818	24	40	28	44
3.256	32	64	56	86	3.565	28	48	44	72	3.819	40	64	44	72
3.267	28	48	56	100	3.571	24	48	40	56	3.822	86	72	32	100
3.273	24	40	24	44	3.571	32	56	40	64	3.837	24	32	44	86
3.275	44	86	64	100	3.572	48	86	64	100	3.837	44	64	48	86
3.281	24	32	28	64	3.582	44	40	28	86	3.840	64	40	24	100
3.300	44	64	48	100	3.588	72	56	24	86	3.840	32	40	48	100
3.300	44	32	24	100	3.600	72	48	24	100	3.850	44	64	56	100
3.308	32	72	64	86	3.600	72	64	32	100	3.850	28	32	44	100
3.333	32	64	48	72	3.600	72	56	28	100	3.876	24	72	100	86
3.333	28	56	48	72	3.600	48	32	24	100	3.889	32	64	56	72
3.333	28	48	32	56	3.618	56	72	40	86	3.889	56	48	24	72
3.345	28	100	86	72	3.636	24	44	32	48	3.889	24	24	28	72
3.349	40	86	72	100	3.636	28	44	32	56	3.896	24	44	40	56

Table of Leads, 3.907" to 4.778".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
3.907	28	40	48	86	4.200	48	64	56	100	4.480	56	40	82	100
3.907	56	40	24	86	4.200	56	32	24	100	4.480	64	40	28	100
3.911	44	72	64	100	4.200	28	32	48	100	4.500	72	64	40	100
3.920	28	40	56	100	4.200	72	48	28	100	4.500	48	40	24	64
3.927	72	44	24	100	4.242	28	44	32	48	4.500	24	32	24	40
3.929	32	56	44	64	4.242	28	44	48	72	4.522	100	72	28	86
3.929	24	48	44	56						4.537	56	48	28	72
3.977	28	44	40	64	4.242	24	44	56	72	4.545	24	44	40	48
3.979	44	72	56	86	4.253	64	56	32	86	4.546	28	44	40	56
3.987	24	28	40	86	4.264	40	48	44	86	4.546	32	44	40	64
3.987	40	56	48	86	4.267	64	48	32	100	4.548	44	72	64	86
4.000	24	40	32	48	4.267	48	72	64	100	4.558	56	40	28	86
4.000	28	40	32	56	4.278	28	40	44	72	4.567	72	44	24	86
4.000	24	24	40	100	4.286	24	28	24	48	4.572	40	56	64	100
4.000	24	40	48	72	4.286	24	28	32	64	4.572	32	28	40	100
4.011	28	48	44	64	4.286	32	56	48	64	4.582	72	44	28	100
4.019	72	86	48	100	4.300	86	56	28	100	4.583	44	64	48	72
4.040	32	44	40	72	4.300	86	64	32	100	4.583	44	32	24	72
4.059	32	44	48	86	4.300	86	48	24	100	4.584	32	48	44	64
4.060	64	44	24	86	4.320	72	40	24	100	4.584	28	48	44	56
4.070	28	32	40	86	4.341	48	72	56	86	4.651	40	24	24	86
4.070	40	64	56	86	4.341	56	48	32	86	4.655	64	44	32	100
4.073	64	44	28	100	4.342	64	48	28	86	4.667	28	40	32	48
4.073	56	44	32	100	4.342	28	24	32	86	4.667	40	24	28	100
4.074	32	48	44	72	4.361	100	64	24	86	4.667	56	40	24	72
4.091	24	44	48	64	4.363	24	40	32	44	4.667	48	40	28	72
4.091	24	32	24	44	4.364	40	44	48	100	4.667	40	48	56	100
4.093	32	40	44	86	4.365	40	56	44	72	4.675	24	28	24	44
4.114	48	28	24	100	4.375	24	24	28	64	4.675	48	44	24	56
4.114	72	56	32	100	4.375	24	32	28	48	4.687	40	32	24	64
4.125	24	40	44	64	4.375	56	48	24	64	4.688	56	86	72	100
4.135	40	72	64	86	4.386	24	28	44	86	4.691	86	44	24	100
4.144	56	44	28	86	4.386	44	56	48	86	4.714	44	40	24	56
4.167	28	48	40	56	4.400	24	24	41	100	4.736	64	44	28	86
4.167	40	64	48	72	4.444	64	56	28	72	4.736	56	44	32	86
4.167	32	48	40	64	4.444	24	24	32	72	4.762	40	28	24	72
4.167	24	32	40	72	4.444	64	48	24	72	4.762	40	48	32	56
4.167	56	86	64	100	4.465	64	40	24	86	4.762	40	56	48	72
4.186	72	64	32	86	4.466	48	40	32	86	4.773	24	32	28	44
4.186	48	32	24	86	4.477	44	32	28	86	4.773	56	44	24	64
4.186	72	48	24	86	4.477	56	64	44	86	4.773	48	44	28	64
4.186	72	56	28	86	4.479	86	64	24	72	4.778	86	72	40	100

Table of Leads, 4.784" to 5.733".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
4.784	72	56	32	86	5.116	44	24	24	86	5.358	64	86	72	100
4.785	48	28	24	86	5.119	86	56	24	72	5.375	86	64	40	100
4.800	48	24	24	100	5.120	64	40	32	100	5.400	72	32	24	100
4.800	56	28	24	100	5.133	56	48	44	100	5.400	72	64	48	100
4.800	64	32	24	100	5.134	44	24	28	100	5.413	64	44	32	86
4.800	72	48	32	100	5.142	72	56	40	100	5.426	40	24	28	86
4.813	44	40	28	64	5.143	24	28	24	40	5.427	40	48	56	86
4.821	72	56	24	64	5.143	24	40	48	56	5.444	56	40	28	72
4.849	32	44	48	72	5.156	44	32	24	64	5.455	48	44	28	56
4.849	64	44	24	72	5.160	86	40	24	100	5.455	32	44	48	64
4.861	40	32	28	72	5.168	100	72	32	86	5.469	40	32	28	64
4.861	56	64	40	72	5.185	28	24	32	72	5.473	86	44	28	100
4.884	48	64	56	86	5.186	64	48	28	72	5.486	64	28	24	100
4.884	72	48	28	86	5.186	56	48	32	72	5.486	48	28	32	100
4.884	48	32	28	86	5.195	32	44	40	56	5.486	48	56	64	100
4.884	56	32	24	86	5.209	100	64	24	72	5.500	44	40	24	48
4.889	32	40	44	72	5.210	64	40	28	86	5.500	44	40	32	64
4.898	24	28	32	56	5.210	56	40	32	86	5.500	40	32	44	100
4.900	56	32	28	100	5.226	86	64	28	72	5.500	44	40	28	56
4.911	40	56	44	64	5.233	72	64	40	86	5.556	40	24	24	72
4.914	86	56	32	100	5.236	72	44	32	100	5.568	56	44	28	64
4.950	56	44	28	72	5.238	44	28	24	72	5.581	64	32	24	86
4.950	72	64	44	100	5.238	32	48	44	56	5.581	56	28	24	86
4.961	64	48	32	86	5.238	44	56	48	72	5.581	72	48	32	86
4.961	64	72	48	86	5.250	24	32	28	40	5.582	48	24	24	86
4.978	56	72	64	100	5.250	56	40	24	64	5.600	56	24	24	100
4.984	100	56	24	86	5.250	48	40	28	64	5.600	48	24	28	100
5.000	24	24	28	56	5.256	86	72	44	100	5.600	64	32	28	100
5.000	24	24	32	64	5.280	48	40	44	100	5.625	48	32	24	64
5.000	48	32	24	72	5.303	28	44	40	48	5.625	72	48	24	64
5.017	86	48	28	100	5.316	40	28	32	86	5.625	72	56	28	64
5.023	72	40	24	86	5.316	40	56	64	86	5.657	56	44	32	72
5.029	44	28	32	100	5.328	72	44	28	86	5.657	72	56	44	100
5.029	64	56	44	100	5.333	40	24	32	100	5.657	64	44	28	72
5.040	72	40	28	100	5.333	64	40	24	72	5.698	56	32	28	86
5.074	40	44	48	86	5.333	32	40	48	72	5.714	48	28	24	72
5.080	64	56	32	72	5.333	40	48	64	100	5.714	24	28	32	48
5.088	100	64	28	86	5.347	44	64	56	72	5.714	24	24	32	56
5.091	56	44	40	100	5.348	44	32	28	72	5.714	64	48	24	56
5.091	28	40	32	44	5.357	40	28	24	64	5.730	40	48	44	64
5.093	40	48	44	72	5.357	40	32	24	56	5.733	86	48	32	100
5.105	28	48	56	64	5.357	40	56	48	64	5.733	86	72	48	100

Table of Leads, 5.756 to 6.757".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
5.756	72	64	44	86	6.089	72	44	32	86	6.417	44	40	28	48
5.759	86	56	24	64	6.109	56	44	48	100	6.429	24	28	24	32
5.760	72	40	32	100	6.112	24	24	44	72	6.429	48	28	24	64
5.788	64	72	56	86	6.122	40	28	24	56	6.429	48	32	24	56
5.814	100	64	32	86	6.125	56	40	28	64	6.429	72	48	24	56
5.814	100	56	28	86	6.137	72	44	24	64	6.429	72	56	32	64
5.814	100	48	24	86	6.140	48	40	44	86	6.450	86	64	48	100
5.818	64	44	40	100	6.143	86	56	40	100	6.450	86	32	24	100
5.833	28	24	24	48	6.160	56	40	44	100	6.460	100	72	40	86
5.833	32	24	28	64						6.465	64	44	32	72
5.833	56	32	24	72	6.171	72	56	48	100	6.482	56	48	40	72
5.833	48	32	28	72	6.172	72	28	24	100	6.482	40	24	28	72
5.833	56	48	32	64	6.202	40	24	32	86	6.512	56	24	24	86
5.833	56	64	48	72	6.202	64	48	40	86	6.512	64	32	28	86
5.847	64	56	44	86	6.222	64	40	28	72	6.512	48	24	28	86
5.848	44	28	32	86	6.222	56	40	32	72	6.515	86	44	24	72
5.861	72	40	28	86	6.234	32	28	24	44	6.534	56	24	28	100
5.867	44	24	32	100	6.234	64	44	24	56	6.545	48	40	24	44
5.867	64	48	44	100	6.234	48	44	32	56	6.545	72	44	40	100
5.893	44	32	24	56	6.250	24	24	40	64	6.548	44	48	40	56
5.893	44	28	24	64	6.250	40	32	24	48	6.563	56	32	24	64
5.893	48	56	44	64	6.250	40	32	28	56	6.563	72	48	28	64
5.912	86	64	44	100	6.255	86	44	32	100	6.563	48	32	28	64
5.920	56	44	40	86	6.279	72	64	48	86	6.578	72	56	44	86
5.926	64	48	32	72	6.279	72	32	24	86	6.600	48	32	44	100
5.952	100	56	24	72	6.286	44	40	32	56	6.600	72	48	44	100
5.954	64	40	32	86	6.286	44	28	40	100	6.645	100	56	32	86
5.969	44	24	28	86	6.300	72	32	28	100	6.667	64	48	28	56
5.969	56	48	44	86	6.300	72	64	56	100	6.667	32	24	28	56
5.972	86	48	24	72	6.343	100	44	24	86	6.667	32	24	24	48
5.972	86	56	28	72	6.350	40	28	32	72	6.667	48	24	24	72
5.972	86	64	32	72	6.350	64	56	40	72	6.667	56	28	24	72
5.980	72	56	40	86	6.364	56	44	24	48	6.667	64	32	24	72
6.000	48	40	28	56	6.364	56	44	32	64	6.689	86	72	56	100
6.000	48	40	32	64	6.364	24	24	28	44	6.697	100	56	24	64
6.000	48	32	40	100	6.379	64	28	24	86	6.698	72	40	32	86
6.000	72	48	40	100	6.379	48	28	32	86	6.719	86	48	24	64
6.016	44	32	28	64	6.379	64	56	48	86	6.719	86	56	28	64
6.020	86	40	28	100	6.396	44	32	40	86	6.720	56	40	48	100
6.061	40	44	32	48	6.400	64	24	24	100	6.735	44	28	24	56
6.061	48	44	40	72	6.400	48	24	32	100	6.750	72	40	24	64
6.077	100	64	28	72	6.400	56	28	32	100	6.757	86	56	44	100

Table of Leads, 6.766" to 7.883".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
6.766	64	44	40	86	7.159	72	44	28	64	7.525	86	32	28	100
6.784	100	48	28	86	7.163	56	40	44	86	7.525	86	64	56	100
6.806	56	32	28	72	7.167	86	40	24	72	7.543	48	28	44	100
6.818	40	32	24	44	7.167	86	48	40	100	7.576	100	44	24	72
6.818	48	44	40	64	7.176	72	28	24	86	7.597	56	24	28	86
6.822	44	24	32	86	7.176	72	56	48	86	7.601	86	44	28	72
6.822	64	48	44	86	7.200	72	24	24	100	7.611	72	44	40	86
6.825	86	56	32	72	7.268	100	64	40	86	7.619	64	48	32	56
6.857	32	28	24	40	7.272	64	44	28	56	7.619	64	56	48	72
6.857	64	40	24	56	7.273	32	24	24	44	7.620	64	28	24	72
6.857	48	40	32	56	7.273	64	44	24	48	7.620	48	28	32	72
6.857	48	28	40	100	7.292	56	48	40	64	7.636	56	40	24	44
6.875	44	24	24	64	7.292	40	32	28	48	7.636	48	40	28	44
6.875	44	32	24	48	7.292	40	24	28	64	7.639	44	32	40	72
6.875	44	32	28	56	7.310	44	28	40	86	7.644	86	72	64	100
6.880	86	40	32	100	7.314	64	28	32	100	7.657	56	32	28	64
6.944	100	48	24	72	7.325	72	32	28	86	7.674	72	48	44	86
6.944	100	64	32	72	7.326	72	64	56	86	7.675	48	32	44	86
6.945	100	56	28	72	7.330	86	44	24	64	7.679	86	48	24	56
6.968	86	48	28	72	7.333	44	24	40	100	7.679	86	56	32	64
6.977	48	32	40	86	7.333	48	40	44	72	7.680	64	40	48	100
6.977	100	40	24	86	7.334	44	40	32	48	7.700	56	32	44	100
6.977	72	48	40	86	7.347	48	28	24	56	7.714	72	40	24	56
6.982	64	44	48	100	7.371	86	56	48	100	7.752	100	48	32	86
6.984	44	28	32	72	7.372	86	28	24	100	7.752	100	72	48	86
6.984	64	56	44	72	7.400	100	44	28	86	7.778	32	24	28	48
7.000	28	24	24	40	7.408	40	24	32	72	7.778	56	24	24	72
7.000	56	40	24	48	7.408	64	48	40	72	7.778	48	24	28	72
7.000	56	40	32	64	7.424	56	44	28	48	7.778	64	32	28	72
7.000	56	32	40	100	7.442	64	24	24	86	7.792	40	28	24	44
7.013	72	44	24	56	7.442	48	24	32	86	7.792	48	44	40	56
7.040	64	40	44	100	7.442	56	28	32	86	7.813	100	48	24	64
7.071	56	44	40	72	7.465	86	64	40	72	7.813	100	56	28	64
					7.467	64	24	28	100	7.815	56	40	48	86
7.104	56	44	48	86						7.818	86	44	40	100
7.106	100	72	44	86	7.467	56	24	32	100	7.838	86	48	28	64
7.111	64	40	32	72	7.467	64	48	56	100	7.855	72	44	48	100
7.130	44	24	28	72	7.500	48	24	24	64	7.857	44	24	24	56
7.130	56	48	44	72	7.500	56	28	24	64	7.857	44	28	24	48
7.143	40	28	32	64	7.500	48	32	28	56	7.872	44	28	32	64
7.143	40	28	24	48	7.500	72	48	28	56	7.875	72	40	28	64
7.143	40	24	24	56	7.500	72	48	32	64	7.883	86	48	44	100

Table of Leads, 7.920" to 9.302".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
7.920	72	40	44	100	8.333	48	32	40	72	8.772	48	28	44	86
7.936	100	56	32	72	8.333	100	40	24	72	8.800	48	24	44	100
7.954	40	32	28	44	8.334	40	24	28	56	8.800	64	32	44	100
7.955	56	44	40	64	8.361	86	40	28	72	8.800	56	28	44	100
7.963	86	48	32	72	8.372	72	24	24	86	8.838	100	44	28	72
7.974	48	28	40	86	8.377	86	44	24	56	8.839	72	56	44	64
7.994	100	64	44	86	8.400	72	24	28	100	8.889	64	24	24	72
8.000	64	32	40	100	8.400	56	32	48	100	8.889	56	28	32	72
8.000	32	24	24	40	8.400	72	48	56	100	8.889	48	24	32	72
8.000	64	40	24	48	8.437	72	32	24	64	8.909	56	40	28	44
8.000	64	40	28	56	8.457	100	44	32	86	8.929	100	48	24	56
8.000	56	28	40	100	8.484	32	24	28	44	8.929	100	56	32	64
8.000	48	24	40	100	8.485	64	44	28	48	8.930	64	40	48	86
8.021	44	32	28	48	8.485	56	44	32	48	8.953	56	32	44	86
8.021	44	24	28	64	8.485	56	44	48	72	8.959	86	48	28	56
8.021	56	48	44	64	8.506	64	28	32	86	8.959	86	32	24	72
8.035	72	56	40	64	8.523	100	44	24	64	8.959	86	64	48	72
8.063	86	40	24	64	8.527	44	24	40	86	8.959	86	48	28	56
8.081	64	44	40	72	8.532	86	56	40	72	8.960	64	40	56	100
8.102	100	48	28	72	8.534	64	24	32	100	8.980	44	28	32	56
8.119	64	44	48	86	8.552	86	44	28	64	9.000	48	32	24	40
8.140	56	32	40	86	8.556	56	40	44	72	9.000	72	40	24	48
8.140	100	40	28	86	8.572	64	32	24	56	9.000	72	40	28	56
8.145	64	44	56	100	8.572	48	28	32	64	9.000	72	40	32	64
8.148	64	48	44	72	8.572	48	24	24	56	9.000	72	32	40	100
8.149	44	24	32	72	8.572	72	48	32	56	9.044	100	72	56	86
8.163	40	28	32	56	8.594	44	32	40	64	9.074	56	24	28	72
8.167	56	40	28	48	8.600	86	24	24	100	9.091	40	24	24	44
8.182	48	32	24	44	8.640	72	40	48	100	9.115	100	48	28	64
8.182	72	44	24	48	8.681	100	64	40	72	9.134	72	44	48	86
8.182	72	44	28	56	8.682	64	24	28	86	9.137	100	56	44	86
8.182	72	44	32	64	8.682	56	24	32	86	9.143	64	40	32	56
8.186	64	40	44	86	8.682	64	48	56	86	9.143	64	28	40	100
8.212	86	64	44	72	8.687	86	44	32	72	9.164	72	44	56	100
8.229	72	28	32	100	8.721	100	32	24	86	9.167	44	24	24	48
8.229	72	56	64	100	8.721	100	64	48	86	9.167	44	24	28	56
8.250	44	32	24	40	8.727	48	40	32	44	9.167	44	24	32	64
8.250	48	40	44	64	8.730	44	28	40	72	9.167	48	32	44	72
8.306	100	56	40	86	8.750	28	24	24	32	9.210	72	40	44	86
8.312	64	44	32	56	8.750	56	32	24	48	9.214	86	40	24	56
8.333	40	24	24	48	8.750	56	24	24	64	9.260	100	48	32	72
8.333	40	24	32	64	8.750	48	24	28	64	9.302	48	24	40	86

Table of Leads, 9.303" to 10.477".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
9.303	56	28	40	86	9.675	86	64	72	100	10.101	100	44	32	72
9.303	64	32	40	86	9.690	100	48	40	86	10.159	64	28	32	72
9.303	100	40	32	86	9.697	64	48	32	44	10.175	100	32	28	86
9.333	64	40	28	48	9.697	64	44	48	72	10.175	100	64	56	86
9.333	56	40	32	48	9.723	40	24	28	48	10.182	64	40	28	44
9.333	56	24	40	100	9.723	56	32	40	72	10.182	56	40	32	44
9.333	56	40	48	72	9.723	100	40	28	72	10.186	44	24	40	72
9.334	32	24	28	40	9.741	100	44	24	56	10.209	56	24	28	64
9.351	48	28	24	44	9.768	72	48	56	86	10.209	56	32	28	48
9.351	72	44	32	56	9.768	56	32	48	86	10.228	72	44	40	64
9.375	48	32	40	64	9.768	72	24	28	86	10.233	48	24	44	86
9.375	100	40	24	64	9.773	86	44	24	48	10.233	56	28	44	86
9.375	72	48	40	64	9.773	86	44	28	56	10.233	64	32	44	86
9.382	86	44	48	100	9.773	86	44	32	64	10.238	86	28	24	72
9.385	86	56	44	72	9.778	64	40	44	72	10.238	86	48	32	56
9.406	86	40	28	64	9.796	64	28	24	56	10.238	86	56	48	72
9.428	44	28	24	40	9.796	48	28	32	56	10.267	56	24	44	100
9.429	48	40	44	56	9.818	72	40	24	44	10.286	48	28	24	40
9.460	86	40	44	100	9.822	44	32	40	56	10.286	72	40	32	56
9.472	64	44	56	86	9.822	44	28	40	64	10.286	72	28	40	100
9.524	40	28	32	48	9.828	86	28	32	100	10.312	48	32	44	64
9.524	40	24	32	56	9.828	86	56	64	100	10.313	72	48	44	64
9.524	48	28	40	72	9.844	72	32	28	64	10.320	86	40	48	100
9.524	64	48	40	56	9.900	72	32	44	100	10.336	100	72	64	86
9.545	72	44	28	48	9.921	100	56	40	72	10.370	64	24	28	72
9.546	56	32	24	44	9.923	64	24	32	86	10.370	56	24	32	72
9.546	48	32	28	44	9.943	100	44	28	64	10.371	64	48	56	72
9.547	56	44	48	64	9.954	86	48	40	72	10.390	40	28	32	44
9.549	100	64	44	72	9.967	100	56	48	86	10.390	64	44	40	56
9.556	86	40	32	72	9.968	100	28	24	86	10.417	100	32	24	72
9.569	72	28	32	86	10.000	56	28	24	48	10.417	100	48	28	56
9.569	72	56	64	86	10.000	48	24	28	56	10.417	100	48	32	64
9.598	86	56	40	64	10.000	64	32	24	48	10.417	100	64	48	72
9.600	72	24	32	100	10.000	64	32	28	56	10.419	64	40	56	86
9.600	56	28	48	100	10.000	56	28	32	64	10.451	86	32	28	72
9.600	64	32	48	100	10.000	48	24	32	64	10.451	86	64	56	72
9.600	72	48	64	100	10.033	86	24	28	100	10.467	72	32	40	86
9.625	44	32	28	40	10.033	86	48	56	100	10.473	72	44	64	100
9.625	56	40	44	64	10.046	72	40	48	86	10.476	44	24	32	56
9.643	72	32	24	56	10.057	64	28	44	100	10.476	44	28	32	48
9.643	72	28	24	64	10.078	86	32	24	64	10.477	48	28	44	72
9.643	72	56	48	64	10.080	72	40	56	100	10.477	64	48	44	56

Table of Leads, 10.500" to 12.272".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
10.500	56	32	24	40	11.111	48	24	40	72	11.667	64	32	28	48
10.500	48	32	28	40	11.111	56	28	40	72	11.667	56	32	48	72
10.500	72	40	28	48	11.111	64	32	40	72	11.667	56	24	32	64
10.500	56	40	48	64	11.111	100	40	32	72	11.688	72	44	40	56
10.558	86	56	44	64	11.137	56	32	28	44	11.695	64	28	44	86
10.571	100	44	40	86	11.160	100	56	40	64	11.719	100	32	24	64
10.606	56	44	40	48	11.163	72	24	32	86	11.721	72	40	56	86
10.606	40	24	28	44	11.163	56	28	48	86	11.728	86	40	24	44
10.631	64	28	40	86	11.163	72	48	64	86	11.733	64	24	44	100
10.655	72	44	56	86	11.163	64	32	48	86	11.757	86	32	28	64
10.659	100	48	44	86	11.169	86	44	32	56	11.785	72	48	44	56
10.667	64	40	48	72	11.198	86	48	40	64	11.786	44	28	24	32
10.667	64	24	40	100	11.200	56	24	48	100	11.786	48	32	44	56
10.667	64	40	32	48	11.200	64	32	56	100	11.786	48	28	44	64
10.694	44	24	28	48	11.225	44	28	40	56	11.825	86	32	44	100
10.694	56	32	44	72	11.250	72	24	24	64	11.852	64	24	32	72
10.713	40	28	24	32	11.250	72	32	24	48	11.905	100	28	24	72
10.714	48	32	40	56	11.250	72	32	28	56	11.905	100	48	32	56
10.714	48	28	40	64	11.313	64	44	56	72	11.905	100	56	48	72
10.714	100	40	24	56	11.314	72	28	44	100	11.938	56	24	44	86
10.714	72	48	40	56	11.363	100	44	24	48	11.944	86	24	24	72
10.750	86	40	24	48	11.363	100	44	28	56	11.960	72	28	40	86
10.750	86	40	28	56	11.363	100	44	32	64	12.000	48	24	24	40
10.750	86	40	32	64	11.401	86	44	28	48	12.000	56	28	24	40
10.750	86	32	40	100	11.429	32	24	24	28	12.000	64	32	24	40
10.800	72	32	48	100	11.429	64	28	24	48	12.000	72	40	32	48
10.853	56	24	40	86	11.429	64	24	24	56	12.000	72	24	40	100
10.859	86	44	40	72	11.429	48	24	32	56	12.031	56	32	44	64
10.909	72	44	32	48	11.454	72	40	28	44	12.040	86	40	56	100
10.909	56	28	24	44	11.459	44	24	40	64	12.121	40	24	32	44
10.909	48	24	24	44	11.459	44	32	40	48	12.121	64	44	40	48
10.909	64	32	24	44	11.467	86	24	32	100	12.153	100	32	28	72
10.913	100	56	44	72	11.467	86	48	64	100	12.153	100	64	56	72
10.937	56	32	40	64	11.512	72	32	44	86	12.178	72	44	64	86
10.937	100	40	28	64	11.518	86	28	24	64	12.216	86	44	40	64
10.945	86	44	56	100	11.518	86	32	24	56	12.222	44	24	32	48
10.949	86	48	44	72	11.518	86	56	48	64	12.222	48	24	44	72
10.972	64	28	48	100	11.520	72	40	64	100	12.222	56	28	44	72
11.000	44	24	24	40	11.574	100	48	40	72	12.222	64	32	44	72
11.021	72	28	24	56	11.629	100	24	24	86	12.245	48	28	40	56
11.057	86	56	72	100	11.638	64	40	32	44	12.250	56	32	28	40
11.111	40	24	32	48	11.667	56	24	24	48	12.272	72	32	24	44

Table of Leads, 12.272" to 14.322".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
12.272	72	44	48	64	12.900	86	32	48	100	13.566	100	48	56	86
12.277	100	56	44	64	12.900	86	48	72	100	13.611	56	24	28	48
12.286	86	28	40	100	12.963	56	24	40	72	13.636	48	32	40	44
12.286	86	40	32	56	12.987	100	44	32	56	13.636	100	40	24	44
12.318	86	48	44	64	13.020	100	48	40	64	13.636	72	44	40	48
12.343	72	28	48	100	13.024	56	24	48	86	13.643	64	24	44	86
12.375	72	40	44	64	13.024	64	32	56	86	13.650	86	28	32	72
12.403	64	24	40	86	13.030	86	44	32	48	13.650	86	56	64	72
12.444	64	40	56	72	13.030	86	44	48	72	13.672	100	32	28	64
12.468	64	28	24	44	13.062	64	28	32	56	13.682	86	40	28	44
12.468	48	28	32	44	13.082	100	64	72	86	13.713	64	40	48	56
12.468	64	44	48	56	13.090	72	40	32	44	13.715	64	28	24	40
12.500	40	24	24	32	13.096	44	28	40	48	13.715	48	28	32	40
12.500	48	24	40	64	13.096	44	24	40	56	13.750	44	24	24	32
12.500	56	28	40	64	13.125	72	32	28	48	13.750	48	24	44	64
12.500	100	40	24	48	13.125	72	24	28	64	13.750	56	28	44	64
12.500	100	40	28	56	13.125	56	32	48	64	13.760	86	40	64	100
12.500	100	40	32	64	13.125	72	48	56	64	13.889	100	24	24	72
12.542	86	40	28	48	13.139	86	40	44	72	13.933	86	48	56	72
12.508	86	44	64	100	13.157	72	28	44	86	13.935	86	24	28	72
12.558	72	32	48	86	13.163	86	28	24	56	13.953	72	24	40	86
12.571	64	40	44	56	13.200	72	24	44	100	13.953	100	40	48	86
12.572	44	28	32	40	13.258	100	44	28	48	13.960	86	44	40	56
12.600	72	32	56	100	13.289	100	28	32	86	13.968	64	28	44	72
12.627	100	44	40	72	13.289	100	56	64	86	14.000	56	24	24	40
12.686	100	44	48	86	13.333	64	24	24	48	14.000	48	24	28	40
12.698	64	28	40	72	13.333	64	24	28	56	14.000	64	32	28	40
12.727	64	32	28	44	13.333	56	28	32	48	14.025	72	44	48	56
12.728	56	24	24	44	13.333	56	28	48	72	14.026	72	28	24	44
12.728	48	24	28	44	13.333	64	32	48	72	14.063	72	32	40	64
12.732	100	48	44	72	13.393	100	56	48	64	14.071	86	44	72	100
12.758	64	28	48	86	13.393	100	28	24	64	14.078	86	48	44	56
12.791	100	40	44	86	13.393	100	32	24	56	14.142	72	40	44	56
12.798	86	48	40	56	13.396	72	40	64	86	14.204	100	44	40	64
12.800	64	28	56	100	13.437	86	32	28	56	14.260	56	24	44	72
12.800	64	24	48	100	13.438	86	24	24	64	14.286	40	24	24	28
12.834	56	40	44	48	13.438	86	32	24	48	14.286	48	24	40	56
12.834	44	24	28	40	13.469	48	28	44	56	14.286	64	32	40	56
12.857	72	28	32	64	13.500	72	32	24	40	14.286	100	40	32	56
12.857	72	24	24	56	13.500	72	40	48	64	14.318	72	32	28	44
12.857	72	28	24	48	13.514	86	28	44	100	14.319	72	44	56	64
12.858	48	28	24	32	13.566	100	24	28	86	14.322	100	48	44	64

Table of Leads, 14.333" to 16.914".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
14.333	86	40	32	48	15.238	64	28	48	72	15.989	100	32	44	86
14.333	86	24	40	100	15.239	64	28	32	48	16.000	64	24	24	40
14.333	86	40	48	72	15.239	64	24	32	56	16.000	48	24	32	40
14.352	72	28	48	86	15.272	56	40	48	44	16.000	56	28	32	40
14.400	72	24	48	100	15.278	44	24	40	48	16.042	56	24	44	64
14.400	72	28	56	100	15.279	100	40	44	72	16.042	56	32	44	48
14.400	72	32	64	100	15.306	100	28	24	56	16.043	44	24	28	32
14.536	100	32	40	86	15.349	72	24	44	86	16.071	72	32	40	56
14.545	64	24	24	44	15.357	86	28	24	48	16.071	72	28	40	64
14.545	48	24	32	44	15.357	86	24	24	56	16.125	86	32	24	40
14.545	56	28	32	44	15.357	86	28	32	64	16.125	86	40	48	64
14.583	56	32	40	48	15.429	72	40	48	56	16.204	100	24	28	72
14.583	56	24	40	64	15.429	72	28	24	40	16.204	100	48	56	72
14.583	100	40	28	48	15.469	72	32	44	64	16.233	100	44	40	56
14.584	40	24	28	32	15.480	86	40	72	100	16.280	100	40	56	86
14.651	72	32	56	86	15.504	100	48	64	86	16.288	86	44	40	48
14.659	86	44	48	64	15.504	100	24	32	86	16.296	64	24	44	72
14.659	86	32	24	44	15.556	64	32	56	72	16.327	64	28	40	56
14.667	64	40	44	48	15.556	64	24	28	48	16.333	56	24	28	40
14.668	44	24	32	40	15.556	56	24	32	48	16.364	72	24	24	44
14.694	72	28	32	56	15.556	32	24	28	24	16.370	100	48	44	56
14.743	86	28	48	100	15.556	56	24	48	72	16.423	86	32	44	72
14.780	86	40	44	64	15.584	48	28	40	44	16.456	72	28	64	100
14.800	100	44	56	86	15.625	100	24	24	64	16.500	72	40	44	48
14.815	64	24	40	72	15.625	100	32	24	48	16.500	48	32	44	40
14.849	56	24	28	44	15.625	100	32	28	56	16.612	100	28	40	86
14.880	100	48	40	56	15.636	86	40	32	44	16.623	64	28	32	44
14.884	64	28	56	86	15.677	86	32	28	48	16.667	56	28	40	48
14.884	64	24	48	86	15.677	86	24	28	64	16.667	64	32	40	48
14.931	86	32	40	72	15.677	86	48	56	64	16.667	100	40	32	48
14.933	64	24	56	100	15.714	44	24	24	28	16.667	100	40	48	72
14.950	100	56	72	86	15.714	48	24	44	56	16.722	86	40	56	72
15.000	48	24	24	32	15.714	64	32	44	56	16.744	72	24	48	86
15.000	56	28	24	32	15.750	72	32	28	40	16.744	72	28	56	86
15.000	72	24	24	48	15.750	72	40	56	64	16.744	72	32	64	86
15.000	72	24	28	56	15.767	86	24	44	100	16.752	86	44	48	56
15.000	72	24	32	64	15.873	100	56	64	72	16.753	86	28	24	44
15.000	56	28	48	64	15.874	100	28	32	72	16.797	86	32	40	64
15.050	86	32	56	100	15.909	100	40	28	44	16.800	72	24	56	100
15.150	100	44	32	48	15.909	56	32	40	44	16.875	72	32	48	64
15.151	100	44	48	72	15.925	86	48	64	72	16.892	86	40	44	56
15.202	86	44	56	72	15.926	86	24	32	72	16.914	100	44	64	86

Table of Leads, 16.969" to 20.20".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
16.969	64	44	56	48	17.918	86	32	48	72	19.091	72	24	28	44
16.970	64	24	28	44	17.959	64	28	44	56	19.096	100	32	44	72
16.970	56	24	32	44	18.000	72	24	24	40	19.111	86	40	64	72
17.045	100	32	24	44	18.181	56	28	40	44	19.136	72	28	64	86
17.046	100	44	48	64	18.181	64	32	40	44	19.197	86	32	40	56
17.062	86	28	40	72	18.181	100	40	32	44	19.197	86	28	40	64
17.101	86	44	56	64	18.182	48	24	40	44	19.200	72	24	64	100
17.102	86	32	28	44	18.229	100	32	28	48	19.250	56	32	44	40
17.141	64	32	48	56	18.229	100	24	28	64	19.285	72	32	48	56
17.143	64	28	24	32	18.229	100	48	56	64	19.285	72	28	48	64
17.144	48	24	24	28	18.273	100	28	44	86	19.286	72	28	24	32
17.144	72	28	32	48	18.285	64	28	32	40	19.350	86	32	72	100
17.144	72	24	32	56	18.333	56	28	44	48	19.380	100	24	40	86
17.144	72	48	64	56	18.333	64	32	44	48	19.394	64	24	32	44
17.188	100	40	44	64	18.367	72	28	40	56	19.444	40	24	28	24
17.200	86	32	64	100	18.428	86	28	24	40	19.444	56	24	40	48
17.200	86	28	56	100	18.428	86	40	48	56	19.444	100	40	56	72
17.200	86	24	48	100	18.476	86	32	44	64	19.480	100	28	24	44
17.275	86	56	72	64	18.519	100	24	32	72	19.480	100	44	48	56
17.361	100	32	40	72	18.519	100	48	64	72	19.531	100	32	40	64
17.364	64	24	56	86	18.605	100	40	64	86	19.535	72	24	56	86
17.373	86	44	64	72	18.663	100	64	86	72	19.545	86	24	24	44
17.442	100	32	48	86	18.667	64	24	28	40	19.590	64	28	48	56
17.442	100	48	72	86	18.667	56	24	32	40	19.635	72	40	48	44
17.454	64	40	48	44	18.667	64	40	56	48	19.642	100	40	44	56
17.500	56	24	24	32	18.700	72	44	64	56	19.643	44	28	40	32
17.500	48	24	28	32	18.700	72	28	32	44	19.656	86	28	64	100
17.500	72	24	28	48	18.750	100	32	24	40	19.687	72	32	56	64
17.500	56	24	48	64	18.750	72	24	40	64	19.710	86	40	44	48
17.550	86	28	32	56	18.750	72	32	40	48	19.840	100	28	40	72
17.677	100	44	56	72	18.750	100	40	48	64	19.886	100	44	56	64
17.679	72	32	44	56	18.770	86	28	44	72	19.887	100	32	28	44
17.679	72	28	44	64	18.812	86	32	28	40	19.908	86	24	40	72
17.778	64	24	32	48	18.812	86	40	56	64	19.934	100	28	48	86
17.778	64	24	48	72	18.858	48	28	44	40	20.00	72	24	32	48
17.778	64	28	56	72	18.939	100	44	40	48	20.00	64	24	24	32
17.858	100	24	24	56	19.029	100	44	72	86	20.00	56	24	24	28
17.858	100	28	32	64	19.048	40	24	32	28	20.07	86	24	56	100
17.858	100	28	24	48	19.048	64	24	40	56	20.09	100	56	72	64
17.917	86	24	32	64	19.048	64	28	40	48	20.16	86	48	72	64
17.917	86	24	28	56	19.090	56	32	48	44	20.16	86	32	48	64
17.918	86	24	24	48	19.090	72	44	56	48	20.20	100	44	64	72

Table of Leads, 20.20" to 24.55".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW
					21.43	100	28	24	40	23.04	86	32	48	56
20.20	72	28	44	56	21.48	100	32	44	64	23.04	86	28	48	64
20.35	100	32	56	86	21.50	86	24	24	40	23.04	86	28	24	32
20.36	64	40	56	44	21.82	72	44	64	48	23.14	100	24	40	72
20.41	100	28	32	56	21.82	100	28	44	72	23.26	100	32	64	86
20.42	56	24	28	32	21.82	64	32	48	44	23.26	100	28	56	86
20.45	72	32	40	44	21.82	56	28	48	44	23.26	100	24	48	86
20.48	86	48	64	56	21.82	72	24	32	44	23.33	64	32	56	48
20.48	86	28	48	72	21.88	100	40	56	64	23.33	48	24	28	24
20.48	86	28	32	48	21.88	100	32	28	40	23.33	64	24	28	32
20.48	86	24	32	56	21.90	86	24	44	72	23.38	72	28	40	44
20.57	72	40	64	56	21.94	86	28	40	56	23.44	100	48	72	64
20.57	72	28	32	40	21.99	86	44	72	64	23.44	100	32	48	64
20.63	72	32	44	48	22.00	64	32	44	40	23.45	86	40	48	44
20.63	72	24	44	64	22.00	48	24	44	40	23.52	86	32	56	64
20.74	64	24	56	72	22.00	56	28	44	40	23.57	72	28	44	48
20.78	64	28	40	44	22.04	72	28	48	56	23.57	72	24	44	56
20.83	100	32	48	72	22.11	86	28	72	100	23.57	48	28	44	32
20.83	100	24	32	64	22.22	100	40	64	72					
20.83	100	24	28	56	22.22	40	24	32	24	23.81	100	48	64	56
20.83	100	24	24	48	22.22	64	24	40	48	23.81	100	28	48	72
20.90	86	32	56	72	22.32	72	24	64	86	23.81	100	28	32	48
20.90	86	24	28	48	22.32	100	32	40	56	23.81	100	24	32	56
20.93	100	40	72	86	22.32	100	28	40	64	23.89	86	32	64	72
20.95	64	28	44	48	22.34	86	44	64	56	23.89	86	28	56	72
20.95	64	24	44	56	22.34	86	28	32	44	23.89	86	24	48	72
20.95	44	24	32	28	22.40	86	32	40	48	23.89	86	24	32	48
21.00	56	32	48	40	22.40	86	24	40	64	24.00	64	40	72	48
21.00	72	40	56	48	22.50	72	24	48	64	24.00	72	24	32	40
21.00	72	24	28	40	22.50	72	24	24	32	24.00	56	28	48	40
21.12	86	32	44	56	22.50	72	28	56	64	24.00	64	32	48	40
21.12	86	28	44	64	22.73	100	24	24	44	24.00	100	56	86	64
21.21	56	24	40	44	22.80	86	48	56	44	24.13	86	28	44	56
21.32	100	24	44	86	22.80	86	24	28	44	24.19	86	40	72	64
21.33	100	56	86	72	22.86	64	24	24	28	24.24	64	24	40	44
21.33	64	24	32	40	22.86	48	24	32	28	24.31	100	32	56	72
21.39	44	24	28	24	22.86	64	24	48	56	24.31	100	24	28	48
21.39	56	24	44	48	22.91	72	44	56	40	24.43	86	32	40	44
21.43	100	40	48	56	22.92	100	40	44	48	24.44	44	24	32	24
21.43	72	28	40	48	22.92	44	24	40	32	24.44	64	24	44	48
21.43	72	24	40	56	22.93	86	24	64	100	24.54	72	32	48	44
21.43	48	28	40	32	23.04	86	56	72	48	24.55	100	32	44	56

Table of Leads, 24.55" to 31.11".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW
24.55	100	28	44	64	26.52	100	24	28	44	28.57	100	56	64	40
24.57	86	40	64	56	26.58	100	28	64	86	28.57	48	28	40	24
24.57	86	28	32	40	26.67	64	28	56	48	28.57	64	32	40	28
24.64	86	24	44	64	26.67	56	24	32	28	28.57	100	28	32	40
24.64	86	32	44	48	26.67	48	24	32	24	28.64	72	44	56	32
24.75	72	32	44	40	26.79	100	48	72	56	28.65	100	32	44	48
24.88	100	72	86	48	26.79	100	32	48	56	28.65	100	24	44	64
24.93	64	28	48	44	26.79	100	28	48	64	28.67	86	40	64	48
25.00	72	24	40	48	26.79	100	28	24	32	28.67	86	24	32	40
25.00	48	24	40	32	26.88	86	28	56	64	29.09	64	24	48	44
25.00	56	28	40	32	26.88	86	24	48	64	29.09	64	48	56	44
25.00	100	24	24	40	26.88	86	24	24	32	29.17	100	40	56	48
25.08	86	24	28	40	27.00	72	32	48	40	29.17	56	24	40	32
25.09	86	40	56	48	27.13	100	24	56	86	29.17	100	24	28	40
25.13	86	44	72	56	27.15	100	44	86	72	29.22	100	56	72	44
25.14	64	28	44	40	27.22	56	24	28	24	29.32	86	48	72	44
25.45	64	44	56	32	27.27	100	40	48	44	29.32	86	32	48	44
25.45	56	24	48	44	27.27	72	24	40	44	29.34	64	24	44	40
25.46	100	24	44	72	27.30	86	28	64	72	29.39	72	28	64	56
25.51	100	28	40	56	27.34	100	32	56	64	29.56	86	32	44	40
25.57	100	64	72	44	27.36	86	40	56	44	29.76	100	28	40	48
25.60	86	28	40	48	27.43	64	28	48	40	29.76	100	24	40	56
25.60	86	24	40	56	27.50	56	32	44	28	29.86	100	40	86	72
25.67	56	24	44	40	27.50	48	24	44	32	29.86	86	24	40	48
25.71	72	24	48	56	27.50	72	24	44	48	29.90	100	28	72	86
25.71	72	56	64	32	27.64	86	40	72	56	30.00	56	28	48	32
25.72	72	24	24	28	27.78	100	32	64	72	30.00	72	32	64	48
25.80	86	24	72	100	27.78	100	28	56	72	30.00	72	28	56	48
25.97	100	44	64	56	27.78	100	24	48	72	30.23	86	32	72	64
25.97	100	28	32	44	27.78	100	24	32	48	30.30	100	48	64	44
26.04	100	32	40	48	27.87	86	24	56	72	30.30	100	24	32	44
26.04	100	24	40	64	27.92	86	28	40	44	30.48	64	24	32	28
26.06	86	44	64	48	28.00	100	64	86	48	30.54	100	44	86	64
26.06	86	24	32	44	28.00	64	32	56	40	30.56	44	24	40	24
26.16	100	32	72	86	28.00	56	24	48	40	30.61	100	28	48	56
26.18	72	40	64	44	28.05	72	28	48	44	30.71	86	24	48	56
26.19	44	24	40	28	28.06	100	28	44	56	30.71	86	32	64	56
26.25	72	32	56	48	28.13	100	40	72	64	30.72	86	24	24	28
26.25	72	24	56	64	28.15	86	28	44	48	30.86	72	28	48	40
26.25	72	24	28	32	28.15	86	24	44	56	31.01	100	24	64	86
26.33	86	28	48	56	28.29	72	28	44	40	31.11	64	24	56	48
26.52	100	44	56	48	28.41	100	32	40	44	31.11	56	24	32	24

Table of Leads, 31.11" to 41.99".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1 ST GEAR ON STUD	2 ND GEAR ON STUD	GEAR ON SCREW
31.11	64	24	28	24	34.09	100	44	48	32	37.50	72	24	40	32
31.25	100	28	56	64	34.20	86	44	56	32	37.63	86	32	56	40
31.25	100	24	48	64	34.29	72	48	64	28	37.88	100	24	40	44
31.25	100	24	24	32	34.29	72	24	64	56	38.10	64	24	40	28
31.27	86	40	64	44	34.29	64	32	48	28	38.18	72	24	56	44
31.35	86	32	56	48	34.29	72	24	32	28	38.20	100	24	44	48
31.35	86	24	56	64	34.38	100	32	44	40	38.39	100	40	86	56
31.36	86	24	28	32	34.55	86	32	72	56	38.39	86	28	40	32
31.43	64	28	44	32	34.55	86	28	72	64	38.57	72	28	48	32
31.43	48	24	44	28	34.72	100	24	40	48	38.89	56	24	40	24
31.50	72	32	56	40	34.88	100	24	72	86	38.96	100	28	48	44
31.75	100	72	64	28	34.90	100	56	86	44	39.09	86	32	64	44
31.82	100	44	56	40	35.00	72	24	56	48	39.09	86	28	56	44
31.85	86	24	64	72	35.00	56	24	48	32	39.09	86	24	48	44
31.99	100	56	86	48	35.00	72	24	28	24	39.29	100	28	44	40
32.00	64	28	56	40	35.10	86	28	64	56	39.42	86	24	44	40
32.00	64	24	48	40	35.16	100	32	72	64					
32.09	56	24	44	32	35.18	86	44	72	40	39.49	86	28	72	56
32.14	100	56	72	40	35.36	72	32	44	28	39.77	100	32	56	44
32.14	72	28	40	32	35.56	64	24	32	24	40.00	72	24	64	48
32.25	86	48	72	40	35.71	100	32	64	56	40.00	64	28	56	32
32.25	86	40	48	32	35.71	100	24	48	56	40.00	64	24	48	32
32.41	100	24	56	72	35.72	100	24	24	28	40.00	56	24	48	28
32.47	100	28	40	44	35.83	86	32	64	48	40.00	72	24	32	24
32.58	86	24	40	44	35.83	86	28	56	48	40.18	100	32	72	56
32.73	72	32	64	44	36.00	72	32	64	40	40.18	100	28	72	64
32.73	72	28	56	44	36.00	72	28	56	40	40.31	86	32	72	48
32.73	72	24	48	44	36.00	72	24	48	40	40.31	86	24	72	64
32.74	100	28	44	48	36.36	100	44	64	40	40.72	100	44	86	48
32.74	100	24	44	56	36.46	100	48	56	32	40.82	100	28	64	56
32.85	86	24	44	48	36.46	100	24	56	64	40.91	100	40	72	44
33.00	72	24	44	40	36.46	100	24	28	32	40.95	86	28	64	48
33.33	100	24	32	40	36.67	48	24	44	24	40.95	86	24	64	56
33.33	100	48	64	40	36.67	64	24	44	32	40.96	86	24	32	28
33.33	64	24	40	32	36.67	56	24	44	28	41.14	72	28	64	40
33.33	56	24	40	28	36.86	86	28	48	40	41.25	72	24	44	32
33.33	48	24	40	24	37.04	100	24	64	72	41.67	100	32	64	48
33.51	86	28	48	44	37.33	100	32	86	72	41.67	100	28	56	48
33.59	100	64	86	40	37.33	64	24	56	40	41.81	86	24	56	48
33.79	86	28	44	40	37.40	72	28	64	44	41.81	86	24	28	24
33.94	64	24	56	44	37.50	100	48	72	40	41.91	64	24	44	28
34.09	100	48	72	44	37.50	100	32	48	40	41.99	100	32	86	64

Table of Leads. 42.00" to 74.65".

	DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER		DRIVEN	DRIVER	DRIVEN	DRIVER
LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW	LEAD IN INCHES	GEAR ON WORM	1ST GEAR ON STUD	2ND GEAR ON STUD	GEAR ON SCREW
42.00	72	24	56	40	48.00	72	24	64	40	56.31	86	24	44	28
					48.38	86	32	72	40	57.14	100	28	64	40
42.23	86	28	44	32	48.61	100	24	56	48	57.30	100	24	44	32
42.66	100	28	86	72	48.61	100	24	28	24	57.33	86	24	64	40
42.78	56	24	44	24	48.86	100	40	86	44	58.33	100	24	56	40
42.86	100	28	48	40	48.89	64	24	44	24	58.44	100	28	72	44
42.86	72	24	40	28	49.11	100	28	44	32	58.64	86	24	72	44
43.00	86	32	64	40	49.14	86	28	64	40	59.53	100	24	40	28
43.00	86	28	56	40	49.27	86	24	44	32	59.72	86	24	40	24
43.00	86	24	48	40	49.77	100	24	86	72	60.00	72	24	64	32
43.64	72	24	64	44	50.00	100	28	56	40	60.00	72	24	56	28
43.75	100	32	56	40	50.00	100	24	48	40	60.00	72	24	48	24
43.98	86	32	72	44	50.00	72	24	40	24	60.61	100	24	64	44
44.44	64	24	40	24	50.00	100	32	64	40	61.08	100	32	86	44
44.64	100	28	40	32	50.17	86	24	56	40	61.43	86	28	64	32
44.68	86	28	64	44	50.26	86	28	72	44	61.43	86	24	48	28
44.79	100	40	86	48	51.14	100	32	72	44	62.22	64	24	56	24
44.79	86	24	40	32	51.19	86	24	40	28	62.50	100	24	72	48
45.00	72	28	56	32	51.43	72	28	64	32	62.50	100	28	56	32
45.00	72	24	48	32	51.43	72	24	48	28	62.50	100	24	48	32
45.45	100	32	64	44	51.95	100	28	64	44	62.71	86	24	56	32
45.45	100	24	48	44	52.08	100	24	40	32	63.99	100	28	86	48
45.46	100	28	56	44	52.12	86	24	64	44	63.99	100	24	86	56
45.61	86	24	56	44	52.50	72	24	56	32	64.29	100	28	72	40
45.72	64	24	48	28	53.03	100	24	56	44	64.50	86	24	72	40
45.84	100	24	44	40	53.33	64	24	56	28	65.48	100	24	44	28
45.92	100	28	72	56	53.33	64	24	48	24	65.70	86	24	44	24
46.07	86	28	72	48	53.57	100	28	72	48	66.67	100	24	64	40
46.07	86	24	72	56	53.57	100	24	72	56	67.19	100	32	86	40
46.07	86	28	48	32	53.57	86	24	72	48	68.18	100	24	72	44
46.67	64	24	56	32	53.57	100	28	48	32	68.57	72	24	64	28
46.67	56	24	48	24						69.11	86	28	72	32
46.88	100	32	72	48	53.75	86	24	48	32	69.44	100	24	40	24
46.88	100	24	72	64	53.75	86	28	56	32	69.80	100	28	86	44
47.15	72	24	44	28	54.85	100	28	86	56	70.00	72	24	56	24
47.62	100	28	64	48	55.00	72	24	44	24	71.43	100	28	64	32
47.62	100	24	64	56	55.28	86	28	72	40	71.43	100	24	48	28
47.62	100	24	32	28	55.56	100	24	32	24	71.67	86	24	64	32
47.78	86	24	64	48	55.56	100	24	64	48	71.67	86	24	56	28
47.78	86	24	32	24	55.99	100	24	86	64	71.67	86	24	48	24
47.99	100	32	86	56	55.99	100	32	86	48	72.92	100	24	56	32
47.99	100	28	86	64	56.25	100	32	72	40	74.65	100	24	86	48



Index Table.

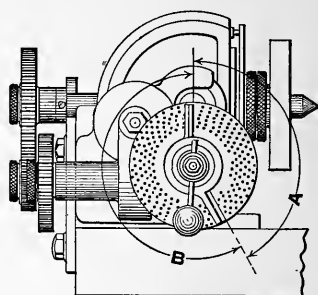
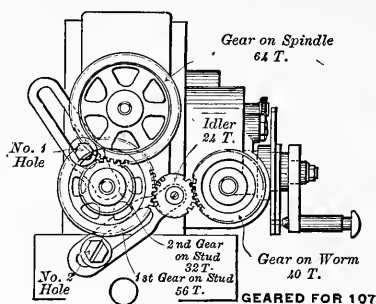
The following table contains all the data necessary to index for any number of divisions from 2 to 399 when using the spiral head of a Universal Milling Machine made by Brown & Sharpe Mfg. Co., equipped for differential indexing.

EXAMPLE: Required to index for 107 divisions.

Referring to table, 107 divisions calls for index plate with a 20 hole circle, 8 holes to be taken at each indexing. Gears must be used as follows: gear on worm 40 teeth, 1st gear on stud 56 teeth, 2d gear on stud 32 teeth and gear on spindle 64 teeth. To turn the index plate in the right direction, one idler is required. The sectors are to be set to the 78 graduation as called for and will then be correct for indexing 8 holes in a 20 hole circle.

INDEX TABLE 2 to 50

PLAIN & DIFFERENTIAL INDEXING



NUMBER OF DIVISIONS	INDEX CIRCLE	NO. OF TURNS OF INDEX	GRADUATION	NUMBER OF DIVISIONS	INDEX CIRCLE	NO. OF TURNS OF INDEX	GRADUATION	NUMBER OF DIVISIONS	INDEX CIRCLE	NO. OF TURNS OF INDEX	GRADUATION	NUMBER OF DIVISIONS	INDEX CIRCLE	NO. OF TURNS OF INDEX	GRADUATION
2	Any	20		13	39	3 $\frac{3}{39}$	14	26	39	1 $\frac{21}{39}$	106	40	Any	1	
3	39	13 $\frac{13}{39}$	65	14	49	2 $\frac{42}{49}$	169	27	27	1 $\frac{13}{27}$	95	41	41	$\frac{40}{41}$	3 *
	33	13 $\frac{11}{33}$	65		21	2 $\frac{18}{21}$	170		49	1 $\frac{21}{49}$	83	42	21	$\frac{20}{21}$	9 *
	18	13 $\frac{6}{18}$	65		39	2 $\frac{26}{39}$	132		21	1 $\frac{9}{21}$	85	43	43	$\frac{40}{43}$	12 *
4	Any	10		15	33	2 $\frac{22}{33}$	132	29	29	1 $\frac{11}{29}$	75	44	33	$\frac{30}{33}$	17 *
5	Any	8			18	2 $\frac{12}{18}$	132	30	39	1 $\frac{13}{39}$	65	45	27	$\frac{24}{27}$	21 *
6	39	6 $\frac{26}{39}$	132		20	2 $\frac{10}{20}$	98		33	1 $\frac{11}{33}$	65		18	$\frac{16}{18}$	21 *
	33	6 $\frac{22}{33}$	132	17	17	2 $\frac{6}{17}$	69		18	1 $\frac{6}{18}$	65	46	23	$\frac{20}{23}$	172
	18	6 $\frac{12}{18}$	132	18	27	2 $\frac{6}{27}$	43	31	31	1 $\frac{9}{31}$	56	47	47	$\frac{40}{47}$	168
7	49	5 $\frac{35}{49}$	140		18	2 $\frac{4}{18}$	43	32	20	1 $\frac{5}{20}$	48	48	18	$\frac{15}{18}$	165
	21	5 $\frac{15}{21}$	142		19	2 $\frac{2}{19}$	19	33	33	1 $\frac{7}{33}$	41	49	49	$\frac{40}{49}$	161
8	Any	5		20	Any	2		34	17	1 $\frac{3}{17}$	33	50	20	$\frac{16}{20}$	158
9	27	4 $\frac{12}{27}$	88	21	21	1 $\frac{10}{21}$	18 *	35	49	1 $\frac{7}{49}$	26	GRADUATIONS IN TABLE INDICATE SETTING FOR ARMS OF SECTOR WHEN INDEX CRANK MOVES THROUGH ARC "A," EXCEPT CASES MARKED * WHEN THE INDEX CRANK MOVES THROUGH ARC "B."			
	18	4 $\frac{8}{18}$	87	22	33	1 $\frac{27}{33}$	161		21	1 $\frac{3}{21}$	28				
10	Any	4		23	23	1 $\frac{17}{23}$	147	36	27	1 $\frac{3}{27}$	21				
11	33	3 $\frac{21}{33}$	126	24	39	1 $\frac{26}{39}$	132		18	1 $\frac{2}{18}$	21				
12	39	3 $\frac{13}{39}$	65		33	1 $\frac{22}{33}$	132	37	37	1 $\frac{3}{37}$	15				
	33	3 $\frac{11}{33}$	65		18	1 $\frac{12}{18}$	132	38	19	1 $\frac{1}{19}$	9				
	18	3 $\frac{6}{18}$	65	25	20	1 $\frac{12}{20}$	118	39	39	1 $\frac{1}{39}$	3				

INDEX TABLE 51 to 92.

NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERs		NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERs	
					1st GEAR ON STUD	2nd GEAR ON STUD		No. 1 HOLE	No. 2 HOLE						1st GEAR ON STUD	2nd GEAR ON STUD		No. 1 HOLE	No. 2 HOLE
51	17	$\frac{14}{17}$	33*	24			48	24	44	69	20	$\frac{12}{20}$	118	40			56	24	44
52	39	$\frac{30}{39}$	152							70	49	$\frac{28}{49}$	112						
53	49	$\frac{35}{49}$	140	56	40	24	72				21	$\frac{12}{21}$	113						
	21	$\frac{15}{21}$	142	56	40	24	72			71	27	$\frac{15}{27}$	110	72			40	24	
54	27	$\frac{20}{27}$	147								18	$\frac{10}{18}$	109	72			40	24	
55	33	$\frac{24}{33}$	144							72	27	$\frac{15}{27}$	110						
56	49	$\frac{35}{49}$	140								18	$\frac{10}{18}$	109						
	21	$\frac{15}{21}$	142							73	49	$\frac{28}{49}$	112	28			48	24	44
57	49	$\frac{35}{49}$	140	56			40	24	44		21	$\frac{12}{21}$	113	28			48	24	44
	21	$\frac{15}{21}$	142	56			40	24	44	74	37	$\frac{20}{37}$	107						
58	29	$\frac{20}{29}$	136							75	15	$\frac{8}{15}$	105						
59	39	$\frac{26}{39}$	132	48			32	44		76	19	$\frac{10}{19}$	103						
	33	$\frac{22}{33}$	132	48			32	44		77	20	$\frac{10}{20}$	98	32			48	44	
	18	$\frac{12}{18}$	132	48			32	44		78	39	$\frac{20}{39}$	101						
60	39	$\frac{26}{39}$	132							79	20	$\frac{10}{20}$	98	48			24	44	
	33	$\frac{22}{33}$	132							80	20	$\frac{10}{20}$	98						
	18	$\frac{12}{18}$	132							81	20	$\frac{10}{20}$	98	48			24	24	44
61	39	$\frac{26}{39}$	132	48			32	24	44	82	41	$\frac{20}{41}$	96						
	33	$\frac{22}{33}$	132	48			32	24	44	83	26	$\frac{10}{26}$	98	32			48	24	44
	18	$\frac{12}{18}$	132	48			32	24	44	84	21	$\frac{10}{21}$	94						
62	31	$\frac{20}{31}$	127							85	17	$\frac{8}{17}$	92						
63	39	$\frac{26}{39}$	132	24			48	24	44	86	43	$\frac{20}{43}$	91						
	33	$\frac{22}{33}$	132	24			48	24	44	87	15	$\frac{7}{15}$	92	40			24	24	44
	18	$\frac{12}{18}$	132	24			48	24	44	88	33	$\frac{15}{33}$	89						
64	16	$\frac{10}{16}$	123							89	27	$\frac{12}{27}$	88	72			32	44	
65	39	$\frac{24}{39}$	121								18	$\frac{8}{18}$	87	72			32	44	
66	33	$\frac{20}{33}$	120							90	27	$\frac{12}{27}$	88						
67	49	$\frac{28}{49}$	112	28			48	44			18	$\frac{8}{18}$	87						
	21	$\frac{12}{21}$	113	28			48	44		91	39	$\frac{18}{39}$	91	24			48	24	44
68	17	$\frac{10}{17}$	116							92	23	$\frac{10}{23}$	86						

INDEX TABLE 93 to 125.

NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERs		NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERs	
					1st GEAR ON STUD	2nd GEAR ON STUD		No. 1 HOLE	No. 2 HOLE						1st GEAR ON STUD	2nd GEAR ON STUD		No. 1 HOLE	No. 2 HOLE
93	27	$\frac{12}{27}$	88	24			32	24	44	114	39	$\frac{13}{39}$	65	24			48	44	
	18	$\frac{8}{18}$	87	24			32	24	44		33	$\frac{11}{33}$	65	24			48	44	
94	47	$\frac{20}{47}$	83								18	$\frac{6}{18}$	65	24			48	44	
95	19	$\frac{8}{19}$	82							115	23	$\frac{8}{23}$	68						
96	49	$\frac{21}{49}$	83	28			32	24	44	116	29	$\frac{10}{29}$	68						
	21	$\frac{9}{21}$	85	28			32	24	44	117	39	$\frac{13}{39}$	65	24			24	56	
97	20	$\frac{8}{20}$	78	40			48	44			33	$\frac{11}{33}$	65	24			24	56	
98	49	$\frac{20}{49}$	79								18	$\frac{6}{18}$	65	24			24	56	
99	20	$\frac{8}{20}$	78	56	28	40	32			118	39	$\frac{13}{39}$	65	48			32	44	
100	20	$\frac{8}{20}$	78								33	$\frac{11}{33}$	65	48			32	44	
101	20	$\frac{8}{20}$	78	72	24	40	48		24		18	$\frac{6}{18}$	65	48			32	44	
102	20	$\frac{8}{20}$	78	40			32	24	44	119	39	$\frac{13}{39}$	65	72			24	44	
103	20	$\frac{8}{20}$	78	40			48	24	44		33	$\frac{11}{33}$	65	72			24	44	
104	39	$\frac{15}{39}$	75								18	$\frac{6}{18}$	65	72			24	44	
105	21	$\frac{8}{21}$	75								39	$\frac{13}{39}$	65						
106	43	$\frac{16}{43}$	73	86	24	24	48			120	33	$\frac{11}{33}$	65						
107	20	$\frac{8}{20}$	78	40	56	32	64		24		18	$\frac{6}{18}$	65						
108	27	$\frac{10}{27}$	73							121	39	$\frac{13}{39}$	65	72			24	24	44
109	16	$\frac{6}{16}$	73	32			28	24	44		33	$\frac{11}{33}$	65	72			24	24	44
110	33	$\frac{12}{33}$	71								18	$\frac{6}{18}$	65	72			24	24	44
111	39	$\frac{13}{39}$	65	24			72	32		122	39	$\frac{13}{39}$	65	48			32	24	44
	33	$\frac{11}{33}$	65	24			72	32			33	$\frac{11}{33}$	65	48			32	24	44
	18	$\frac{6}{18}$	65	24			72	32			18	$\frac{6}{18}$	65	48			32	24	44
112	39	$\frac{13}{39}$	65	24			64	44		123	39	$\frac{13}{39}$	65	24			24	24	44
	33	$\frac{11}{33}$	65	24			64	44			33	$\frac{11}{33}$	65	24			24	24	44
	18	$\frac{6}{18}$	65	24			64	44			18	$\frac{6}{18}$	65	24			24	24	44
113	39	$\frac{13}{39}$	65	24			56	44		124	31	$\frac{10}{31}$	63						
	33	$\frac{11}{33}$	65	24			56	44			39	$\frac{13}{39}$	65	24			40	24	44
	18	$\frac{6}{18}$	65	24			56	44		125	33	$\frac{11}{33}$	65	24			40	24	44
											18	$\frac{6}{18}$	65	24			40	24	44

INDEX TABLE 126 to 168.

NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERS		NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERS	
					1ST GEAR ON STUD	2ND GEAR ON STUD		No. 1 HOLE	No. 2 HOLE						1ST GEAR ON STUD	2ND GEAR ON STUD		No. 1 HOLE	No. 2 HOLE
126	39	$\frac{13}{39}$	65	24			48	24	44	143	49	$\frac{14}{49}$	55	28			24	24	44
	33	$\frac{11}{33}$	65	24			48	24	44		21	$\frac{6}{21}$	56	28			24	24	44
	18	$\frac{6}{18}$	65	24			48	24	44		18	$\frac{5}{18}$	54						
127	39	$\frac{13}{39}$	65	24			56	24	44	145	29	$\frac{8}{29}$	54						
	33	$\frac{11}{33}$	65	24			56	24	44		49	$\frac{14}{49}$	55	28			48	24	44
	18	$\frac{6}{18}$	65	24			56	24	44		21	$\frac{6}{21}$	56	28			48	24	44
128	16	$\frac{5}{16}$	61							147	49	$\frac{14}{49}$	55	24			48	24	44
129	39	$\frac{13}{39}$	65	24			72	24	44		21	$\frac{6}{21}$	56	24			48	24	44
	33	$\frac{11}{33}$	65	24			72	24	44		37	$\frac{10}{37}$	53						
	18	$\frac{6}{18}$	65	24			72	24	44	149	49	$\frac{14}{49}$	55	28			72	24	44
130	39	$\frac{12}{39}$	60								21	$\frac{6}{21}$	56	28			72	24	44
131	20	$\frac{6}{20}$	58	40			28	44		150	15	$\frac{4}{15}$	52						
132	33	$\frac{10}{33}$	59							151	20	$\frac{5}{20}$	48	32			72	44	
133	49	$\frac{14}{49}$	55	24			48	44		152	19	$\frac{5}{19}$	51						
	21	$\frac{6}{21}$	56	24			48	44		153	20	$\frac{5}{20}$	48	32			56	44	
134	49	$\frac{14}{49}$	55	28			48	44		154	20	$\frac{5}{20}$	48	32			48	44	
	21	$\frac{6}{21}$	56	28			48	44		155	31	$\frac{8}{31}$	50						
135	27	$\frac{8}{27}$	58							156	39	$\frac{10}{39}$	50						
136	17	$\frac{5}{17}$	57							157	20	$\frac{5}{20}$	48	32			24	56	
137	49	$\frac{14}{49}$	55	28			24	56		158	20	$\frac{5}{20}$	48	48			24	44	
	21	$\frac{6}{21}$	56	28			24	56		159	20	$\frac{5}{20}$	48	64	32	56	28		
138	49	$\frac{14}{49}$	55	56			32	44		160	20	$\frac{5}{20}$	48						
	21	$\frac{6}{21}$	56	56			32	44		161	20	$\frac{5}{20}$	48	64	32	56	28		24
139	49	$\frac{14}{49}$	55	56	32	48	24			162	20	$\frac{5}{20}$	48	48			24	24	44
	21	$\frac{6}{21}$	56	56	32	48	24			163	20	$\frac{5}{20}$	48	32			24	24	44
140	49	$\frac{14}{49}$	55							164	41	$\frac{10}{41}$	47						
	21	$\frac{6}{21}$	56							165	33	$\frac{8}{33}$	47						
141	18	$\frac{5}{18}$	54	48			40	44		166	20	$\frac{5}{20}$	48	32			48	24	44
142	49	$\frac{14}{49}$	55	56			32	24	44	167	20	$\frac{5}{20}$	48	32			56	24	44
	21	$\frac{6}{21}$	56	56			32	24	44	168	21	$\frac{5}{21}$	47						

INDEX TABLE 169 to 214.

NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERS		NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERS	
					1st GEAR ON STUD	2nd GEAR ON STUD		No. 1 HOLE	No. 2 HOLE						1st GEAR ON STUD	2nd GEAR ON STUD		No. 1 HOLE	No. 2 HOLE
169	20	$\frac{5}{20}$	48	32			72	24	44	187	27	$\frac{6}{27}$	43	72	48	24	56		24
170	17	$\frac{4}{17}$	45								18	$\frac{4}{18}$	43	72	48	24	56		24
171	21	$\frac{5}{21}$	47	56			40	24	44	188	47	$\frac{10}{47}$	40						
172	43	$\frac{10}{43}$	44							189	27	$\frac{6}{27}$	43	32			64	24	44
173	27	$\frac{6}{27}$	43	72	56	32	64				18	$\frac{4}{18}$	43	32			64	24	44
	18	$\frac{4}{18}$	43	72	56	32	64			190	19	$\frac{4}{19}$	40						
174	27	$\frac{6}{27}$	43	24			32	56		191	20	$\frac{4}{20}$	38	40			72	24	
	18	$\frac{4}{18}$	43	24			32	56		192	20	$\frac{4}{20}$	38	40			64	44	
175	27	$\frac{6}{27}$	43	72	40	32	64			193	20	$\frac{4}{20}$	38	40			56	44	
	18	$\frac{4}{18}$	43	72	40	32	64			194	20	$\frac{4}{20}$	38	40			48	44	
176	27	$\frac{6}{27}$	43	72	24	24	64			195	39	$\frac{8}{39}$	39						
	18	$\frac{4}{18}$	43	72	24	24	64			196	49	$\frac{10}{49}$	38						
177	27	$\frac{6}{27}$	43	72			48	24		197	20	$\frac{4}{20}$	38	40			24	56	
	18	$\frac{4}{18}$	43	72			48	24		198	20	$\frac{4}{20}$	38	56	28	40	32		
178	27	$\frac{6}{27}$	43	72			32	44		199	20	$\frac{4}{20}$	38	100	40	64	32		
	18	$\frac{4}{18}$	43	72			32	44		200	20	$\frac{4}{20}$	38						
179	27	$\frac{6}{27}$	43	72	24	48	32			201	20	$\frac{4}{20}$	38	72	24	40	24		24
	18	$\frac{4}{18}$	43	72	24	48	32			202	20	$\frac{4}{20}$	38	72	24	40	48		24
180	27	$\frac{6}{27}$	43							203	20	$\frac{4}{20}$	38	40			24	24	44
	18	$\frac{4}{18}$	43							204	20	$\frac{4}{20}$	38	40			32	24	44
181	27	$\frac{6}{27}$	43	72	24	48	32		24	205	41	$\frac{8}{41}$	37						
	18	$\frac{4}{18}$	43	72	24	48	32		24	206	20	$\frac{4}{20}$	38	40			48	24	44
182	27	$\frac{6}{27}$	43	72			32	24	44	207	20	$\frac{4}{20}$	38	40			56	24	44
	18	$\frac{4}{18}$	43	72			32	24	44	208	20	$\frac{4}{20}$	38	40			64	24	44
183	27	$\frac{6}{27}$	43	48			32	24	44	209	20	$\frac{4}{20}$	38	40			72	24	44
	18	$\frac{4}{18}$	43	48			32	24	44	210	21	$\frac{4}{21}$	37						
184	23	$\frac{5}{23}$	42							211	16	$\frac{3}{16}$	36	64			28	44	
185	37	$\frac{8}{37}$	42							212	43	$\frac{8}{43}$	35	86	24	24	48		
186	27	$\frac{6}{27}$	43	48			64	24	44	213	27	$\frac{5}{27}$	36	72			40	44	
	18	$\frac{4}{18}$	43	48			64	24	44	214	20	$\frac{4}{20}$	38	40	56	32	64		24

INDEX TABLE 215 to 270.

NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERS		NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERS	
					1ST GEAR ON STUD	2ND GEAR ON STUD		No. 1 HOLE	No. 2 HOLE						1ST GEAR ON STUD	2ND GEAR ON STUD		No. 1 HOLE	No. 2 HOLE
215	43	$\frac{8}{43}$	35							245	49	$\frac{6}{49}$	30						
216	27	$\frac{5}{27}$	36							246	18	$\frac{3}{18}$	32	24			24	24	44
217	21	$\frac{4}{21}$	37	48			64	24	44	247	18	$\frac{3}{18}$	32	48			56	24	44
218	16	$\frac{3}{16}$	36	64			56	24	44	248	31	$\frac{5}{31}$	31						
219	21	$\frac{4}{21}$	37	28			48	24	44	249	18	$\frac{3}{18}$	32	32			48	24	44
220	33	$\frac{6}{33}$	35							250	18	$\frac{3}{18}$	32	24			40	24	44
221	17	$\frac{3}{17}$	33	24			24	56		251	18	$\frac{3}{18}$	32	48	44	32	64		24
222	18	$\frac{3}{18}$	32	24			72	44		252	18	$\frac{3}{18}$	32	24			48	24	44
223	43	$\frac{8}{43}$	35	86	48	24	64		24	253	33	$\frac{5}{33}$	29	24			40	56	
224	18	$\frac{3}{18}$	32	24			64	44		254	18	$\frac{3}{18}$	32	24			56	24	44
225	27	$\frac{5}{27}$	36	24			40	24	44	255	18	$\frac{3}{18}$	32	48	40	24	72		24
226	18	$\frac{3}{18}$	32	24			56	44		256	18	$\frac{3}{18}$	32	24			64	24	44
227	49	$\frac{8}{49}$	30	56	64	28	72			257	49	$\frac{8}{49}$	30	56	48	28	64		24
228	18	$\frac{3}{18}$	32	24			48	44		258	43	$\frac{7}{43}$	31	32			64	24	44
229	18	$\frac{3}{18}$	32	24			44	48		259	49	$\frac{7}{49}$	26	24			72	44	
230	23	$\frac{4}{23}$	34							260	21	$\frac{3}{21}$	28	24			72	44	
231	18	$\frac{3}{18}$	32	32			48	44		261	39	$\frac{6}{39}$	29						
232	29	$\frac{5}{29}$	33							262	29	$\frac{4}{29}$	26	48	64	24	72		
233	18	$\frac{3}{18}$	32	48			56	44		263	20	$\frac{3}{20}$	28	40			28	44	
234	18	$\frac{3}{18}$	32	24			24	56		264	49	$\frac{8}{49}$	30	56	64	28	72		24
235	47	$\frac{8}{47}$	32							265	33	$\frac{5}{33}$	29						
236	18	$\frac{3}{18}$	32	48			32	44		266	49	$\frac{7}{49}$	26	56	40	24	72		
237	18	$\frac{3}{18}$	32	48			24	44		267	21	$\frac{3}{21}$	28	56	40	24	72		
238	18	$\frac{3}{18}$	32	72			24	44		268	49	$\frac{7}{49}$	26	32			64	44	
239	18	$\frac{3}{18}$	32	72	24	64	32			269	21	$\frac{3}{21}$	28	32			64	44	
240	18	$\frac{3}{18}$	32							270	27	$\frac{4}{27}$	28				32	44	
241	18	$\frac{3}{18}$	32	72	24	64	32		24	271	49	$\frac{7}{49}$	26	28			48	44	
242	18	$\frac{3}{18}$	32	72			24	24	44	272	21	$\frac{3}{21}$	28	28			48	44	
243	18	$\frac{3}{18}$	32	64			32	24	44	273	20	$\frac{3}{20}$	28	64	32	40	28		24
244	18	$\frac{3}{18}$	32	48			32	24	44	274	27	$\frac{4}{27}$	28						

INDEX TABLE 271 to 310

NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERs		NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERs	
					1ST GEAR ON STUD	2ND GEAR ON STUD		No. 1 HOLE	No. 2 HOLE						1ST GEAR ON STUD	2ND GEAR ON STUD		No. 1 HOLE	No. 2 HOLE
271	49	$\frac{7}{49}$	26	56	24	24	72			287	49	$\frac{7}{49}$	26	24			24	24	44
	21	$\frac{3}{21}$	28	56	24	24	72				21	$\frac{3}{21}$	28	24			24	24	44
272	49	$\frac{7}{49}$	26	56			64	24		288	49	$\frac{7}{49}$	26	28			32	24	44
	21	$\frac{3}{21}$	28	56			64	24			21	$\frac{3}{21}$	28	28			32	24	44
273	49	$\frac{7}{49}$	26	24			24	56		289	49	$\frac{7}{49}$	26	56	24	24	72		24
	21	$\frac{3}{21}$	28	24			24	56			21	$\frac{3}{21}$	28	56	24	24	72		24
274	49	$\frac{7}{49}$	26	56			48	44		290	29	$\frac{4}{29}$	26						
	21	$\frac{3}{21}$	28	56			48	44			15	$\frac{2}{15}$	25	40			48	44	
275	49	$\frac{7}{49}$	26	56			40	44		292	49	$\frac{7}{49}$	26	28			48	24	44
	21	$\frac{3}{21}$	28	56			40	44			21	$\frac{3}{21}$	28	28			48	24	44
276	49	$\frac{7}{49}$	26	56			32	44		293	15	$\frac{2}{15}$	25	48	32	40	56		
	21	$\frac{3}{21}$	28	56			32	44			49	$\frac{7}{49}$	26	24			48	24	44
277	49	$\frac{7}{49}$	26	56			24	44		294	21	$\frac{3}{21}$	28	24			48	24	44
	21	$\frac{3}{21}$	28	56			24	44			15	$\frac{2}{15}$	25	48			32	44	
278	49	$\frac{7}{49}$	26	56	32	48	24			296	37	$\frac{5}{37}$	26						
	21	$\frac{3}{21}$	28	56	32	48	24				33	$\frac{4}{33}$	23	28	48	24	56		
279	27	$\frac{4}{27}$	28	24			32	24	44	298	49	$\frac{7}{49}$	26	28			72	24	44
	49	$\frac{7}{49}$	26								21	$\frac{3}{21}$	28	28			72	24	44
280	49	$\frac{7}{49}$	26							299	23	$\frac{3}{23}$	25	24			24	56	
	21	$\frac{3}{21}$	28								15	$\frac{2}{15}$	25						
281	49	$\frac{7}{49}$	26	72	24	56	24		24	300	43	$\frac{6}{43}$	26	24			48	24	44
	21	$\frac{3}{21}$	28	72	24	56	24		24		16	$\frac{2}{16}$	24	32			72	24	
282	43	$\frac{6}{43}$	26	86	24	24	56			302	15	$\frac{2}{15}$	25	72	24	40	48		24
	49	$\frac{7}{49}$	26	56			24	24	44		16	$\frac{2}{16}$	24	24			48	44	
283	49	$\frac{7}{49}$	26	56			32	24	44	304	15	$\frac{2}{15}$	25	48			32	24	44
	21	$\frac{3}{21}$	28	56			32	24	44		15	$\frac{2}{15}$	25	40			32	24	44
284	49	$\frac{7}{49}$	26	56			40	24	44	306	15	$\frac{2}{15}$	25	72	48	40	56		24
	21	$\frac{3}{21}$	28	56			40	24	44		16	$\frac{2}{16}$	24	32			48	44	
285	49	$\frac{7}{49}$	26	56			48	24	44	308	15	$\frac{2}{15}$	25	40			48	24	44
	21	$\frac{3}{21}$	28	56			48	24	44		31	$\frac{4}{31}$	24						
286	49	$\frac{7}{49}$	26	56			48	24	44	310	49	$\frac{7}{49}$	26	28			48	24	44
	21	$\frac{3}{21}$	28	56			48	24	44		21	$\frac{3}{21}$	28	28			48	24	44

INDEX TABLE 311 to 355

NUMBER OF DIVISIONS	INDEX CIRCLE	NO. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No.1 HOLE		GEAR ON SPINDLE	IDLERS		NUMBER OF DIVISIONS	INDEX CIRCLE	NO. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No.1 HOLE		GEAR ON SPINDLE	IDLERS	
					1ST GEAR ON STUD	2ND GEAR ON STUD		No. 1 HOLE	No. 2 HOLE						1ST GEAR ON STUD	2ND GEAR ON STUD		No. 1 HOLE	No. 2 HOLE
311	16	$\frac{2}{16}$	24	64	24	24	72			339	27	$\frac{3}{27}$	21	24			56	44	
312	39	$\frac{5}{39}$	24								18	$\frac{2}{18}$	21	24			56	44	
313	16	$\frac{2}{16}$	24	32			28	56		340	17	$\frac{2}{17}$	22						
314	16	$\frac{2}{16}$	24	32			24	56		341	43	$\frac{5}{43}$	21	86	24	32	40		
315	16	$\frac{2}{16}$	24	64			40	24		342	27	$\frac{3}{27}$	21	32			64	44	
316	16	$\frac{2}{16}$	24	64			32	44			18	$\frac{2}{18}$	21	32			64	44	
317	16	$\frac{2}{16}$	24	64			24	44		343	15	$\frac{2}{15}$	25	40	64	24	86		24
318	16	$\frac{2}{16}$	24	56	28	48	24			344	43	$\frac{5}{43}$	21						
319	29	$\frac{4}{29}$	26	48	64	24	72		24	345	27	$\frac{3}{27}$	21	24			40	56	
320	16	$\frac{2}{16}$	24								18	$\frac{2}{18}$	21	24			40	56	
321	16	$\frac{2}{16}$	24	72	24	64	24		24	346	27	$\frac{3}{27}$	21	72	56	32	64		
322	23	$\frac{3}{23}$	25	32			64	24	44		18	$\frac{2}{18}$	21	72	56	32	64		
323	16	$\frac{2}{16}$	24	64			24	24	44	347	43	$\frac{5}{43}$	21	86	24	32	40		24
324	16	$\frac{2}{16}$	24	64			32	24	44	348	27	$\frac{3}{27}$	21	24			32	56	
325	16	$\frac{2}{16}$	24	64			40	24	44		18	$\frac{2}{18}$	21	24			32	56	
326	16	$\frac{2}{16}$	24	32			24	24	44	349	27	$\frac{3}{27}$	21	72	44	24	48		
327	16	$\frac{2}{16}$	24	32			28	24	44		18	$\frac{2}{18}$	21	72	44	24	48		
328	41	$\frac{5}{41}$	23							350	27	$\frac{3}{27}$	21	72	40	32	64		
329	16	$\frac{2}{16}$	24	64	24	24	72		24		18	$\frac{2}{18}$	21	72	40	32	64		
330	33	$\frac{4}{33}$	23							351	27	$\frac{3}{27}$	21	24			24	56	
331	16	$\frac{2}{16}$	24	64	44	24	48		24		18	$\frac{2}{18}$	21	24			24	56	
332	16	$\frac{2}{16}$	24	32			48	24	44	352	27	$\frac{3}{27}$	21	72	24	24	64		
333	27	$\frac{3}{27}$	21	24			72	44			18	$\frac{2}{18}$	21	72	24	24	64		
	18	$\frac{2}{18}$	21	24			72	44		353	27	$\frac{3}{27}$	21	72	24	24	56		
334	16	$\frac{2}{16}$	24	32			56	24	44		18	$\frac{2}{18}$	21	72	24	24	56		
335	33	$\frac{4}{33}$	23	72	48	44	40		24	354	27	$\frac{3}{27}$	21	72			48	24	
336	16	$\frac{2}{16}$	24	32			64	24	44		18	$\frac{2}{18}$	21	72			48	24	
337	43	$\frac{5}{43}$	21	86	40	32	56			355	27	$\frac{3}{27}$	21	72			40	24	
338	16	$\frac{2}{16}$	24	32			72	24	44		18	$\frac{2}{18}$	21	72			40	24	

INDEX TABLE 356 to 399.

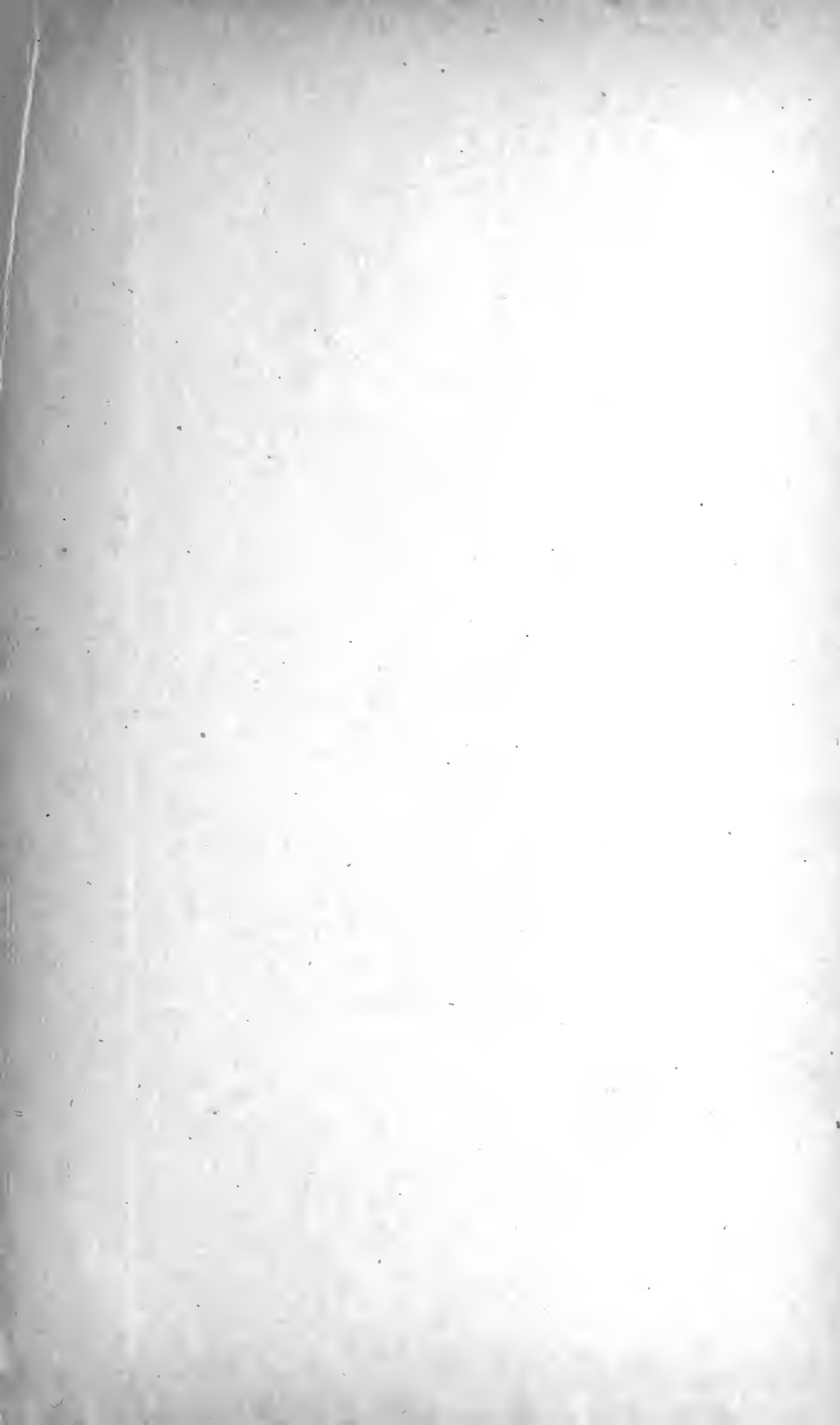
NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERS		NUMBER OF DIVISIONS	INDEX CIRCLE	No. OF TURNS OF INDEX	GRADUATION	GEAR ON WORM	No. 1 HOLE		GEAR ON SPINDLE	IDLERS	
					1st GEAR ON STUD	2nd GEAR ON STUD		No. 1 HOLE	No. 2 HOLE						1st GEAR ON STUD	2nd GEAR ON STUD		No. 1 HOLE	No. 2 HOLE
356	27	$\frac{3}{27}$	21	72			32	24		374	27	$\frac{3}{27}$	21	72	56	32	64		24
	18	$\frac{2}{18}$	21	72			32	24			18	$\frac{2}{18}$	21	72	56	32	64		24
357	27	$\frac{3}{27}$	21	72			24	44		375	27	$\frac{3}{27}$	21	24			40	24	44
	18	$\frac{2}{18}$	21	72			24	44			18	$\frac{2}{18}$	21	24			40	24	44
358	27	$\frac{3}{27}$	21	72	32	48	24			376	47	$\frac{5}{47}$	19						
	18	$\frac{2}{18}$	21	72	32	48	24			377	29	$\frac{3}{29}$	19	24			24	56	
359	43	$\frac{5}{43}$	21	86	48	32	100		24	378	27	$\frac{3}{27}$	21	32			64	24	44
	27	$\frac{3}{27}$	21								18	$\frac{2}{18}$	21	32			64	24	44
360	18	$\frac{2}{18}$	21							379	20	$\frac{2}{20}$	18	48	56	40	72		
	19	$\frac{2}{19}$	19	32			64	44		380	19	$\frac{2}{19}$	19						
362	27	$\frac{3}{27}$	21	72	28	56	32		24	381	27	$\frac{3}{27}$	21	24			56	24	44
	18	$\frac{2}{18}$	21	72	28	56	32		24		18	$\frac{2}{18}$	21	24			56	24	44
363	27	$\frac{3}{27}$	21	72			24	24	44	382	20	$\frac{2}{20}$	18	40			72	24	
	18	$\frac{2}{18}$	21	72			24	24	44	383	20	$\frac{2}{20}$	18	40			68*		
364	27	$\frac{3}{27}$	21	72			32	24	44	384	20	$\frac{2}{20}$	18	40			64	44	
	18	$\frac{2}{18}$	21	72			32	24	44	385	20	$\frac{2}{20}$	18	32			48	44	
365	20	$\frac{2}{20}$	18	32	48	24	56			386	20	$\frac{2}{20}$	18	40			56	44	
	27	$\frac{3}{27}$	21	48			32	24	44	387	43	$\frac{4}{43}$	15	32	56	28	64		
366	18	$\frac{2}{18}$	21	48			32	24	44	388	20	$\frac{2}{20}$	18	40			48	44	
	27	$\frac{3}{27}$	21	72	24	24	56		24	389	20	$\frac{2}{20}$	18	40			44	56	
367	18	$\frac{2}{18}$	21	72	24	24	56		24	390	39	$\frac{4}{39}$	17						
	27	$\frac{3}{27}$	21	72	24	24	64		24	391	20	$\frac{2}{20}$	18	48	24	40	72		
368	18	$\frac{2}{18}$	21	72	24	24	64		24	392	49	$\frac{5}{49}$	16						
	41	$\frac{4}{41}$	18	32	56	28	64			393	20	$\frac{2}{20}$	18	40			28	44	
370	37	$\frac{4}{37}$	20							394	20	$\frac{2}{20}$	18	40			24	56	
	21	$\frac{2}{21}$	18	32	56	24	64			395	20	$\frac{2}{20}$	18	64			32	44	
372	27	$\frac{3}{27}$	21	48			64	24	44	396	20	$\frac{2}{20}$	18	56	28	40	32		
	18	$\frac{2}{18}$	21	48			64	24	44	397	20	$\frac{2}{20}$	18	64	24	40	32		
373	20	$\frac{2}{20}$	18	40	48	32	72			398	20	$\frac{2}{20}$	18	100	40	64	32		
										399	21	$\frac{2}{21}$	18	32			64	44	

* SPECIAL GEAR.

DECIMAL EQUIVALENTS OF PARTS OF AN INCH.

$\frac{1}{64}$. . .01563	$\frac{21}{64}$. .32813	$\frac{45}{64}$. .70313
$\frac{1}{32}$. . .03125	$\frac{11}{32}$. .34375	$\frac{23}{32}$. .71875
$\frac{3}{64}$. .04688	$\frac{23}{64}$. .35938	$\frac{47}{64}$. .73438
1-16 . . .0625	3-8 . . .375	3-4 . . .75
$\frac{5}{64}$. .07813	$\frac{25}{64}$. .39063	$\frac{49}{64}$. .76563
$\frac{3}{32}$. .09375	$\frac{13}{32}$. .40625	$\frac{25}{32}$. .78125
$\frac{7}{64}$. .10938	$\frac{27}{64}$. .42188	$\frac{51}{64}$. .79688
1-8 . . .125	7-16 . .4375	13-16 . .8125
$\frac{9}{64}$. .14063	$\frac{29}{64}$. .45313	$\frac{53}{64}$. .82813
$\frac{5}{32}$. .15625	$\frac{15}{32}$. .46875	$\frac{27}{32}$. .84375
$\frac{11}{64}$. .17188	$\frac{31}{64}$. .48438	$\frac{55}{64}$. .85938
3-16 . . .1875	1-2 . . .5	7-8 . . .875
$\frac{13}{64}$. .20313	$\frac{33}{64}$. .51563	$\frac{57}{64}$. .89063
$\frac{7}{32}$. .21875	$\frac{17}{32}$. .53125	$\frac{29}{32}$. .90625
$\frac{15}{64}$. .23438	$\frac{35}{64}$. .54688	$\frac{59}{64}$. .92188
1-4 . . .25	9-16 . .5625	15-16 . .9375
$\frac{17}{64}$. .26563	$\frac{37}{64}$. .57813	$\frac{61}{64}$. .95313
$\frac{9}{32}$. .28125	$\frac{19}{32}$. .59375	$\frac{31}{32}$. .96875
$\frac{19}{64}$. .29688	$\frac{39}{64}$. .60938	$\frac{63}{64}$. .98438
5-16 . . .3125	5-8 . . .625	1 . . .1.00000
	$\frac{41}{64}$. .64063	
	$\frac{21}{32}$. .65625	
	$\frac{43}{64}$. .67188	
	11-16 . .6875	

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